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Fatigue Load Sensitivity Based Optimal Active Power Dispatch For Wind Farms

Haoran Zhao, Qiuwei Wu, Shaojun Huang, Mohammad Shahidehpour, Qinglai Guo and Hongbin Sun

Abstract—This paper proposes an optimal active power dispatch algorithm for wind farms based on Wind Turbine (WT) load sensitivity. The control objectives include tracking power references from the system operator and minimizing fatigue loads experienced by WTs. The sensitivity of WT fatigue loads to power references is defined which simplifies the formulation of the optimal power dispatch problem. Since the sensitivity value is calculated at the local WT controller, the computation burden of the central wind farm controller is largely reduced. Moreover, explicit analytical equations of the fatigue load sensitivity are derived, which significantly improves the computation efficiency of the local WT controller. The proposed algorithm can be implemented in different active power control schemes. Case studies were conducted with a wind farm under balance control for both low and high wind conditions. By comparing the rainflow cycles and Damage Equivalent Load (DEL), the efficacy of the proposed algorithm is verified.

Index Terms—Fatigue load, load sensitivity, optimal active power dispatch, wind farm, wind turbine.

I. INTRODUCTION

NOWADAYS, wind power is the fastest growing Renewable Energy Resource (RES). According to the report of the European Wind Energy Association (EWEA), the newly installed wind power capacity of EU in 2014 is 12.8 GW [1]. By the end of 2015, the cumulative capacity of wind power had reached 141.6 GW, which can meet around 11.4% of Europe’s electricity demand.

With the increasing penetration level, variability and uncertainty of wind power have brought new technical challenges to power system operation [2]–[4]. The technical requirements for wind power integration are more stringent [5]. For the active power, different control requirements are specified, such as balance control, delta limitation, ramp rate limitation, etc. [6]. In other words, a wind farm shall be capable of tracking the power reference from the system operator.

With fast development of power electronics, controllability of modern Wind Turbines (WTs) has been largely improved. When required wind farm power is less than the maximum available power, WTs will limit power production and operate in the derated mode. In order to achieve specific control objectives, it is very important to optimally dispatch power references to individual WTs.

The initial dispatch schemes for wind farms only focus on the power reference tracking. The power reference is proportionally distributed to individual WTs according to either the available power [7] or the actual output power [8]. Fatigue loads (load for short hereinafter) experienced by WTs, which has a significant impact on the lifetime of WTs, are not considered.

In recent studies, several multi-objective dispatch algorithms have been proposed [9]–[18]. The studies of [9]–[11] focus on the multi-objective control at the WT level. On top of providing the desired power production, mechanical loads are minimized by coordinating the pitch angle and electrical torque. For the wind farm level control, as long as the power requirement specified by the system operator is met, loads can be minimized by coordination among WTs [19]. The optimal control problem is either solved in a centralized manner [12]–[14] or a distributed manner [15]–[18]. For the former case, the wind farm model is formulated as a coupled, constrained Multiple Input and Multiple Output (MIMO) system whose order drastically grows with increasing the number of WTs. Since a modern large-scale wind farm may consist of several hundred WTs, the computation burden of the centralized control scheme is quite heavy and it cannot be used for real-time application. For the latter case, the distributed control scheme can efficiently reduce the computation burden. However, in order to guarantee the optimality, the iteration among WTs is required which implies high sampling communication required.

In this paper, a load sensitivity based optimal active power dispatch algorithm is proposed for wind farms to overcome the aforementioned problems. It minimizes WT loads while tracking the wind farm power reference. The proposed approach includes the following two aspects. Firstly, the sensitivity of WT fatigue loads to power references is defined and introduced as the signal exchanged between the central and local controllers. Secondly, explicit expression of the WT load sensitivities are derived.

The main contribution is that the proposed scheme enables efficient implementation of the optimal wind farm control, especially for large-scale wind farms. The proposed scheme is solved in the centralized manner. Compared with the other central optimal wind farm control schemes, the formulation of the optimal dispatch algorithm is simplified. Most of
the computation task is undertaken by the local controller and solved in parallel. The explicit expressions of the load sensitivities can reduce the online computation burden of the local controller. Moreover, the optimal control problem is formulated as a standard Quadratic Programming (QP) problem and can be efficiently solved. Compared with the distributed control scheme, the global optimum of the QP problem can be obtained without additional iterations.

The paper is organized as follows. Section II describes the structure of the wind farm control based on the load sensitivity. The modeling and operation of a power-controlled WT are introduced in Section III and Section IV, respectively. The explicit equations of load sensitivities are derived in Section V. Section VI explains the formulation of the optimal dispatch problem. Case studies are presented and discussed in Section VII, followed by conclusions.

II. LOAD SENSITIVITY BASED WIND FARM CONTROL STRUCTURE

The proposed wind farm control structure is shown in Fig. 1. According to the requirement of the system operator and the available power $P_{\text{wfc}}$, the active power control scheme of the wind farm is decided. The power reference of the wind farm $P_{\text{wfc}}$ is calculated and delivered to the wind farm controller. In the optimal wind farm control schemes of the previous studies, the measurements of individual WTs are sent directly to the local controller. Moreover, the optimal control problem is formulated based on a complicated wind farm model.

![Wind farm control structure](image)

In the proposed wind farm control, the load sensitivity $\frac{\partial L}{\partial P_{\text{wt ref}}} \left[ \left[ P_{\text{wt min}}, P_{\text{wt max}} \right] \right]$ are used for the formulation of the optimal dispatch problem. They are calculated locally and sent to the wind farm controller. The details of calculating $\frac{\partial L}{\partial P_{\text{wt ref}}}$ and constraints $\left[ P_{\text{wt min}}, P_{\text{wt max}} \right]$ are described in Section IV and Section V, respectively. By solving the optimization problem, the power references of individual WTs $P_{\text{wt ref}}$ are updated for each interval of wind farm control. During the control interval, based on $P_{\text{wt ref}}$, a torque reference $T_{\text{wt ref}}$ for the local torque control and a pitch angle reference $\theta_{\text{ref}}$ for the pitch actuator are generated. The control interval of the local controller is smaller.

III. MODELING OF A POWER-CONTROLLED WT

In the wind farm control, the role of individual WTs is an actuator, which operates in a derated condition and tracks $P_{\text{wt ref}}$. The power-controlled WT model developed by National Renewable Energy Laboratory (NREL) is used to represent a variable speed pitch-controlled WT [20], [21]. The model structure is shown in Fig. 2.

![Power-controlled WT model](image)

Normally, the sampling time of the wind farm controller $t_{\text{s}}$ is in seconds [17]. Therefore, the fast dynamics in the generator and pitch actuator can be ignored [12]. Moreover, the oscillations in the shaft torsion and tower nodding are disregarded to reduce the model complexity. In this study, a simplified nonlinear WT model with its local control is introduced in the wind farm control, which is used to calculate the load sensitivities. Its controller and operation are described in Section IV.

