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Topology-optimized mode converter in a silicon-on-insulator photonic wire waveguide

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Abstract: A $1.4\ \mu\text{m} \times 3.4\ \mu\text{m}$ fundamental to first order mode converter for the transverse electric polarization was designed using topology optimization. Insertion loss $< 2\ \text{dB}$ (100 nm bandwidth) and extinction ratio $> 9.5\ \text{dB}$.

OCIS codes: (230.3120) Integrated optics devices; (130.1750) Components

1. Introduction

Mode division multiplexing (MDM) is one of the proposed methods for increasing on-chip data capacity in optical communications [1]. Mode converters are components essential to support the processing of MDM signals and several approaches has been taken to realize such devices [1,2].

Topology optimization (TO) is a powerful inverse design tool, that has previously been shown to deliver robust, compact designs for nanophotonic components exhibiting low loss and controllable bandwidth [3].

Here, we experimentally demonstrate a topology-optimized design for a compact, low-loss, and broad-band mode converter converting the transverse electric fundamental even mode (TE_0) to the first higher order odd mode (TE_1).

2. Design and modelling

Previous work in the group has shown that compact mode conversion can be achieved through interferometric designs [4]. Hence, the initial structure for the TO, shown in figure 1(a), was made to reflect previous designs including a splitting region in the center of the structure and a narrow $1.4\ \mu\text{m} \times 3.4\ \mu\text{m}$ design domain. The objective of the TO is to convert a TE_0 mode excited at position A (yellow) to the TE_1 mode at position B (green). This is achieved by iteratively changing the material distribution within the design domain (purple) until the objective is fulfilled. The TO algorithm was developed in house [5] and performs repeated 3D finite-difference time-domain (FDTD) calculations to find the solutions of the state, adjoint equations combined with mathematical programming-based sensitivity analysis, and design updates. The light source used in the TO was a Gaussian pulse with a spectral width of $\sim 280\ \text{nm}$ (full-width half maximum) centered at $\sim 1580\ \text{nm}$. The optimization was done using a mesh with a resolution of $40\ \text{nm}$ and in order to end up with a ‘black and white’ design feasible for fabrication progressive filtering, with a size of $120\ \text{nm}$, was used. The TO was made for a $340\ \text{nm}$ thick silicon slab, $\epsilon_{\text{Si}}=11.68$ and is placed on top of a silica buffer layer with a permittivity of $\epsilon_{\text{silica}}=2.085$ and having air above the structure while the boundary conditions are perfectly matched absorbing layers. The topology-optimized structures were restricted to be uniform in the vertical direction to ensure the feasibility of fabrication. The resulting topology-optimized design is presented in figure 1(b).

Figure 1 (a) The starting point structure for the optimization indicating source position (yellow) objective (green) and design domain (purple). The hole at the center of the structure was included based on knowledge from previous work. (b) The topology optimized design obtained after 200 iterations of optimization.

The performance of the structure was evaluated through simulations of the transmission, mode profile and visualization of the out-of-plane H-field (H_z), all shown in figure 2. The theoretical insertion loss is found to be $< 0.5\ \text{dB}$ for a range of $100\ \text{nm}$ and the design exhibits an extinction ratio of $\sim 14\ \text{dB}$.

3. Experimental results

The design was fabricated in an ~340 nm silicon layer on top of an ~2000 nm thick silica buffer layer. Using a JEOL JBX-9500 electron-beam lithography system the design was defined in a ~110 nm thick layer positive electron beam resist (ZEP520A). The resist was used as a soft mask for inductively coupled plasma reactive ion etching using SF₆ and C₄F₄. Finally SU-8 polymer waveguides were added on inversely tapered silicon in- and out-put waveguides to optimize the coupling of light.

Figure 2 (a) H_z -field simulations for the initial structure (top) and topology optimized structure (bottom). (b) Recorded mode profiles from the range of 1520 nm to 1620 nm. (c) Simulated and measured mode profile 1600 nm. (d) Simulated and measured transmission of a single device, for easier comparison with the theoretical results.

The functionality of the device was experimentally verified by recording the mode profile of the converted signal with an InGaAs infrared camera (Xenics XEVA XC130). The measurements are shown in figure 2(b) along with a line scan across the mode profile, figure 2(c), revealing an extinction ratio of >9.5 dB seemingly limited by the resolution of the setup.

The insertion loss of the design was determined by the measurement of light transmission converted first from TE₀ to TE₁ and then sent through a mirrored structure converting the light back to TE₁ once more. As the device is reversible and characterized in the linear regime, the loss of a single device can be found by halving the values measured as has been done to the data presented in figure 2(d). The insertion loss is found to be < 1 dB for a range of 40 nm and to be < 2 dB for the entire 100 nm range of the laser.

4. Conclusion

Topology optimization was utilized to design a TE₀-TE₁ in a photonic wire waveguide with a compact footprint of 1.4 μm x 3.4 μm . The design was fabricated using e-beam lithography and functionality was experimentally verified. The transmission loss of the device was found to be < 2 dB for a 100 nm bandwidth and an extinction ratio of > 9.5 dB was exhibited.

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