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Modification of poly(styrene-block-butadiene-block-styrene) [SBS] with phosphorus containing fire retardants

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Keywords

Poly(styrene-block-butadiene-block-styrene) [SBS] copolymer, 9,10-dihydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO), fire retardant, thermoplastic elastic additive, epoxidation, cone calorimetry
Abstract

An elaborate survey of the chemical modification methods for endowing highly flammable SBS with increased fire resistant properties by means of chemical modification of the polymer backbone with phosphorus containing fire retardant species is presented. Optimal conditions for free radical addition of the P-H containing fire retardants to a double bonds of poly(butadiene) block of SBS were found, affording varied degree of the modification (0.2-21 mol%). Alternatively, a two-step procedure based on an epoxidation step followed by hydrolysis of the epoxides with phosphoric acid was developed resulting in 20 mol% of poly(butadiene) block modification. Based on TGA results, organophosphorus-modified SBS was found to be amenable to charring – a property which correlated directly with the reduced flammability of the modified polymer observed in Cone Calorimetry tests. Furthermore, conceptually novel application of the H₃PO₄ modified SBS as a fire retardant additive for bitumen material, in combination with synergetic melamine species, offered 25 % better self-extinguishing properties of such formulation already at a low loading level of the fire retardant components (3.5 wt.%).

Introduction

The range of applications of thermoplastic elastomer poly(styrene-block-butadiene-block-styrene) [SBS] includes its usage as an additive to materials where elasticity and strength is to be preserved at temperatures well below zero. The formation of physical cross-links or anchor points by glassy poly(styrene) domains in the matrix where SBS is dispersed while maintaining the overall flexibility rendered by rubbery poly(butadiene) chains accounts for the wide use of SBS as an additive to bitumen, footwear, car tires and other compatible materials.¹⁻³

The inherent disadvantage of SBS, namely its flammability, could be overcome by using supplementary fire retardants added to the polymer matrix, such as aluminium hydroxide, magnesium hydroxide, colemanite, antimony oxide etc. However, high loadings (> 30 wt.%) of the
filler are needed to impair the flammability of the matrix to a sufficient level which may deleteriously affect the elastic properties of matrix itself.4

Chemical incorporation of phosphorus containing substituents into a polymer backbone has been shown to result in substantial improvement of fire retardation at low loading levels.5,6 For example, phosphorylation of the hydroxyl groups of poly(vinyl alcohol) with H3PO4 increased the char yield and limiting oxygen index (LOI) values for the modified polymer.7 Dialkyl/diaryl phosphates introduced to a poly(1,4-isoprene) backbone also increased the LOI values for the modified rubber.8 In addition, synthesized polyethers with chemically bound 10-dihydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO) derivatives were capable of scavenging reactive radicals from a fire and successfully prevent combustion.9 Somewhat relevant work was realized by Fu et al. with respect to the hydrosilylation reaction of SBS with polyhedral oligomeric silsesquioxane (POSS).10 POSS-modified SBS can be thought of as a potential fire resistant material because of high thermal stability and protective properties of the silica shell formed from silsesquioxanes upon their decomposition.11

In the present work the possibility of SBS modification with DOPO and H3PO4 fire retardants is elucidated for the first time. The approach was realized by one step free radical addition of P-H bonds of DOPO to the double bonds of the poly(butadiene) block (PBD) in the SBS as well as by two step addition of H3PO4 to beforehand epoxidized SBS.

Materials and Methods

All chemicals were purchased from Sigma-Aldrich unless otherwise stated. Tetrahydrofuran (99.9%), toluene (99.9%), water (Milli-Q, 18 MΩcm) were used as solvents. 9,10-Dihydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO, >97%) was supplied by TCI America. Dimethyl phosphite (DMPP, 98%), triphenylphosphine (≥95.0%), lithium (granular, 99%), tert-butyllithium (1.7 M in pentane), iodine monobromide (IBr, 98%), 3-chloroperbenzoic acid (MCPBA, ≤77%)
were used as received. Diphenylphosphine (DPP) was synthesized by reacting triphenylphosphine with lithium according to the literature described procedure \(^{12,13}\) and lithium diphenylphosphanide (DPP-Li) was obtained by titrating DPP solution in THF with tert-butyllithium at 0 °C affording a dark red colored solution. Dicumyl peroxide (DCP), benzoyl peroxide (BPO, 75%), lauroyl peroxide (LPO) and 2,2'-azobisisobutyronitrile (AIBN) were used as free radical initiators. Poly(styrene-block-butadiene-block-styrene) [SBS] with 19 mol% (32 wt.%) of styrene, commercially known as Calprene ® 411, was supplied by Icopal A/S.