A. Aerodynamics

The aerodynamic torque $T_a$ and thrust force $F_t$ are the main sources of nonlinearity [22], calculated by,

$$T_a = \frac{0.5\pi \rho R^2 \nu_t^3 C_p(\lambda, \theta)}{\omega_g},$$

$$F_t = \frac{0.5\pi \rho R^2 \nu_t^2 C_t(\lambda, \theta)},$$

where $C_p$ and $C_t$ are the power coefficient and thrust coefficient, respectively, $\omega$ is the tip speed ratio, defined by $\lambda = \frac{\omega \cdot R}{\nu_t}$.

B. Drive Train

The drive train is considered to be rigidly coupled and the single-mass model is used in this study, where the rotor mass $J_r$ and generator mass $J_g$ are merged into one equivalent mass $J_t$ [23], expressed by,

$$J_t = J_r + \eta_g^2 J_g.$$  

According to the low-shaft motion equation,

$$\dot{\omega}_r = \frac{1}{J_t} (T_a - \eta_r T_g),$$

$$\dot{\omega}_g = \eta_g \omega_r,$$

where $\omega_r$ and $\omega_g$ are the rotor and generator speeds, respectively, and $\eta_r$ is the gear box ratio.
C. Generator

In the torque control loop, the vector control is used to ensure a fast (in milliseconds) and accurate response [24]. Since the dynamic is neglected, the generator torque \( T_g \) is approximately equal to its reference, i.e.,

\[
T_g \approx T_{g\text{,ref}}.
\]

D. Tower

The tower dynamics is not included in the simplified WT model. According to [14], [25], it is assumed the fore-aft bending moment at the tower base \( M_t \) can be approximately derived by,

\[
M_t \approx H \cdot F_t,
\]

where \( H \) indicates the tower height.

IV. OPERATION AND CONTROL OF WT IN A WIND FARM

Conventionally, WTs are controlled to track its Optimal Regimes Characteristic (ORC), as shown in Fig. 3. The polyhedron marked in the figure shows the feasible operation area where the power coefficient \( C_p > 0 \). Define the rated wind speed as \( v_{\text{rated}} \) and the rated power as \( P_{\text{rated}} \). When \( v_w \leq v_{\text{rated}} \), the pitch control is deactivated (\( \theta = 0 \)) and \( T_g \) is regulated to track the optimal rotor speed. The maximum available wind power is extracted (\( P_{\text{ref}} = P_{\text{rated}} \)). When \( v_w > v_{\text{rated}} \), \( T_g \) is kept at its rated value and the pitch control is activated to prevent the generator speed \( \omega_g \) from over-speeding. The captured wind power is limited to the rated value \( P_{\text{ref}} = P_{\text{rated}} \).

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A. Region I

The pitch control is activated. The captured power is controlled by regulating \( \theta_{\text{ref}} \) and \( T_{g\text{,ref}} \). The measured generator speed \( \omega_g \) is filtered by a low-pass filter and the filtered speed \( \omega_f \) is derived by,

\[
\omega_f = \frac{1}{1 + s\tau_1} \omega_g,
\]

where \( \tau_1 \) is the time constant of the filter.

According to the deviation of \( \omega_f \) from its rated value \( \omega_{g\text{,rate}} \), \( \theta_{\text{ref}} \) is obtained by the gain-scheduled PI controller,

\[
\theta_{\text{ref}} = \frac{K_p}{K_c} (\omega_f - \omega_{g\text{,rate}}) + \frac{K_i}{s} \omega_f - \omega_{g\text{,rate}},
\]

where \( K_p \) and \( K_i \) are proportional and integral gains of the PI controller, respectively, and \( K_c \) is the correction factor. In [21], \( K_c \) is a function of \( \theta \), i.e., \( K_c = K_0 + K_0 \theta \), where \( K_0 \) and \( K_0 \) are the constants.

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B. Region II

The pitch control is deactivated, i.e., \( \theta_{\text{ref}} = 0 \). The captured power is only controlled by regulating \( T_{g\text{,ref}} \), which is also calculated by (10).

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V. SENSITIVITY CALCULATION OF WT LOAD

The fatigue loads of WTs can be divided into aerodynamic and gravity loads (external), and structural loads (internal) [26]. In this paper, the fatigue loads mainly focus on the loads of the drive train due to the torsion of the shaft and the loads of the tower structure due to the tower deflection. Compared with static loads, the dynamic stress causing structural damage of WTs is a much bigger issue. By damping the fluctuations of low-speed shaft torque \( T_s \) and thrust force \( F_t \), the related fatigue loads can be reduced. Accordingly, for the drive train loads, the load sensitivity \( \frac{\partial L}{\partial F_{\text{ref}}} \) can be represented by \( \frac{\partial T_s}{\partial F_{\text{ref}}} \). For the tower structure loads, \( \frac{\partial L}{\partial F_{\text{ref}}} \) can be represented by \( \frac{\partial F_t}{\partial F_{\text{ref}}} \). If both drive train and tower structure loads are considered, \( \frac{\partial L}{\partial F_{\text{ref}}} \) can be represented by the combination of \( \frac{\partial L}{\partial F_{\text{ref}}} \) and \( \frac{\partial F_t}{\partial F_{\text{ref}}} \).

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A. Incremental State Space Model

Suppose the time of the operating point is \( t_0 \). The wind speed \( v_t \) is a variable which can either be measured or estimated [27]. In this study, \( v_t \) is estimated. The value at \( t = t_0 \) is \( v_{t_0} \) and assumed to be constant for the short control period. The measured power production, generator speed, filtered speed and pitch angle at \( t = t_0 \) are defined as \( P_{g0}, \omega_{g0}, \omega_{f0}, \text{ and } \theta_{0} \), respectively. According to (1) and (10), the aerodynamic torque and generator torque at \( t = t_0 \) can be calculated and are defined as \( T_{g0} \) and \( T_{g0} \), respectively.

Based on linearization of the simplified nonlinear WT model at the operating point, the incremental state space model for Region I is derived by the following steps. Then, the model

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for Region II can be derived by neglecting the term related to the pitch angle. The sign $\Delta$ indicates the increment of a variable.

