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Publication date: 2014

Document Version Publisher's PDF, also known as Version of record

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*Citation (APA):* Sørensen, N. N. (Author), Zahle, F. (Author), & Michelsen, J. (Author). (2014). Prediction of airfoil performance at high Reynolds numbers.. Sound/Visual production (digital)

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# Prediction of airfoil performance at high Reynolds numbers EFMC 2014, Copenhagen 17-20 Sept 2014

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#### Introduction Large Scale Wind Turbines

Increasing the rotor size may potentially lead to two obvious aerodynamic issues

- High Mach numbers in the tip region
  - Might be harmful for performance
  - Possible to avoid
- High Reynolds numbers
  - Might be beneficial for performance
  - Hard to avoid



DTU 10 MW Reference Turbine

## Introduction Airfoil performance at high Reynolds Numbers



We expect that increasing the Reynolds Number will:

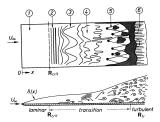
- Decrease the viscous effects due to the thinning of the boundary layer
- Promote earlier transition due to increased Reynolds number

Quantification of the effects can be done by:

- Measurements
  - Tunnel measurements are difficult to obtain at high Re and low Mach
  - Openly available data are sparse
- Computations
  - Model performance in this range is unknown

#### Introduction Laminar turbulent transition

- The transition process depend on many parameters
  - Reynolds Number
  - Free stream turbulence level
  - Laminar separation bubbles
  - Cross flow
  - Surface roughness
  - Mass injection
- Typically approaches for transition modeling
  - *e<sup>n</sup>* method (Orr-Sommerfeld eqn.)
  - Empirical correlations
    - Michel
    - Mayle
    - Abu-Ghannam and Shaw
    - Suzen





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 The model is based on comparing the local Momentum Thickness Reynolds number with a critical value from empirical expressions

 $Re_{\theta} = Re_{\theta t}$ 

- In the present form the model handles natural transition, by-pass transition, and separation induced transition
- The model is based on transport equations, and can easily be implemented in general purpose flow solvers



#### Approach E<sup>n</sup> model for natural transition

 The E<sup>n</sup> method is based on analyzing the behavior of small disturbances in the boundary layer

$$\psi(\mathbf{y}) = \phi(\mathbf{y}) \exp\left[i(\alpha \mathbf{x} - \omega t)\right]$$

 The disturbances are inserted in the Navier-Stokes equations, and linearized to give the Orr-Sommerfeld equation

$$(U^* - c^*)(\phi^{\prime\prime} - \alpha^2 \phi) - (u^*)^{\prime\prime} \phi = \frac{-i}{\alpha Re_{\theta}}(\phi^{\prime\prime\prime\prime} - 2\alpha^2 \phi^{\prime\prime} + \alpha^4 \phi)$$

- The model is heavily related to BL physics, and not straight forward to implement in general purpose flow solvers.
- In our inhouse code the EllipSys, the E<sup>n</sup> model can be used together with a bypass and a bubble criteria.

### Approach Flow Solver and test cases

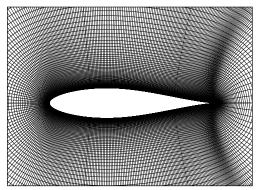


- We use the EllipSys2D incompressible solver.
- Diffusive terms by second order accurate central differences.
- Convective terms by QUICK.
- Steady state computations.
- Turbulence modeling by the  $k \omega$  SST model
- Transitional computations using  $\gamma Re_{\theta t}$  transition model and  $E^n$  model

We will analyze a series of airfoils at Reynolds numbers [3-40] million

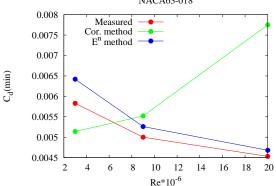
#### Test Case, NACA63-018 Computational setup

- Airfoil computations for Re=[3, 9, 20] million
- Using two transition models,  $E^n$  and  $\gamma Re_{\theta}$
- Assuming natural transition (N=9)
- Mesh resolution 384 × 256



#### Test Case, NACA63-018 Performance for varying Re



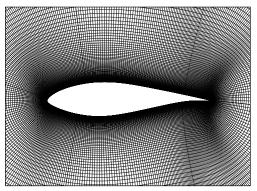


NACA63-018

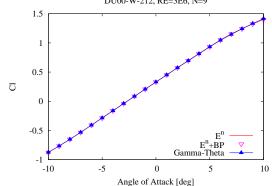
The correlation based model do not respond correctly to varying Re !