**Gel Permeation Chromatography (GPC).** The molecular weight was determined using THF as an eluent (at 0.5 ml/min low rate) with a column set consisting of a 5 µm precolumn and two 300 × 8 mm columns (PLgel Mixed C and Mixed D). The system was equipped with a triple detector system (a combined Viscotek model 200 differential diffractive index (DRI) and differential viscosity detector plus a Viscotek model LD 600 right angle laser light scattering detector (RALLS)). Prior to the SEC analysis all samples were filtered on 0.45 µm PTFE filter as 1 mg/ml solutions. 1,3,5-trimethyl-2, 4,6-tris (3,5-di-t-butyl-4-hydroxybenzyl) benzene (Irganox 1330,775 g/mol) was used as an internal calibration standard.

**Free radical addition of P-H to SBS (R1).** In a typical experiment 5.0 g SBS (63 mmol olefinic units) and 42.4 g DOPO (190 mmol, 3x excess relative to olefinic units) was dissolved in 150 ml of toluene (deoxygenated by three freeze-pump-thaw cycles) by heating to 115 °C under argon. Then, 0.197 g (0.73 mmol) of DCP dissolved in 15 ml deoxygenated toluene was added under argon. The reaction continued for 3 h and the product was precipitated into 1 L of methanol followed by reprecipitation from chloroform to methanol. The modified polymer was dried for 16 h at 50 °C under vacuum (1e-2 mbar) affording 5.1 g of the product with the degree of poly(butadiene) block (PBD) modification equal to 3 mol%, yield 95%. \(^1\)H NMR spectra of DOPO modified SBS samples
with the degree of modification ranging from 0.2 to 21 mol% are collected in the Supporting Information (SI1).

**Halogenation of SBS with IBr followed by reaction with lithium diphenylphosphanide DPP-Li (R2, R3).** First, to a solution of 2.5 g SBS (32 mmol olefinic) in 75 ml THF 6 g of IBr (28 mmol) in 20 ml THF was added dropwise in the dark at 0 °C. The product was precipitated in acetone and stored at -17 °C for further use. Second, 1.2 g of halogenated SBS was dissolved in 20 mL of dry THF and then 15 ml of ca. 1.5 M solution of DPP-Li was added at 0 °C. The temperature was allowed to rise to 25 °C and the reaction was terminated after 3 h by precipitation into aqueous methanol. NMR spectra of the halogenated SBS and its adduct with DPP-Li are collected in the Supporting Information, SI2.

**Epoxidation of SBS (R4).** The epoxidation of SBS was realized by adding the solution of 3 g (13 mmol) MCPBA in chloroform to a solution of 2.5 g (32 mmol olefinic) SBS in 75 ml chloroform at 0 °C (Scheme 1). The reaction was allowed to proceed for 16 h allowing the temperature gradually to rise from 0 to 25 °C. The resulting polymer was precipitated into methanol and reprecipitated from CHCl₃ to methanol in order to remove 3-chlorobenzoic acid. The targeted degree of PBD block epoxidation was 41 mol%, whereas the experimentally achieved epoxidation level was 21 mol%, as estimated from NMR (Supporting Information, SI3). Hence, the efficiency of MCPBA was 51 mol%.

**Ring opening of the epoxidized SBS with phosphoric acid (R7).** 60 g of SBS with the degree of epoxidation of PBD block equal to 21 mol% was dissolved in THF (1500 ml) and 10 ml of 6M H₃PO₄ (ca. 10x excess relative to epoxy) was added dropwise at room temperature. The resulting homogeneous mixture was refluxed at 80 °C for 16 h under nitrogen and the product was precipitated into excess of water followed by vacuum drying at 50 °C for another 16 h. The product shows a major peak at -0.66 ppm in ³¹P NMR as well as characteristic phosphoryl P=O (1200 cm⁻¹)
and P-OH (1040-910 cm\(^{-1}\)) absorbance in ATR FT-IR (Supporting Information, SI4). The sample is further abbreviated as E1.

**Scheme 1.** The synthesis routes for modification of SBS with phosphorus containing species.

**Cone calorimetry.** The cone calorimetry experiments were performed according to ISO 5660, 2002: Reaction-to-fire tests – heat release, smoke production and mass loss rate using Mass Loss Cone (Fire Testing Technology, UK). Polymer plaques (5 x 100 x 100 mm) were prepared by solvent casting of the concentrated polymer solutions in THF, followed by consequent drying under nitrogen at 60 °C for 1 day, at 80 °C for 1 day and finally at 2e-3 mbar (22 °C) for 2 days. The optimal conditions for making the pallets with uniform thickness were found by trial and error.

**Flammability tests for bitumen mixtures.** In a typical experiment, 51 g of the H\(_3\)PO\(_4\) modified SBS (Sample E1) was added into a mixture of bitumen (353 g) and chalk (343 g) along with equimolar relative to phosphoric acid monoester quantity of melamine (15 g). The melamine was used as a synergetic additive that formed ionic poly(melamine phosphate) species \textit{in-situ} during the mixing process. A homogeneous mix was obtained after mechanical stirring for 20 min at 200 °C.
Furthermore, thin plaques (5 x 5 x 0.2 cm) of the bitumen modified in such way were prepared from a hot melt in order to test the flammability of the mixtures. The flammability behavior was assessed by either irradiating the plaque of bitumen located on the steel dish from the top using Epiradiator or by heating the sample from the bottom with a butane flame until the bitumen caught fire.