**Step 1: Derivative equations of $\Delta \omega_g$, $\Delta \omega_l$ and $\Delta \beta$.**

Based on (4) and (5),

$$\Delta \omega_g = \frac{\eta_{e}}{J_t}(\Delta T_a - \eta_{e} \Delta T_g) + \frac{\eta_{e}}{J_t} (T_{0b} - \eta_{e} \omega_g \tau_0).$$  

(11)

Based on (8),

$$\Delta \omega_l = -\frac{1}{\tau_l} \Delta \omega_l + \frac{1}{\tau_l} \Delta \omega_g.$$  

(12)

By defining $\beta \triangleq K_c \theta = K_o \theta + K_o \theta^2$, (8) is transformed into,

$$\beta = K_p(\omega_l - \omega_{g, \text{rate}}) + K_i \frac{\omega_l - \omega_{g, \text{rate}}}{\tau}.$$  

(13)

Based on (12) and (13),

$$\Delta \beta = K_p \Delta \omega_l + K_i (\omega_{l, \text{rate}} + \Delta \omega_l - \omega_{g, \text{rate}})$$  

$$= \frac{K_p}{\tau_l} \Delta \omega_g + \left(-\frac{K_p}{\tau_l} + K_i \right) \Delta \omega_l + K_i (\omega_{l, \text{rate}} - \omega_{g, \text{rate}}).$$  

(14)

**Step 2: Calculation of $\Delta T_a$ and $\Delta T_g$.**

Equation (10) is nonlinear. It could be approximately calculated around the operating point according to the Taylor series,

$$\Delta T_g \approx - \frac{P_{0g0}}{\omega_{0g0}^2} \Delta \omega_l + \frac{1}{\omega_{0g0}} \Delta P_{\text{ref}}^w.$$  

(15)

Similarly, according to (11), $\Delta T_a$ can be calculated by,

$$\Delta T_a \approx \frac{\partial T_a}{\partial \omega_g} \big|_{(\omega_{0g0}, \nu_{0g0}, \theta_0)} \Delta \omega_g + \frac{\partial T_a}{\partial \beta} \big|_{(\omega_{0g0}, \nu_{0g0}, \theta_0)} \Delta \beta.$$  

(16)

In the following, $\frac{\partial T_a}{\partial \omega_g}$ and $\frac{\partial T_a}{\partial \beta}$ are used for $\frac{\partial T_a}{\partial \omega_g} \big|_{(\omega_{0g0}, \nu_{0g0}, \theta_0)}$ and $\frac{\partial T_a}{\partial \beta} \big|_{(\omega_{0g0}, \nu_{0g0}, \theta_0)}$, respectively.

**Step 3: Calculation of $\frac{\partial T_a}{\partial \omega_g}$ and $\frac{\partial T_a}{\partial \beta}$.**

By defining $P_0 \triangleq 0.5 \pi R^2 \nu_0^3$, the partial derivatives of $T_a$ are derived according to (1),

$$\frac{\partial T_a}{\partial \omega_g} = -\frac{\eta_{e} P_0 C_p(\omega_{g0}, \nu_{0g0}, \theta_0)}{\omega_{0g0}^2} + \frac{\eta_{e} P_0}{\omega_{0g0}} \frac{\partial C_p(\omega_{g0}, \nu_{0g0}, \theta_0)}{\partial \omega_g}$$  

(17)

$$\frac{\partial T_a}{\partial \beta} = \frac{\eta_{e} P_0}{\omega_{0g0}} \frac{\partial C_p(\omega_{g0}, \nu_{0g0}, \theta_0)}{\partial \beta}.$$  

(18)

Accordingly,

$$\frac{\partial T_a}{\partial \beta} = \frac{\partial T_a}{\partial \theta} \bigg|_{\nu_{0g0}, \omega_{0g0}, \theta_0} = \frac{\partial T_a}{\partial \theta} \frac{1}{\partial \theta} K_0 + 2K_0 \theta_0.$$  

(19)

**Step 4: Calculation of $\frac{\partial C_p}{\partial \omega_g}$ and $\frac{\partial C_p}{\partial \beta}$.**

The function $C_p(\omega_g, \nu, \theta)$ is nonlinear. Normally, it can be expressed in two formats. For the first format, $C_p$ is described by an empirical formula [28], e.g.,

$$C_p(\omega_g, \nu, \theta) = 0.22 \left( \frac{116}{\lambda} - 0.4 \theta - 5 \right) e^{\frac{12 + \lambda}{\lambda}},$$  

(20)

$$1 \frac{1}{\lambda} = \frac{1}{\lambda + 0.08 \theta} - \frac{0.035 \theta}{\lambda + 1}, \ \beta = \frac{\eta_g \omega_g \rho R}{\nu}.$$  

For the second format, $C_p$ is described in a lookup table derived from the geometry of the blades with inputs $\lambda$ and $\theta$. As shown in Fig. 4. The differences of $\lambda$ and $\theta$ of neighboring cells are $\Delta \lambda_{\text{tab}}$ and $\Delta \theta_{\text{tab}}$, respectively. In this study, the second format is used. The corresponding data for this study can be accessed in the wind turbine model of SimWindFarm—a publicly available Simulink toolbox for dynamic wind farm modeling, simulation, and control [21]. The plot of $C_p(\lambda, \theta)$ based on the lookup table is shown in Fig. 5.

**Step 5: Formulation of the state space model.**

According to (11)-(22), the continuous state space model for Region I is formulated as,

$$\dot{x} = A_1 x + B_1 \Delta P_{\text{ref}}^w + E_1,$$  

(23)

with

$$x = [\Delta \omega_g, \Delta \beta, \Delta \omega_l]^T,$$

$$A_1 = \begin{bmatrix} \eta_{e} \frac{\partial T_a}{\partial \omega_g} & \eta_{e} \frac{\partial T_a}{\partial \beta} & \eta_{e}^2 \frac{\partial P_0}{\partial \beta} \\ \frac{\partial T_a}{\partial \nu} & \frac{\partial T_a}{\partial \beta} & \frac{\partial T_a}{\partial \nu} \\ \frac{\partial T_a}{\partial \theta} & \frac{\partial T_a}{\partial \beta} & \frac{\partial T_a}{\partial \theta} \end{bmatrix},$$  

and

$$B_1 = \begin{bmatrix} \frac{\eta_{e}}{J_t} & \frac{\eta_{e}}{J_t} & \frac{\eta_{e}}{J_t} \\ 0 & - \frac{K_p}{\tau_l} + K_i \\ 0 & 0 & - \frac{1}{\tau_f} \end{bmatrix}.$$
\[ B_1 = \begin{bmatrix} -\frac{\eta_k^2}{J_t\omega_{00}} \\ \frac{\eta_k}{J_t} \\ 0 \\ \eta_k(T_{s0} - \eta_k T_{g0}) \end{bmatrix}, \quad E_1 = \begin{bmatrix} \frac{\eta_k}{J_t} \\ 0 \\ K_t(\omega_{00} - \omega_{g_{\text{rated}}}) \end{bmatrix}. \]

For Region II, the terms related to the pitch angle is neglected,
\[ x = [\Delta \omega_g, \Delta \omega_t]^T, \]
\[ A_{11} = \begin{bmatrix} \frac{\eta_k \partial T_a}{J_t \partial \omega_g} & \frac{\eta_k^2 P_{g0}}{J_t \omega_{00}} \\ -1 & -\frac{1}{J_t} \end{bmatrix}, \quad B_{11} = \begin{bmatrix} \frac{\eta_k}{J_t} \\ 0 \end{bmatrix}, \]
\[ E_{11} = \begin{bmatrix} \frac{\eta_k}{J_t}(T_{s0} - \eta_k T_{g0}) \\ 0 \end{bmatrix}. \]

**Step 5: Discretization.**

The continuous state space model (23) is discretized with the sampling period \( t_s \).

