

Prediction of airfoil performance at high Reynolds numbers.

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Prediction of airfoil performance at high Reynolds numbers EFMC 2014, Copenhagen 17-20 Sept 2014

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Introduction Large Scale Wind Turbines

Increasing the rotor size may potentially lead to two obvious aerodynamic issues

- High Mach numbers in the tip region
 - Might be harmful for performance
 - Possible to avoid
- High Reynolds numbers
 - Might be beneficial for performance
 - Hard to avoid



DTU 10 MW Reference Turbine

Introduction Airfoil performance at high Reynolds Numbers



We expect that increasing the Reynolds Number will:

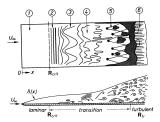
- Decrease the viscous effects due to the thinning of the boundary layer
- Promote earlier transition due to increased Reynolds number

Quantification of the effects can be done by:

- Measurements
 - Tunnel measurements are difficult to obtain at high Re and low Mach
 - Openly available data are sparse
- Computations
 - Model performance in this range is unknown

Introduction Laminar turbulent transition

- The transition process depend on many parameters
 - Reynolds Number
 - Free stream turbulence level
 - Laminar separation bubbles
 - Cross flow
 - Surface roughness
 - Mass injection
- Typically approaches for transition modeling
 - *eⁿ* method (Orr-Sommerfeld eqn.)
 - Empirical correlations
 - Michel
 - Mayle
 - Abu-Ghannam and Shaw
 - Suzen





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 The model is based on comparing the local Momentum Thickness Reynolds number with a critical value from empirical expressions

 $Re_{\theta} = Re_{\theta t}$

- In the present form the model handles natural transition, by-pass transition, and separation induced transition
- The model is based on transport equations, and can easily be implemented in general purpose flow solvers



Approach Eⁿ model for natural transition

 The Eⁿ method is based on analyzing the behavior of small disturbances in the boundary layer

$$\psi(\mathbf{y}) = \phi(\mathbf{y}) \exp\left[i(\alpha \mathbf{x} - \omega t)\right]$$

 The disturbances are inserted in the Navier-Stokes equations, and linearized to give the Orr-Sommerfeld equation

$$(U^* - c^*)(\phi^{\prime\prime} - \alpha^2 \phi) - (u^*)^{\prime\prime} \phi = \frac{-i}{\alpha Re_{\theta}}(\phi^{\prime\prime\prime\prime} - 2\alpha^2 \phi^{\prime\prime} + \alpha^4 \phi)$$

- The model is heavily related to BL physics, and not straight forward to implement in general purpose flow solvers.
- In our inhouse code the EllipSys, the Eⁿ model can be used together with a bypass and a bubble criteria.

Approach Flow Solver and test cases

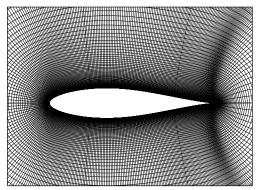


- We use the EllipSys2D incompressible solver.
- Diffusive terms by second order accurate central differences.
- Convective terms by QUICK.
- Steady state computations.
- Turbulence modeling by the $k \omega$ SST model
- Transitional computations using $\gamma Re_{\theta t}$ transition model and E^n model

We will analyze a series of airfoils at Reynolds numbers [3-40] million

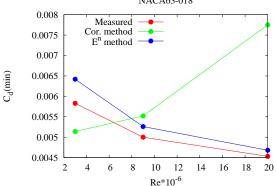
Test Case, NACA63-018 Computational setup

- Airfoil computations for Re=[3, 9, 20] million
- Using two transition models, E^n and γRe_{θ}
- Assuming natural transition (N=9)
- Mesh resolution 384 × 256



Test Case, NACA63-018 Performance for varying Re



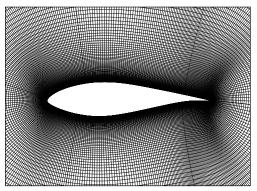


NACA63-018

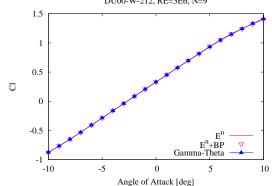
The correlation based model do not respond correctly to varying Re !

Test Case, DU00-W-212 Computational set-up

- Airfoil computations for Re=[3, 15] million
- Using three transition models, E^n , E^n + BP and γRe_{θ}
- All assuming natural transition (N=9)
- Mesh resolution 384 × 256

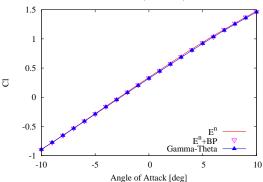


Test Case, DU00-W-212 Lift, Natural Transition



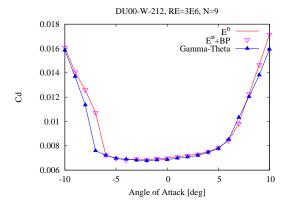
DU00-W-212, RE=3E6, N=9

Test Case, DU00-W-212 Lift, Natural Transition

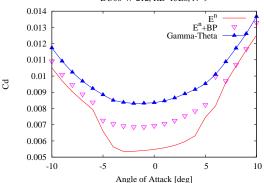


DU00-W-212, RE=15E6, N=9

Test Case, DU00-W-212 Drag, Natural Transition

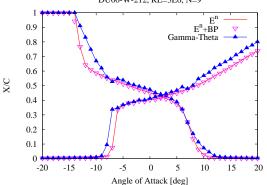


Test Case, DU00-W-212 Drag, Natural Transition



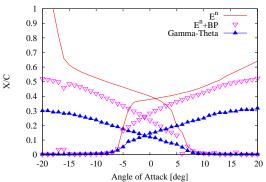
DU00-W-212, RE=15E6, N=9

Test Case, DU00-W-212 Transition Location, Natural Transition



DU00-W-212, RE=3E6, N=9

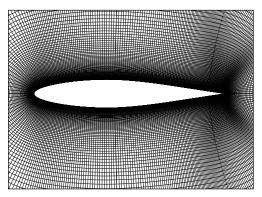
Test Case, DU00-W-212 Transition Location, Natural Transition



DU00-W-212, RE=15E6, N=9

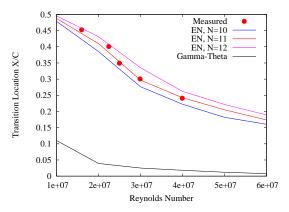
Test Case, NACA64₂A015 Computational setup

- Airfoil computations for Re=[10:40] million, AOA=0 deg.
- Using two transition models, E^n and γRe_{θ}
- Mesh resolution 384 × 256



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Test Case, NACA64₂A015 Performance at high Re



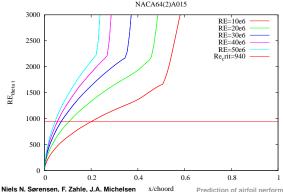


Explanation

Behavior of the correlation based model

The following behavior is observed

- The Reynolds number is varied through the viscosity
- The pressure distribution stays nearly constant
- Turbulent quantities are unchanged away from the airfoil
- The critical Reynolds number predicted by the γRe_{θ} model stays constant





Conclusion Conclusion and outlook

- Wind turbine rotors will face high Re with increasing size
- Lift is weakly dependent on the transition location in normal operation even at high Re
- The available data show that the γRe_{θ} model over-predict drag at high Re
- The present computations indicate that the γ Re_θ model do not react correctly to changes in Re
- There is very little data available for comparison
- The present study suggest to use the Eⁿ model to correctly capture effects of the Re

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