Results and discussion

**Free radical addition of P-H to SBS.** The addition of modifiers with P-H bonds prone to homolytic cleavage toward the olefinic units of SBS was realized using four types of free radical initiators, namely DCP, BPO, LPO and AIBN (Scheme 1, R1). The kinetics of DOPO addition was studied first using DCP only at 115 °C. From the data in Table 1 and Figure 1 it is inferred that at high concentration of DCP (10 mM) gelation of the reaction medium took place soon after the addition of initiator. The resulting degree of poly(butadiene) block (PBD) modification was as low as 1.8 mol% and the molecular weight distribution became 3 times broader compared to unmodified SBS (Sample A2). The broadening of the molecular weight distribution (Figure 2) was attributed to the occurrence of cross-linking side-reactions via recombination of two radicals centered on polymer backbone which eventually led to the formation of a gel. It is thus reasonable to assume that by decreasing the initial concentration of DCP it will be possible to decrease the steady-state concentration of the radicals in the system and thereby diminish the rate of the biradical recombination reaction. Indeed, a decrease in the concentration of DCP from 10 to 5 mM delayed the time of gelation from one to three hours and increased the degree of PBD modification from 1.8 to 3 mol% (Sample A8). Furthermore, at 1 mM of DCP the gelation was completely prevented even for prolonged reaction times (20 h). Hence, by varying the steady state concentration of free radicals in the reaction medium it was possible to control/prevent the onset of gelation as well as to
achieve maximum, under these conditions, PBD block modification efficiency equal to 5.5 mol\% (Sample A9).

In most cases, three times excess (1.2/0.4) of the modifier relative to olefinic units of SBS was used to ensure that the hydrogen abstraction from the modifier dominated over direct binding of the radicals from free radical initiator to the double bonds of SBS. From Table 1 it follows that lowering the ratio of modifier/double bonds to 1.5 (sample A10) leads to a decrease in the binding efficiency of DOPO to SBS at all otherwise equal conditions.

Stepwise addition of initiator was also attempted in order to overcome the gelation in the system at high concentration of free radical initiator. First, the free radical addition of DOPO was realized using 1 mM of BPO initiator resulting in expectable low percentage of modification, i.e., 3.5 mol\% (Sample A11). After the completion of BPO decomposition (20 h), a fresh portion of initiator was added to the same reaction mixture so that its new concentration in the system was 10 mM (sample A12). After 20 h the gelation of the polymer did not take place, because the concentration of double bonds prone to cross-linking had diminished after the first step of the free radical addition. At last,
the procedure was repeated for the third time by modifying the remaining double bonds at 20 mM of BPO (sample A13). That approach afforded the highest percent of the PBD block modification reported in the present work, that is, 21 mol%.

Table 1. Reaction conditions for modification of SBS with organophosphorus compounds.\(^a\)