For Region I, the discrete state space model is,
\[ x(k + 1) = A_{1}^d x(k) + B_{1}^d \Delta P_{\text{ref}} + E_{1}^d, \tag{24} \]
with
\[ A_{1}^d = e^{A_{1} t_s}, \quad B_{1}^d = \int_0^{t_s} (e^{A_{1} s} B_1) ds, \quad E_{1}^d = \int_0^{t_s} (e^{A_{1} s} E_1) ds, \]

where \( k \) is the step index.

For Region II, the discrete state space model is,
\[ x(k + 1) = A_{II}^d x(k) + B_{II}^d \Delta P_{\text{ref}} + E_{II}^d, \tag{25} \]
with
\[ A_{II}^d = e^{A_{II} t_s}, \quad B_{II}^d = \int_0^{t_s} (e^{A_{II} s} B_{II}) ds, \quad E_{II}^d = \int_0^{t_s} (e^{A_{II} s} E_{II}) ds. \]

**B. Calculation of \( \frac{\partial T_s}{\partial P_{\text{ref}}} \)**

The shaft torque \( T_s \) twists the low-speed shaft. According to the motion equation,
\[ \omega_t = \frac{J_t}{J_s} (T_s - T_a) \Rightarrow T_s = T_a - J_t \omega_t. \tag{26} \]

Substituting (3) and (4) into (26),
\[ T_s = T_a - J_t \omega_t = T_a - \frac{J_t}{J_s} (T_a - \eta_s T_g), \tag{27} \]
\[ = \frac{J_t}{J_s} T_a + \frac{\eta_s J_t T_g}{J_t}, \]
\[ = \frac{\eta_s J_t}{J_t} T_a + \eta_s \frac{J_t}{J_s} T_g. \]

Accordingly,
\[ \Delta T_s = \frac{\eta_s^2 J_t}{J_t} \Delta T_a + \frac{\eta_s J_t}{J_t} \Delta T_g. \tag{28} \]

During the sampling period, the operation region of the WT may stay or change to another. When the current operating point is in Region I, i.e., \( \theta_0 > 0 \), with the increase of \( \Delta P_{\text{ref}} \), \( \theta_0 + \Delta \theta \) will decrease. If \( \theta_0 + \Delta \theta = 0 \), the system will transit into Region II. The corresponding \( \Delta P_{\text{ref}} \) is defined by \( \Delta P_{\text{ref}}^{\text{II}} \), which can be considered as the threshold.

According to (24),
\[ \Delta \beta = B_{1}^d(2, 1) \Delta P_{\text{ref}} + E_{1}^d(2, 1), \tag{29} \]
where \( B_{1}^d(2, 1) \) and \( E_{1}^d(2, 1) \) are the matrix elements of \( B_1^d \) and \( E_1^d \), respectively. Since \( \Delta \frac{\partial T_s}{\partial \theta} \approx \Delta \frac{\partial T_s}{\partial \theta_0} = K_0 + 2K_0 \theta_0, \)
\[ \Delta \theta = \frac{B_{1}^d(2, 1) \Delta P_{\text{ref}} + E_{1}^d(2, 1)}{K_0 + 2K_0 \theta_0}. \tag{30} \]

According to \( \Delta \theta = -\theta_0, \) \( \Delta P_{\text{ref}}^{\text{II}\rightarrow\text{I}} \) can be derived by,
\[ \Delta P_{\text{ref}}^{\text{II}\rightarrow\text{I}} = -\theta_0 (K_0 + 2K_0 \theta_0) - E_{1}^d(2, 1) B_{1}^d(2, 1). \tag{31} \]

When the current operating point is in Region II, i.e., \( \theta_0 = 0 \), with the decrease of \( \Delta P_{\text{ref}} \), \( \omega_{00} + \Delta \omega_t \) will increase. If \( \omega_{00} + \Delta \omega_t = \omega_{g_{\text{rated}}}, \) the system will transit into Region I. The corresponding \( \Delta P_{\text{ref}} \) is defined by \( \Delta P_{\text{ref}}^{\text{I}\rightarrow\text{II}} \), which can be considered as the threshold.

According to (25),
\[ \Delta \omega_t = B_{II}^d(2, 1) \Delta P_{\text{ref}} + E_{II}^d(2, 1), \tag{32} \]
where \( B_{II}^d(2, 1) \) and \( E_{II}^d(2, 1) \) are the matrix elements of \( B_{II}^d \) and \( E_{II}^d \), respectively. According to \( \omega_{00} + \Delta \omega_t = \omega_{g_{\text{rated}}}, \) \( \Delta P_{\text{ref}}^{\text{II}\rightarrow\text{I}} \) can be derived by,
\[ \Delta P_{\text{ref}}^{\text{II}\rightarrow\text{I}} = \eta_s \omega_{g_{\text{rated}}} - \omega_{00} - E_{II}^d(2, 1) B_{II}^d(2, 1). \tag{33} \]

In the following, 4 cases are summarized to calculate \( \frac{\partial T_s}{\partial P_{\text{ref}}} \).

**Case 1: Region I \rightarrow Region I.**

If \( \Delta P_{\text{ref}} \leq \Delta P_{\text{ref}}^{\text{II}\rightarrow\text{I}} \), the system stays in Region I. Based on (15) and (16), (28) can be transformed into,
\[ \Delta T_s = C_{1}^T \Delta \omega_t + D_{1}^T \Delta P_{\text{ref}}, \tag{34} \]
with
\[ C_{1}^T = \begin{bmatrix} \eta_s^2 J_t \frac{\partial T_a}{\partial \omega_g} & \eta_s J_t \frac{\partial T_a}{\partial \beta} - P_{g0} \eta_s J_t \omega_{00} \omega_t \end{bmatrix}, \]
\[ D_{1}^T = \frac{\eta_s J_t}{J_t \omega_{00}}. \]

Based on (24) and (34),
\[ \Delta T_s(k + 1) = (C_{1}^T B_{1}^d + D_{1}^T) \Delta P_{\text{ref}} + C_{1}^T E_{1}^d. \tag{35} \]

Hence,
\[ \frac{\partial T_s}{\partial P_{\text{ref}}} \approx \Delta T_s \Delta P_{\text{ref}} = S_{1}^T + Y_{1}^T, \tag{36} \]
with \( S_{1}^T = C_{1}^T B_{1}^d + D_{1}^T, \) \( Y_{1}^T = C_{1}^T E_{1}^d \). The subscript of \( S_{1}^T \) and \( Y_{1}^T \) indicates the case index.