#### Test Case, DU00-W-212 Computational set-up

- Airfoil computations for Re=[3, 15] million
- Using three transition models,  $E^n$ ,  $E^n$  + BP and  $\gamma Re_{\theta}$
- All assuming natural transition (N=9)
- Mesh resolution 384 × 256

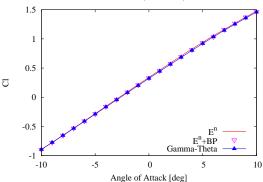


#### Test Case, DU00-W-212 Lift, Natural Transition



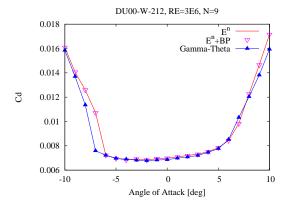
DU00-W-212, RE=3E6, N=9

#### Test Case, DU00-W-212 Lift, Natural Transition

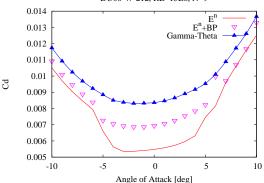


DU00-W-212, RE=15E6, N=9

#### Test Case, DU00-W-212 Drag, Natural Transition

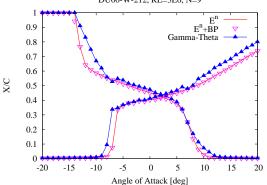


#### Test Case, DU00-W-212 Drag, Natural Transition



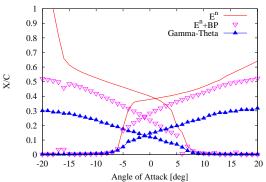
DU00-W-212, RE=15E6, N=9

#### Test Case, DU00-W-212 Transition Location, Natural Transition



DU00-W-212, RE=3E6, N=9

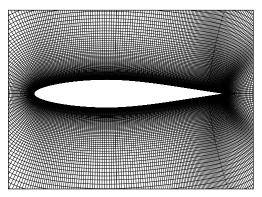
#### Test Case, DU00-W-212 Transition Location, Natural Transition



DU00-W-212, RE=15E6, N=9

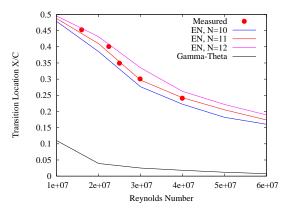
#### Test Case, NACA64<sub>2</sub>A015 Computational setup

- Airfoil computations for Re=[10:40] million, AOA=0 deg.
- Using two transition models,  $E^n$  and  $\gamma Re_{\theta}$
- Mesh resolution 384 × 256



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#### Test Case, NACA64<sub>2</sub>A015 Performance at high Re



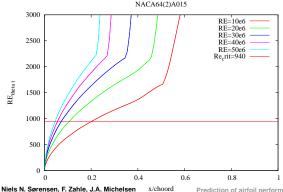


# **Explanation**

# Behavior of the correlation based model

The following behavior is observed

- The Reynolds number is varied through the viscosity
- The pressure distribution stays nearly constant
- Turbulent quantities are unchanged away from the airfoil
- The critical Reynolds number predicted by the  $\gamma Re_{\theta}$  model stays constant





#### Conclusion Conclusion and outlook

- Wind turbine rotors will face high Re with increasing size
- Lift is weakly dependent on the transition location in normal operation even at high Re
- The available data show that the  $\gamma Re_{\theta}$  model over-predict drag at high Re
- The present computations indicate that the γ Re<sub>θ</sub> model do not react correctly to changes in Re
- There is very little data available for comparison
- The present study suggest to use the E<sup>n</sup> model to correctly capture effects of the Re

The present work was supported by the InnWind, AVATAR and COMFLOW projects.