<table>
<thead>
<tr>
<th>No</th>
<th>P-H type</th>
<th>[P-H], M</th>
<th>[In], mM</th>
<th>T, °C</th>
<th>t, h</th>
<th>Modification, mol%</th>
<th>Mn, kDa</th>
<th>PDI</th>
</tr>
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<tr>
<td>SBS</td>
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<td>0</td>
<td>0</td>
<td>-</td>
<td>0</td>
<td>0</td>
<td>258</td>
<td>1.2</td>
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<tr>
<td>A1</td>
<td>DOPO</td>
<td>1.2</td>
<td>10 (DCP)</td>
<td>115</td>
<td>0.5</td>
<td>0.8</td>
<td>136</td>
<td>2.2</td>
</tr>
<tr>
<td>A2</td>
<td>DOPO</td>
<td>1.2</td>
<td>10 (DCP)</td>
<td>115</td>
<td>1.0</td>
<td>1.8</td>
<td>134</td>
<td>3.1</td>
</tr>
<tr>
<td>A3</td>
<td>DOPO</td>
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<td>5 (DCP)</td>
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<td>0.3</td>
<td>0.2</td>
<td>178</td>
<td>1.6</td>
</tr>
<tr>
<td>A4</td>
<td>DOPO</td>
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<td>5 (DCP)</td>
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<td>0.7</td>
<td>0.5</td>
<td>190</td>
<td>1.8</td>
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<tr>
<td>A5</td>
<td>DOPO</td>
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<td>5 (DCP)</td>
<td>115</td>
<td>1.0</td>
<td>0.8</td>
<td>187</td>
<td>2.2</td>
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<tr>
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<td>5 (DCP)</td>
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<td>1.3</td>
<td>150</td>
<td>2.7</td>
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<tr>
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<td>5 (DCP)</td>
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<td>1.8</td>
<td>146</td>
<td>2.7</td>
</tr>
<tr>
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<td>5 (DCP)</td>
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<td>3.0</td>
<td>108</td>
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<tr>
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<td>1 (DCP)</td>
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<td>20</td>
<td>5.5</td>
<td>36</td>
<td>1.5</td>
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<td>A10</td>
<td>DOPO</td>
<td>0.6</td>
<td>1 (DCP)</td>
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<td>20</td>
<td>3.6</td>
<td>78</td>
<td>2.6</td>
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<tr>
<td>A11^b</td>
<td>DOPO</td>
<td>1.2</td>
<td>1 (BPO)</td>
<td>70</td>
<td>20</td>
<td>3.5</td>
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<td>-</td>
</tr>
<tr>
<td>A12^b</td>
<td>DOPO</td>
<td>1.2</td>
<td>10 (BPO)</td>
<td>70</td>
<td>20</td>
<td>5.0</td>
<td>-</td>
<td>-</td>
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<tr>
<td>A13^b,^c</td>
<td>DOPO</td>
<td>1.2</td>
<td>20 (BPO)</td>
<td>70</td>
<td>20</td>
<td>21</td>
<td>-</td>
<td>-</td>
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<tr>
<td>B1</td>
<td>DMPP</td>
<td>1.2</td>
<td>1 (DCP)</td>
<td>115</td>
<td>20</td>
<td>0.5</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>B2</td>
<td>DMPP</td>
<td>1.2</td>
<td>10 (DCP)</td>
<td>115</td>
<td>20</td>
<td>0.6</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>C1</td>
<td>DPP</td>
<td>1.2</td>
<td>10 (DCP)</td>
<td>115</td>
<td>16</td>
<td>0.6</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>C2</td>
<td>DPP</td>
<td>1.2</td>
<td>10 (LPO)</td>
<td>80</td>
<td>16</td>
<td>0.6</td>
<td>55</td>
<td>2.4</td>
</tr>
<tr>
<td>C3</td>
<td>DPP</td>
<td>2.4</td>
<td>20 (LPO)</td>
<td>80</td>
<td>16</td>
<td>1.0</td>
<td>56</td>
<td>2.8</td>
</tr>
<tr>
<td>C4</td>
<td>DPP</td>
<td>0.9</td>
<td>10 (AIBN)</td>
<td>80</td>
<td>3</td>
<td>1.0</td>
<td>44</td>
<td>2.2</td>
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<tr>
<td>C5</td>
<td>DPP</td>
<td>0.9</td>
<td>30 (AIBN)</td>
<td>80</td>
<td>3</td>
<td>1.1</td>
<td>36</td>
<td>1.9</td>
</tr>
</tbody>
</table>

\(^a\)Concentration of the olefinic fragments from SBS was fixed to 0.4 M for all cases.
\(^b\)Stepwise addition of BPO: first amount of BPO corresponding to its 1mM concentration was added, after 20 h at 70 °C another portion of BPO corresponding to its 10 mM concentration was added and finally after additional 20 h at 70 °C the last portion of BPO was added yielding 20 mM concentration of the peroxide in the reaction medium.
\(^c\)The molecular weight could not be reliably determined due to sorption of the polymer on SEC column.

As for DMPP and DPP free radical addition to double bonds, the modification efficiency was found to be low for both reagents (0.5-1.1%). The higher acidity of DMPP and hence its lower tendency for the homolytic P-H cleavage compared to DOPO (pK\(_a\) of DMPP and DOPO are ca. 20 and 21, respectively)\(^17\) may account for only 0.6 % of the PBD modification with DMPP (Sample B2). On the contrary, the low polarity of P-H in the case of DPP favors the hydrogen abstraction by
the free radical initiator, however, the resulting P centered radicals appear to be unreactive toward
double bonds presumably due to the resonance stabilization by phenyl substituents of DPP. Also,
Attempts to vary the type and concentration of free radical initiator only led to 1.1 mol% of
modification.

Anionic addition of DPP-Li to halogenated SBS. SBS copolymer was subjected to a pre-
modification step with IBr (Scheme 1, R2) in order to introduce good living groups (I⁻ and Br⁻)
using the conditions described by Ceaușescu et al.14 The resulting halogenated product contained
around 76% of PBD-IBr and 24% of unreacted PBD double bonds as estimated by NMR
(Supporting Information, SI2). The targeted degree of PBD modification was 90%, so the efficiency
of IBr reagent was estimated to be 85%. The halogenated product was further subjected to
nucleophilic substitution reaction with lithium diphenylphosphane (DPP-Li) in the conditions
specified in Table 2 (see also Scheme 1, R3). This procedure resulted in 6.8 mol% of the DPP-Li addition to the PBD. Apart from addition of the DPP-Li, deleterious chain scission reaction took place as evidenced from the decrease in molecular weight of the modified SBS (Sample D1, Table 2).