**Case 2: Region II \rightarrow Region II.**

If \( \Delta P_{\text{ref}} > \Delta P_{\text{ref}}^{\text{II}\rightarrow\text{I}} \), the system stays in Region II. Based on (15) and (16), (28) can be transformed into,
\[ \Delta T_s = C_{II}^T \Delta \omega_t + D_{II}^T \Delta P_{\text{ref}}, \tag{37} \]
with
\[ C_{II}^T = \begin{bmatrix} \eta_s^2 J_t \frac{\partial T_a}{\partial \omega_g} - P_{g0} \eta_s J_t \omega_{00} \omega_t \end{bmatrix}, \quad D_{II}^T = \frac{\eta_s J_t}{J_t \omega_{00}}. \]
Based on (25) and (37),
\[ \Delta T_s(k+1) = (C_{II}^{T} B_{II}^{d} + D_{II}^{T}) \Delta P_{ref}^{wt} + C_{II}^{T} E_{II}^{d}. \]  
(38)

Hence,
\[ \frac{\partial T_s}{\partial P_{ref}^{wt}} \approx \frac{\Delta T_s}{\Delta P_{ref}^{wt}} = S_2^{T_s} + \frac{Y_2^{T_s}}{S_2^{P_{ref}^{wt}}}, \]  
(39)

with \( S_2^{T_s} = C_{II}^{T} B_{II}^{d} + D_{II}^{T}, \ Y_2^{T_s} = C_{II}^{T} E_{II}^{d}. \)

**Case 3: Region I→Region II.**

If \( \Delta P_{ref}^{wt} > \Delta P_{ref}^{wt}, \) the system transits from Region I to Region II. In that case, \( \Delta P_{ref}^{wt} \) could be divided into two parts: \( \Delta P_{ref}^{wt} \) and \( \Delta P_{ref}^{wt} - \Delta P_{ref}^{wt}. \) The former part works in Region I and the latter part works in Region II.

Accordingly, \( \Delta T_s(k+1) \) can be approximately calculated by,
\[ \Delta T_s(k+1) \approx \Delta T_s^{T_s} \Delta P_{ref}^{wt} + Y_1^{T_s} + \]
\[ \approx S_2^{T_s} \Delta P_{ref}^{wt} + Y_1^{T_s} + Y_2^{T_s} + (S_1^{T_s} - S_2^{T_s}) \Delta P_{ref}^{wt}. \]  
(40)

Hence,
\[ \frac{\partial T_s}{\partial P_{ref}^{wt}} \approx \frac{\Delta T_s}{\Delta P_{ref}^{wt}} = S_2^{T_s} + \frac{Y_2^{T_s}}{S_2^{P_{ref}^{wt}}}, \]  
(41)

with \( S_3^{T_s} = S_2^{T_s}, \ Y_3^{T_s} = Y_1^{T_s} + Y_2^{T_s} + (S_1^{T_s} - S_2^{T_s}) \Delta P_{ref}^{wt}. \)

**Case 4: Region II→Region I.**

If \( \Delta P_{ref}^{wt} \) is less than or equal to \( \Delta P_{ref}^{wt} \), the system transits from Region II to Region I. Similarly, \( \Delta P_{ref}^{wt} \) could be divided into two parts: \( \Delta P_{ref}^{wt} \) and \( \Delta P_{ref}^{wt} - \Delta P_{ref}^{wt}. \) The former part works in Region II and the latter part works in Region I. \( \Delta T_s(k+1) \) can be calculated by approximately,
\[ \Delta T_s(k+1) \approx \Delta T_s^{T_s} \Delta P_{ref}^{wt} + Y_2^{T_s} + \]
\[ \approx S_1^{T_s} \Delta P_{ref}^{wt} + Y_1^{T_s} + Y_2^{T_s} + (S_2^{T_s} - S_1^{T_s}) \Delta P_{ref}^{wt}. \]  
(42)

Hence,
\[ \frac{\partial T_s}{\partial P_{ref}^{wt}} \approx \frac{\Delta T_s}{\Delta P_{ref}^{wt}} = S_1^{T_s} + \frac{Y_1^{T_s}}{S_1^{P_{ref}^{wt}}}, \]  
(43)

with \( S_3^{T_s} = S_2^{T_s}, \ Y_3^{T_s} = Y_1^{T_s} + Y_2^{T_s} + (S_2^{T_s} - S_1^{T_s}) \Delta P_{ref}^{wt}. \)

In the following, for generality, the subscripts of \( S_1^{T_s} \) and \( Y_2^{T_s} \) are omitted. Based on the measurements, \( S_1^{T_s} \) and \( Y_2^{T_s} \) can be calculated explicitly, which are sent to the wind farm controller to formulate the optimal dispatch algorithm.

**C. Calculation of \( \frac{\partial F_t}{\partial P_{ref}^{wt}} \)**

Similar to \( \frac{\partial T_s}{\partial P_{ref}^{wt}} \), 4 cases are summarized to calculate \( \frac{\partial F_t}{\partial P_{ref}^{wt}} \).

**Case 1: Region I→Region I.**

If \( \Delta P_{ref}^{wt} \) is less than or equal to \( \Delta P_{ref}^{wt} \), the system stays in Region I. \( F_t \) can be calculated by,
\[ F_t = C_1^{F_t} x, \]  
(44)

with \( C_1^{F_t} = [\frac{\partial F_t}{\partial x}, \frac{\partial F_t}{\partial x} \ 0]. \)

**Case 2: Region II→Region II.**

If \( \Delta P_{ref}^{wt} > \Delta P_{ref}^{wt} \), the system stays in Region II. \( F_t \) can be calculated by,
\[ F_t = C_2^{F_t} x, \]  
(47)

Based on (24) and (47),
\[ \frac{\partial F_t}{\partial P_{ref}^{wt}} \approx \frac{\Delta F_t}{\Delta P_{ref}^{wt}} = S_2^{F_t} + \frac{Y_2^{F_t}}{S_2^{P_{ref}^{wt}}}, \]  
(49)

with \( S_2^{F_t} = C_1^{F_t} B_1^{d}, \ Y_2^{F_t} = C_1^{F_t} E_1^{d}. \) The subscript of \( S_2^{F_t} \) and \( Y_2^{F_t} \) indicates the case index.