Table 2. Ionic addition of the DPP-Li to halogenated SBS.

<table>
<thead>
<tr>
<th>No</th>
<th>P-H type</th>
<th>[P-H], M</th>
<th>[In], mM</th>
<th>T, °C</th>
<th>t, h</th>
<th>Modification, %</th>
<th>Mn, kDa</th>
<th>PDI</th>
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<td>SBS</td>
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<td>-</td>
<td>0</td>
<td>0</td>
<td>258</td>
<td>1.2</td>
</tr>
<tr>
<td>D1</td>
<td>DPP-Li</td>
<td>0.9</td>
<td>0</td>
<td>0→25</td>
<td>16</td>
<td>6.8</td>
<td>15</td>
<td>1.4</td>
</tr>
<tr>
<td>D2</td>
<td>DPP-Li</td>
<td>0.9</td>
<td>0</td>
<td>0→50</td>
<td>16</td>
<td>5.8</td>
<td>-</td>
<td>-</td>
</tr>
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</table>

Epoxidation of SBS followed by ring opening with P-containing reagents. Epoxidized SBS (SBS-epoxy) was used as a precursor for further immobilization of the P-containing reagents via ring opening addition to the epoxides (Scheme 1, R4). The epoxidation reaction itself was found primarily to affect 1,4 PBD chains due to 5 times lower activation energy for the epoxidation of 1,4-cis double bonds of PBD compared to the epoxidation of 1,2-vinyl fragments of PBD. Thus, the epoxidized PBD block of SBS mainly contained 1,2-substituted epoxides (Supporting Information, SI3).

First, a direct reaction of SBS-epoxy with DOPO and DMPP was attempted in butanone at 90 °C (R5) in accordance with the procedure described by Liu et al. which resulted in less than 1% degree of modification due to the low acidity of the P-H bonds (pKₐ of DOPO and DMPP are ca. 21 and 20 respectively). An even higher temperature was suggested in the literature (160 °C) for analogous reaction between DOPO and monosubstituted epoxides in solvent free conditions, however, it was not tried in the present work due to the following reason: at elevated temperatures C-Si bond in the polymer backbone (originating from dichlorodimethylsilane linker used for SBS synthesis) may undergo homolytic cleavage thereby destroying the block copolymer structure itself.
Using acids stronger than DOPO and DMPP, such as p-toluenesulfonic acid in chloroform ($pK_a = -2.8$) and hydrochloric acid in THF ($pK_a = -7$) resulted in quantitative conversion of the epoxides to the corresponding addition products in mild conditions (R6).\textsuperscript{15} Hence, phosphoric acid ($pK_{a1} = 2.1$) was deduced to be a suitable candidate for the role of phosphorus containing modifier (R7). Heating the THF solution of the SBS-epoxy (degree of epoxidation = 21 mol\%) with equimolar relative to epoxy groups amount of 1 M H\(_3\)PO\(_4\) to 50 °C did not significantly change the epoxy content in the polymer. However, an increase in the temperature (80 °C), reaction time (16 h) and concentration of H\(_3\)PO\(_4\) (6 M) led to complete conversion of epoxides to the corresponding monoalkyl esters of phosphoric acid (Supporting Information, SI4).\textsuperscript{21} Even though the modified product could easily be dissolved in THF, analysis of the molecular weight by SEC was challenging due to irreversible adsorption of the hydrophilic-hydrophobic product onto the stationary phase [poly(styrene-divinylbenzene)] of the chromatography column. The sample denoting SBS modified with H\(_3\)PO\(_4\) is further abbreviated as E1.

The direct reaction of SBS-epoxy with 10-chloro-9-hydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO-Cl) obtained by oxidation of DOPO with trichloroisocyanuric acid was also performed (R8).\textsuperscript{22} The total percent of the PBD modification was 0.1%. In spite of the fact that monosubstituted epoxides are known to react with chlorophosphates with ease,\textsuperscript{23} ring opening of 1,2-disubstituted epoxides was shown to be not feasible even when catalyzed by Lewis acids.\textsuperscript{24} This fact in combination with preferred epoxidation of 1,4 over 1,2 chains\textsuperscript{18} of the PBD may account for the low degree of ring opening of the epoxy groups with DOPO-Cl reagent observed in the present studies.

The alternative route of incorporating DOPO into the polymer backbone encompassing intermediate ring opening of the epoxides with ethanolamine followed by reaction of the incorporated hydroxyl groups with DOPO-Cl with was also pursued (R9). As seen in the previous
cases, the 1,2-substituted epoxides were not reactive toward ethanolamine mainly due to the bulky polymeric substituents which preclude $S_N^2$ type reaction. Even when SBS-epoxy was heated to 110 °C in the presence of large excess of ethanolamine in toluene the level of epoxides conversion was below 1%. Stronger nucleophile such as deprotonated form of DOPO (DOPO-Li) was also unreactive toward 1,2-substituted epoxides (R10).

Hence, 2 out of 10 synthesis routes described above were selected as most viable approaches to covalently introduce the organophosphorus substituents into the SBS structure. Namely, free radical addition of DOPO to SBS which afforded to vary the degree of PBD modification from 0.2 to 21 mol% as well as the two step route encompassing (i) epoxidation followed by (ii) ring opening of the epoxides with phosphoric acid. The latter approach was utilized to incorporate only fixed amount of the monoalkyl ester of phosphoric into the PBD backbone predetermined by the epoxidation step, that is, 20 mol%.

**TGA of the modified SBS copolymers.** Thermal degradation behavior of unmodified SBS as well as DOPO and H$_3$PO$_4$ modified polymer was studied by TGA in air. The onset decomposition temperatures corresponding to the weight loss of 5% ($T_{5\%}$) and 10% ($T_{10\%}$) are summarized in Table 3. Also, from differential thermogravimetric curves (Supporting Information, SI5) the temperatures at which the decomposition rate acquires its local maximum ($T_{\max 1}$, $T_{\max 2}$, $T_{\max 3}$) were determined (Table 3).

Unmodified SBS starts to degrade already at 350 °C as can be seen from the decomposition temperature corresponding to the 5% of the weight loss, $T_{5\%}$. Thermal degradation rate reaches its first local maximum at $T_{\max 1} = 365$ °C which signifies the degradation step of poly(styrene) blocks in SBS.$^{25,26}$ Taking into account the ceiling temperature of styrene monomer (395 °C) $^{27}$, it is evident that both depolymerization and oxidative destruction of the poly(styrene) commences at this stage. Also, at 300-420 °C, i.e., when the slope of the TGA curve is steady, the weight loss is 30
wt.% which correlates well with the weight fraction of poly(styrene) blocks in SBS (32 wt.%). The second degradation step at $T_{\text{max}2} = 435$ °C probably corresponds to the depolymerization/oxidative destruction of poly(butadiene) block as inferred from the ceiling temperature of 1,3 butadiene equal to 585 °C. At last, thermal destruction of the harshly oxidized and cross-linked polymer residue takes place at $T_{\text{max}3} = 476$ °C.

Figure 3. TGA of DOPO and H$_3$PO$_4$ modified SBS (A) at low (0.2-5.5%) and (B) high (20-21%) degree of modification of PBD block (in air, 10 °C/min).

Thermal stability of DOPO modified SBS samples (A3, A5, A7, A8, A9) with low degree of PBD block modification (0.2, 0.8, 1.8, 3.0, 5.5 % respectively) was found to be higher compared to that of unmodified SBS (Figure 2A). In particular, the decomposition temperatures corresponding to the weight loss of 5% ($T_{5\%}$) and 10% ($T_{10\%}$) are 50 °C higher for DOPO modified SBS (Table 3, sample A9) relative to its unmodified analog.

Such behavior is attributed to the effect of bulky DOPO substituents present in the main chain of modified SBS that hinder the relaxation processes and thereby increase the activation energy for the homolytic cleavage of the C-C bonds in the polymer backbone.
Table 3. TGA parameters for SBS modified with DOPO and H₃PO₄ residuals.

<table>
<thead>
<tr>
<th>Sample</th>
<th>PBD modification (%)</th>
<th>T₁0% (°C)</th>
<th>T₁0% (°C)</th>
<th>T₁0% max1 (°C)</th>
<th>T₁0% max2 (°C)</th>
<th>T₁0% max3 (°C)</th>
<th>Residue at 550°C (wt.%)</th>
<th>Residue at 800°C (wt.%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>SBS</td>
<td>0</td>
<td>350</td>
<td>365</td>
<td>365</td>
<td>435</td>
<td>476</td>
<td>1.5</td>
<td>1.4</td>
</tr>
<tr>
<td>A9</td>
<td>5.5</td>
<td>398</td>
<td>416</td>
<td>466</td>
<td>602</td>
<td>-</td>
<td>8.0</td>
<td>1.3</td>
</tr>
<tr>
<td>A13ᵃ</td>
<td>21</td>
<td>259</td>
<td>405</td>
<td>446</td>
<td>552</td>
<td>729</td>
<td>24.9</td>
<td>5.9</td>
</tr>
<tr>
<td>E1ᵇ</td>
<td>20</td>
<td>200</td>
<td>225</td>
<td>434</td>
<td>492</td>
<td>655</td>
<td>23.8</td>
<td>5.5</td>
</tr>
</tbody>
</table>

ᵃAdditional minor T₁0% max4 = 148 °C was identified.ᵇAdditional minor T₁0% max4 = 140 °C and T₁0% max5 = 220 °C were identified.