**Case 3: Region I→Region II.**

If \( \Delta P_{ref}^{wt} > \Delta P_{ref}^{wt} \), the system stays in Region II. \( F_t \) can be calculated by,
\[ F_t = C_1^{F_t} x, \]  
(47)

Based on (25) and (49),
\[ \frac{\partial F_t}{\partial P_{ref}^{wt}} \approx \frac{\Delta F_t}{\Delta P_{ref}^{wt}} = S_3^{F_t} + \frac{Y_3^{F_t}}{S_3^{P_{ref}^{wt}}}, \]  
(51)

with \( S_3^{F_t} = C_1^{F_t} B_1^{d}, \ Y_3^{F_t} = C_1^{F_t} E_1^{d}. \)

**Case 4: Region II→Region I.**

If \( \Delta P_{ref}^{wt} \) is less than or equal to \( \Delta P_{ref}^{wt} \), the system stays in Region I. \( F_t \) can be calculated by,
\[ F_t = C_1^{F_t} x, \]  
(47)

Based on (24) and (49),
\[ \frac{\partial F_t}{\partial P_{ref}^{wt}} \approx \frac{\Delta F_t}{\Delta P_{ref}^{wt}} = S_4^{F_t} + \frac{Y_4^{F_t}}{S_4^{P_{ref}^{wt}}}, \]  
(53)

with \( S_4^{F_t} = S_1^{F_t}, \ Y_4^{F_t} = Y_1^{F_t} + Y_2^{F_t} + (S_1^{F_t} - S_2^{F_t}) \Delta P_{ref}^{wt}. \)

Hence,
\[ \frac{\partial F_t}{\partial \omega} = \frac{P_0}{v_{10}} \frac{\partial C_1}{\partial \omega} \frac{\partial F_t}{\partial \delta} = \frac{P_0}{v_{10}} \frac{\partial C_1}{\partial \delta}, \]  
(54)
The function $C_t$ is nonlinear. Similar to $C_p$, $C_t$ is also described in a lookup table derived from the geometry of the blades with inputs $\lambda$ and $\theta$ [21]. The corresponding data for this study can be obtained in the wind turbine model of SimWindFarm. The plot of $C_t(\lambda, \theta)$ based on the lookup table is shown in Fig. 6.

![Fig. 6. $C_t(\lambda, \theta)$ based on the data from SimWindFarm [21].](image)

According to $v_{r0}$, $\omega_{g0}$, and $\theta_0$, the power coefficient at the operating point $C_{t0}$ can be found based on the lookup table, i.e., $C_{t0} = C_{t(n,m)}$, where $n$ and $m$ are the corresponding row and column indices, respectively. $\frac{\partial C_t}{\partial \omega_g}$ and $\frac{\partial C_t}{\partial \theta}$ can be calculated by,

$$\frac{\partial C_t}{\partial \omega_g} = \frac{R_{\eta g}}{v_{r0}} \frac{\partial C_t}{\partial \lambda}, \quad \frac{\partial C_t}{\partial \lambda} \approx \frac{C_t(n,m+1) - C_{t0}}{\Delta \lambda_{tab}}, \quad (55)$$

$$\frac{\partial C_t}{\partial \theta} = \frac{\partial C_t}{\partial \lambda} \frac{1}{K_0 + 2K_0\theta_0}, \quad \frac{\partial C_t}{\partial \theta} \approx \frac{C_t(n+1,m) - C_{t0}}{\Delta \theta_{tab}}, \quad (56)$$

In the following, for generality, the subscripts of $S_i$, and $Y_{Fi}$ are omitted. Based on the measurements, $S_i$, and $Y_{Fi}$ can be calculated explicitly, which are sent to the wind farm controller to formulate the optimal dispatch algorithm.

VI. FORMULATION OF OPTIMAL DISPATCH ALGORITHM

A. Cost Function

Conventionally, the dispatch algorithm is based on a proportional distribution of the available active power [7]. Suppose a wind farm consists of $N_{wt}$ WTs. According to [7], the power reference of the $i$th WT is calculated by,

$$P_{ref, i}^{wt} = \alpha_i P_{ref, i}^{wfc}, \quad \alpha_i = \frac{P_{ref, i}^{wt}}{P_{ref, i}^{wfc}}, \quad P_{ref, i}^{wfc} = \sum_{i=1}^{N_{wt}} P_{ref, i}^{wt} \frac{P_{ref, i}^{wt}}{P_{ref, i}^{wfc}}, \quad (57)$$

where $\alpha_i$ is the distribution factor of the $i$th WT and $P_{ref, i}^{wt}$ is the available power of the $i$th WT.

In this study, based on the proportional dispatch algorithm, the control objective is to dynamically redistribute power to minimize the fatigue loads experienced by the WTs while tracking $P_{ref}^{wfc}$ all the time. The $P_{ref}^{wfc}$ tracking is regarded as an equality constraint, described in Section VI-B. The minimization of the fatigue loads implies the minimization of the variation of $T_a$ and $F_t$, which is included in the cost function.

By defining the control vector $u_{ref}$,

$$u_{ref} \triangleq [\Delta P_{ref, 1}^{wt}, \ldots, \Delta P_{ref, N_{wt}}^{wt}]^T, \quad u_{ref} \in \mathbb{R}^{N_{wt} \times 1},$$

the optimization problem can be formulated as,

$$\min_{u_{ref}} \sum_{i=1}^{N_{wt}} \parallel u_{ref}^i + P_{g0}^i - \alpha_i P_{ref}^{wfc} \parallel^2_{Q_P}, \quad \min_{u_{ref}} \sum_{i=1}^{N_{wt}} \parallel \Delta T_{a0}^i u_{ref}^i \parallel^2_{Q_{T_{a0}}}, \quad \min_{u_{ref}} \sum_{i=1}^{N_{wt}} \parallel \Delta F_{t0}^i u_{ref}^i \parallel^2_{Q_{F_{t0}}}, \quad (58)$$

where $Q_P$ is the weighting factor which penalizes the deviation of $P_{ref}^{wt}$ to its proportional value, $Q_{T_{a0}}$ is the weighting factor which penalizes the variation of $T_a$, and $Q_{F_{t0}}$ is the weighting factor which penalizes the variation of $F_t$.

As shown in Term 1 of (58), $u_{ref}^i$ is around $\alpha_i P_{ref}^{wfc} - P_{g0}^i$. Therefore, by assuming $u_{ref}^i \approx \alpha_i P_{ref}^{wfc} - P_{g0}^i$, the case index of the system during the control interval (Case 1~Case 4) in Subsection V-B and Subsection V-C could be estimated. Accordingly, $S_{T_{a0}}^i$ and $S_{F_{t0}}^i$ could be decided. Term 2 and Term 3 in (58) can be transformed into,

$$\min_{u_{ref}} \sum_{i=1}^{N_{wt}} \parallel ST_{a0}^i u_{ref}^i + Y_{T_{a0}}^i u_{ref} \parallel^2_{Q_{T_{a0}}} + \parallel SF_{t0}^i u_{ref}^i + Y_{F_{t0}}^i u_{ref} \parallel^2_{Q_{F_{t0}}}, \quad (59)$$

B. Constraints

The constraints are summarized as follows:

1) Power Reference Tracking: According to $P_{ref}^{wfc}$, the total power reference increments of WTs should follow,

$$\sum_{i=1}^{N_{wt}} u_{ref}^i = P_{ref}^{wfc} - P_{g0}, \quad (60)$$

where $P_{ref}^{wfc}$ is the measured output of the wind farm.