At high loadings of the fire retardant, 4 and 5 stage decomposition occurs for DOPO and H₃PO₄ modified SBS, respectively (samples A13 and E1). The decomposition of A13 the 100-400 °C temperature range results in 9 % mass loss, whereas E1 loses 18 % of its weight, probably due to occurrence of the cross-linking reactions between phosphate groups resulting in evolution of water. Also, evaporation of non-chemically bound water of hydration emanating from phosphate groups may lead to twice higher mass loss at 100-400 °C for sample E1. Similarly, polar phosphoryl groups (P=O) in the polymer sample A13 tend to be solvated by toluene and water and therefore retain these minor solvent components even after extensive vacuum drying at 50 °C. After heating to 100 °C non-chemically bound impurities evaporate giving rise to the onset of weight loss at 100 °C.

At higher temperatures, oxidative decomposition of poly(styrene) and poly(butadiene) blocks primarily accounts for further weight loss. In the case of unmodified SBS, the decomposition process is complete at 550 °C and only 1.5 % of the initial weight remains. However, for phosphorus containing samples the decomposition process is competing with a so-called charring process which entails condensation reactions and formation of aromatic residue (char). The charring affords preservation of a significant fraction of material (25 and 24 % for samples A13 and E1 respectively) at 550 °C that would otherwise be oxidized to volatile products.
As shown in the literature, phosphorus containing substituents covalently incorporated into the polymer structure are capable to act as char promoting agents at elevated temperatures.\textsuperscript{28} Their mechanism of action implies the release of poly(phosphoric) acid which subsequently phosphorylates and dehydrates the organic material affording compact char.\textsuperscript{29-31} It is the barrier properties of the char that endow a material with higher thermal stability and resistivity to further combustion in the condensed state.

**Cone calorimetry studies of the modified SBS.** Unmodified SBS and H\textsubscript{3}PO\textsubscript{4} modified SBS (sample E1) were tested under a heat flux from a cone heater providing a radiation exposure of 35 kW/m\textsuperscript{2}. The heat release rate (HRR) curve in Figure 4 shows that these specimens behave as thermally thick by having a secondary peak after the initial increase, and a plateau is reached before the backside of the samples are heated and starts to pyrolyse.\textsuperscript{32} The E1 decreased the peak heat release rate (PHRR) by as much as 60 % and the initial growth by 28 % with respect to unmodified SBS. The average heat release rate (AHRR) taken over the plateau from 60 to 120 seconds was 405 kW/m\textsuperscript{2} for E1 whereas SBS released on average 565 kW/m\textsuperscript{2} over the same period.

![Figure 4. Heat release rate curves for unmodified and H\textsubscript{3}PO\textsubscript{4} modified SBS exposed to 35 kW/m\textsuperscript{2}](image)
A summary of the most important parameters characterizing the flammability of SBS and E1 are collected in Table 4. The flaming duration of the specimens were comparable, but the total energy released during this period was 196 MJ/m² and 96 MJ/m² for SBS and E1, respectively. The SBS specimen was completely consumed, whereas the E1 self-extinguished, leaving 20% of its initial mass in the sample holder (Figure 5). The initial mass loss rate for the first 120 s after ignition was 0.19 g/s and 0.20 g/s for SBS and E1, respectively, and thus almost identical. However, a large percentage of the mass of the samples was lost between 120 s and 180 s where there was a clear difference in the behaviour between the two samples. The SBS had an increasing mass loss rate, and it has lost a significant percentage of its mass in this period, whereas E1 had a decreasing mass loss rate in the same time period. From 180 s to burnout or self-extinguishing the mass loss rates were 0.133 g/s and 0.064 g/s for SBS and E1, respectively, which is more than a factor of 2 difference.

Table 4. Summary of important measured and calculated properties of SBS and E1 (5 x 100 x 100 mm) as a result of an exposure to a heat flux of 35 kW/m²

<table>
<thead>
<tr>
<th>Parameter</th>
<th>SBS</th>
<th>E1</th>
</tr>
</thead>
<tbody>
<tr>
<td>Time to ignition [s]</td>
<td>41</td>
<td>47</td>
</tr>
<tr>
<td>Time to peak heat release [s]</td>
<td>192</td>
<td>177</td>
</tr>
<tr>
<td>PHRR [kW/m2]</td>
<td>1186</td>
<td>473</td>
</tr>
<tr>
<td>AHRR from 60 to 120 s [kW/m²]</td>
<td>565</td>
<td>405</td>
</tr>
<tr>
<td>Mass Loss Rate (MLR) initial [g/s]</td>
<td>0.19</td>
<td>0.202</td>
</tr>
<tr>
<td>MLR final [g/s]</td>
<td>0.133</td>
<td>0.064</td>
</tr>
<tr>
<td>MLR initial [wt%/s]</td>
<td>0.0032</td>
<td>0.0035</td>
</tr>
<tr>
<td>MLR final [wt%/s]</td>
<td>0.0023</td>
<td>0.0011</td>
</tr>
<tr>
<td>Total Heat Release (THR) [MJ]</td>
<td>196</td>
<td>96</td>
</tr>
</tbody>
</table>

The visual difference between the two specimens after the exposure can be seen in the images shown in Figure 5, where it is evident that SBS has burned out and no residue was left whereas E1 created a char layer that prevented complete consumption of the sample.
Bitumen mixtures with modified SBS. The unmodified SBS constitutes the most widely used bitumen additive\textsuperscript{1} known to date, however, high flammability of SBS renders its chemical modification with a fire retardant species advantageous. Since H\textsubscript{3}PO\textsubscript{4} modified SBS (E1) demonstrated a pronounced charring behavior during thermal degradation in air (see TGA and Cone calorimeter results), we anticipate that this property could be beneficial for further development of the fire retarded bitumen materials.

The data on flammability behavior of the pure bitumen and its mixture with modified SBS (E1) show similar average ignition time for both Mix1 and Mix2 while the average self-extinguishing time was reduced by 25% even at low loading of the fire retardant (Table 5). The amount of H\textsubscript{3}PO\textsubscript{4} monoester which corresponds to the total 7 wt.% of the modified SBS with the degree of modification equal to 22 wt.% in the bitumen mixture is translated to 1.5 wt.% (7 x 0.22) of H\textsubscript{3}PO\textsubscript{4} monoester. Importantly, 1.5 wt.% of H\textsubscript{3}PO\textsubscript{4} monoester and 2 wt.% of the melamine correspond to their 1:1 molar ratio. Equimolar amounts of the fire retardant species in Mix2 formulation afforded the formation of the polymeric fire retardant via deprotonation of the acidic phosphoric acid.
residues by the basic melamine species. The resulting melamine phosphate monoester therefore resembles a well-known and efficient fire retardant additive, namely melamine phosphate.\textsuperscript{33}

Table 5. The composition of the bitumen mixtures and their flammability.

<table>
<thead>
<tr>
<th>Sample</th>
<th>Bitumen, wt.%</th>
<th>Chalk, wt.%</th>
<th>SBS, wt.%</th>
<th>SBS-H\textsubscript{3}PO\textsubscript{4}, wt.%</th>
<th>Melamine, wt.%</th>
<th>Av. ignition time, s</th>
<th>Av. self-extinguishing time, s</th>
</tr>
</thead>
<tbody>
<tr>
<td>Mix1</td>
<td>48</td>
<td>45</td>
<td>7</td>
<td>0</td>
<td>0</td>
<td>22.5</td>
<td>44</td>
</tr>
<tr>
<td>Mix2</td>
<td>46</td>
<td>45</td>
<td>0</td>
<td>7</td>
<td>2</td>
<td>22.0</td>
<td>33</td>
</tr>
</tbody>
</table>

The advantage in using melamine phosphate is exemplified by its dual mechanism of action. At elevated temperatures melamine sublimes and thus cools down the combustion zone while the released phosphoric acid results in phosphorylation and dehydration of the carbon rich material (bitumen) affording formation of carbonaceous char. As mentioned, the char layer opposes further propagation of fire due to its barrier properties.\textsuperscript{5,11,33,34}

The amount of heat produced by the Epiradiator was not sufficient to ignite the samples, therefore the obtained results are semi-quantitative. However, from visual observation, the formation of bubbles (Figure 6) on a sample containing modified SBS indicated that the fire retardant, in addition to charring process, releases gases originating from melamine which dilute the combustion zone, - the phenomena also known as intumescence mechanism of action.

Furthermore, it is beyond the scope of the paper to elucidate whether H\textsubscript{3}PO\textsubscript{4} modified SBS blended with bitumen and chalk alone, i.e., without melamine will impair the flammability of the resulting mixtures. Based on the pronounced fire retardant properties of H\textsubscript{3}PO\textsubscript{4} modified SBS, as confirmed by cone calorimetry, we can only suppose that an improvement in flammability of the blend containing H\textsubscript{3}PO\textsubscript{4} modified SBS, bitumen and chalk may be observed.
Conclusions

Free radical addition of P-H to poly(butadiene) block of SBS was optimized for DOPO modifier yielding 20 mol% of the poly(butadiene) block modification on the condition that free radical initiator is added stepwise. Large excess of expensive DOPO modifier over the double bonds (3x) was needed to achieve high modification efficiency of poly(butadiene) block, which hindered
further scale up of the procedure. On the contrary, relatively cheap and scalable process consisting of epoxidation of poly(butadiene) block followed by ring opening of the epoxides with phosphoric acid afforded preparation of a substantial quantity of H₃PO₄ modified SBS (200 g), with the degree of modification 21 mol%. Compared to unmodified SBS, H₃PO₄ modified SBS increased the char yield in the 500-800 °C temperature range as well as decreased peak heat release rate by 60 % and final mass loss rates by 52 % evidencing that chemical alterations endowed SBS with enhanced fire resistance. Also, bitumen mixtures containing H₃PO₄ modified SBS and melamine self-extinguished 25% faster even at low loadings of the polymeric retardant (3.5 wt.%).

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References