2) Local WT Constraint: For individual WTs, there exists the available power limit,

$$u_{ref} \in [-P_{g0}, P_{ref, i}^{avg} - P_{g0}]. \quad (61)$$

For generality, the turbine index $i$ is omitted.

Besides, as mentioned in Subsection VI-A, the case index of the system is estimated based on $\alpha P_{ref}^{wfc} - P_{g0}$. Accordingly, $u_{ref}$ should be limited in the local constraint to guarantee that the system will be in the estimated case, i.e.,

$$\left\{ \begin{array}{l}
    \text{If } \alpha P_{ref}^{wfc} - P_{g0} \leq \Delta P_{ref, i}^{wt} 
    \text{(Case 1)}, \quad u_{ref} \leq \Delta P_{ref, i}^{wt} \\
    \text{If } \alpha P_{ref}^{wfc} - P_{g0} > \Delta P_{ref, i}^{wt} 
    \text{(Case 2)}, \quad u_{ref} > \Delta P_{ref, i}^{wt} \\
    \text{If } \alpha P_{ref}^{wfc} - P_{g0} > \Delta P_{ref, i}^{avg} 
    \text{(Case 3)}, \quad u_{ref} > \Delta P_{ref, i}^{avg} \\
    \text{If } \alpha P_{ref}^{wfc} - P_{g0} \leq \Delta P_{ref, i}^{avg} 
    \text{(Case 4)}, \quad u_{ref} \leq \Delta P_{ref, i}^{avg}.
\end{array} \right. \quad (62)$$

By merging (61) and (62), the feasible operation range of $u_{ref}$ can be derived,

$$u_{ref} \in [u_{min}, u_{max}]. \quad (63)$$

Accordingly, $P_{min} = P_{g0} + u_{min}$ and $P_{max} = P_{g0} + u_{max}$.

The derived optimization problem can be reformulated as a standard Quadratic Programming (QP) problem, whose rank is equal to the number of WTs. It can be efficiently solved by a number of commercial solvers.
C. Discussion

The computation task of the optimal wind farm control mainly consists of formulating and solving the optimal problem. Accordingly, the improvement with the proposed method can be described in the following two aspects.

1) Formulation of the optimal problem: With the proposed method, the operation region can be determined according to the measurements. Accordingly, the offline calculated parameters of the region can be derived and the load sensitivities can be calculated based on the explicit equations. As such, a part of the computation burden required for the online computation can be removed. Moreover, the task has been distributed to local controllers, which can be solved in parallel. With increasing the number of WTs, this efficiency improvement becomes higher. Therefore, the dedicated controller is computationally viable for implementation in large wind farms.

2) Solution of the optimal problem: The time complexity, expressed by $O$, is used to indicate the amount of time taken by an algorithm. As mentioned in [29], QP problems can be solved roughly with the same efficiency as LP problems. The time complexity of the practical algorithm to solve LP problem with $n$ variables and $m$ constraints requires roughly $O(n^{3}m^{0.5} + n^{2}m^{1.5})$. Compared with the method in [14], the formulated optimal problem of the proposed method has reduced optimization variables ($n = N_{wt}$) and constraints ($m = N_{wt} + 1$). The corresponding time complexity of the proposed method is less.

VII. CASE STUDIES

A wind farm comprised of 10×5MW WTs is used as the test system. The wind field modeling considering turbulences and wake effects for the wind farm is generated from SimWindFarm [21]. The control period of the wind farm control $t_{s}$ is set as 1s.

![Fig. 7. $p_{wfc}^{av}$ and $p_{wfc}^{pref}$ under both low and high wind conditions.](image)

In order to test the efficacy of the developed dispatch algorithm, the operation of the wind farm under both low and high conditions were studied. The available power of the wind farm $P_{wfc}^{av}$ under both conditions is shown in Fig. 7. The typical active control scheme, balance control mode, is used in this study, where the wind farm production is reduced to specified constant levels [30]. The simulation results of the proposed optimal algorithm ("OPT") are compared with the conventional proportional dispatch algorithm in [7] ("CON").

The dynamic turbine behavior in a simulated wind field yields time series of loads or stresses. Through post-processing, the fatigue cycles based on the rainflow counting method is derived to evaluate the performance of the proposed scheme [31]. Besides, the Damage Equivalent Load (DEL), based on Miner’s rule and dependent on materials properties specified by the slope of the S-N curve, is used to quantify the load minimization. In this study, the related calculations are completed by MCrunch, developed by NREL [32].

A. Decision of Weighting Factors

The control objective of the cost function (58) consists of the following two parts, which represent the minimization of $\Delta T_{s}$ and $\Delta F_{i}$, respectively,

$$\text{Obj1} \equiv \sum_{i=1}^{N_{wt}} \|\Delta T_{s}^{i}\|^{2}, \quad \text{Obj2} \equiv \sum_{i=1}^{N_{wt}} \|\Delta F_{i}^{i}\|^{2}. \quad (64)$$

The weighting factors for Obj1 and Obj2 are $Q_{T}$ and $Q_{F}$. They can be considered as a whole part, which represents the load minimization of the wind farm. By defining $Q_{Load} \equiv Q_{T} + Q_{F}$, it is obvious that larger $Q_{Load}$ can lead to a better performance of the load alleviation. In this study, $Q_{F} = 1$ and $Q_{Load} = 600$. By defining $\gamma \equiv \frac{Q_{T}}{Q_{Load}}$,

$$Q_{T} = \gamma Q_{Load}, \quad Q_{F} = (1 - \gamma)Q_{Load}. \quad (65)$$

Fig. 8 shows the Pareto frontier under both low and high wind conditions. By increasing the ratio $\gamma$, Obj1 decreases while Obj2 increases. For the low wind condition, it can be observed that $\gamma = 0.0017$ is the optimum solution. A significant reduction of $\Delta F_{i}$ (Obj2) can be observed, which is from 1 to 0.33 (67%). Comparably, the reduction of $\Delta T_{s}$ (Obj1) is not sensitive, which is from 1 to 0.81 (19%). For the high wind condition, it can be observed that $\gamma = 0.003$ is the optimum solution. The reduction of $\Delta F_{i}$ (Obj2) is from 1 to 0.83 (17%). Comparably, the reduction of $\Delta T_{s}$ (Obj1) is similar, which is from 1 to 0.84 (16%).

![Fig. 8. Pareto frontier under low and high wind conditions.](image)

It can be observed that the optimum $\gamma$ is related to the available power. In this study, $\gamma$ is adaptive to different wind conditions and can be approximately calculated by,

$$\gamma \approx \frac{\sum_{i=1}^{N_{wt}} P_{av}^{opt,i}}{18000}, \quad P_{av}^{opt,i} = 0.5 \pi R^{2} v_{i}^{3} C_{p}^{max}, \quad (66)$$
where $C_{P,\text{max}}^{1}$ is the maximum power coefficient. The unit of $P_{\text{avw, max}}$ is in MW. Accordingly, $Q_{T_{s}}$ and $Q_{F_{i}}$ can be derived, which are used for the following case scenarios.

### B. Operation under Low Wind Condition

The average wind speeds of all WTs ($v_{\text{avr}}$) in the wind farm are listed in Table II, which range from 8.85 m/s to 9.97 m/s. As shown in Fig. 9, three scenarios are defined according to different $P_{\text{wfc, ref}}$: $P_{\text{wfc, ref}} = 20$ MW (Scenario 1), $P_{\text{wfc, ref}} = 17.5$ MW (Scenario 2), and $P_{\text{wfc, ref}} = 15$ MW (Scenario 3). The simulation time is 300 s.

![Fig. 9. $P_{\text{wfc,avr}}$ and $P_{\text{wfc,ref}}$ under the low wind condition.](image)

#### 1) Power Reference Tracking:

To evaluate the tracking performance, the Root Mean Square Errors (RMSEs) for both algorithms are calculated and listed in Table I. Both values are identical and quite small, which implies the same tracking performances of both algorithms.

<table>
<thead>
<tr>
<th>Scenario</th>
<th>CON ($P_{\text{wfc,avr}}$)</th>
<th>OPT ($P_{\text{wfc,avr}}$)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Scenario 1</td>
<td>0.012 MW</td>
<td>0.012 MW</td>
</tr>
<tr>
<td>Scenario 2</td>
<td>0.005 MW</td>
<td>0.005 MW</td>
</tr>
<tr>
<td>Scenario 3</td>
<td>0.003 MW</td>
<td>0.003 MW</td>
</tr>
</tbody>
</table>

![Fig. 10. $T_{s}$ of WT08 for Scenario 2.](image)

#### 2) Fatigue Loads Reduction:

Firstly, more details of the simulation result for Scenario 2 are shown. A representative WT (WT08) is used as an example. The variations of $T_{s}$ with the two algorithms are shown in Fig. 10(a). Compared with the CON, the variation of the shaft torque $\Delta T_{s}$ is reduced with the OPT. According to the cumulative rainflow cycles in Fig. 10(b), less cycles are found for the OPT, which implies less fatigue loads experienced by the WT.

The variations of $M_{t}$ with the two algorithms are shown in Fig. 11(a). Compared with the CON, the variation of $\Delta M_{t}$ is reduced with the OPT. According to the cumulative rainflow cycles in Fig. 11(b), less cycles are found in the large tower bending moment for the OPT, which implies less fatigue loads experienced by the WT.

![Fig. 11. $M_{t}$ of WT08 for Scenario 2.](image)

The calculated DELs of $T_{s}$ and $M_{t}$ for all WTs are listed in Table II and III, respectively. As shown in Table II, with the OPT, most DELs are reduced. From the whole wind farm point of view, the total DEL of $T_{s}$ is reduced by 2.11%. Similarly, as shown in Table III, most DELs are reduced. The reduction of the total DEL of $M_{t}$ is 11.36%.

The simulation results of Scenario 1–3 are summarized in Table IV. As mentioned in Section VII-A, $\Delta F_{i}$ is more sensitive under the load wind condition. Therefore, for the DELs of $M_{t}$, the reductions of the OPT are significant, which range from 11.30% to 13.32%. Comparably, the changes of the DELs of $T_{s}$ for the OPT are limited, which range from 0.73% to −2.11%.

### C. Operation under High Wind Condition

The average wind speeds of all WTs ($v_{\text{avr}}$) in the wind farm are listed in Table VI, which range from 12.85 m/s to 13.97 m/s. As shown in Fig. 12, three scenarios are defined according to different $P_{\text{wfc, ref}}$: $P_{\text{wfc, ref}} = 45$ MW (Scenario 4),
with the two algorithms are shown in Fig. 13(a). Compared with the CON, the variation of $\Delta M_t$ is reduced with the OPT. According to the cumulative rainflow cycles in Fig. 13(b), less cycles are found for the OPT, which implies less fatigue loads experienced by the WT.

![Fig. 13. $P_{wfc}^{ref}$ and $P_{wfc}^{ave}$ under the high wind condition.](image)

**TABLE V**

<table>
<thead>
<tr>
<th>Scenario</th>
<th>CON</th>
<th>OPT</th>
</tr>
</thead>
<tbody>
<tr>
<td>Scenario 4</td>
<td>0.010 MW</td>
<td>0.009 MW</td>
</tr>
<tr>
<td>Scenario 5</td>
<td>0.009 MW</td>
<td>0.009 MW</td>
</tr>
<tr>
<td>Scenario 6</td>
<td>0.008 MW</td>
<td>0.008 MW</td>
</tr>
</tbody>
</table>

$P_{wfc}^{ref} = 42.5$ MW (Scenario 5), and $P_{wfc}^{ref} = 40$ MW (Scenario 6). The simulation time is 300 s.

1) **Power Reference Tracking**: To evaluate the tracking performance, the RMSEs for both algorithms are calculated and listed in Table V. Most values of the OPT are the same as those of the CON.

![Fig. 12. Power reference tracking for WTs.](image)

![Fig. 14. Fatigue loads reduction for WTs.](image)

**TABLE III**

<table>
<thead>
<tr>
<th>No.</th>
<th>$v_{ave}$ in m/s</th>
<th>DEL (CON) in MNm</th>
<th>DEL (OPT) in MNm</th>
<th>Percentage</th>
</tr>
</thead>
<tbody>
<tr>
<td>WT01</td>
<td>8.85</td>
<td>2.60</td>
<td>2.60</td>
<td>0.73%</td>
</tr>
<tr>
<td>WT02</td>
<td>9.09</td>
<td>3.17</td>
<td>3.05</td>
<td>-13.76%</td>
</tr>
<tr>
<td>WT03</td>
<td>9.46</td>
<td>3.49</td>
<td>3.32</td>
<td>-13.32%</td>
</tr>
<tr>
<td>WT04</td>
<td>9.10</td>
<td>3.86</td>
<td>3.70</td>
<td>-9.99%</td>
</tr>
<tr>
<td>WT05</td>
<td>9.75</td>
<td>4.71</td>
<td>4.42</td>
<td>-13.32%</td>
</tr>
<tr>
<td>WT06</td>
<td>9.09</td>
<td>1.86</td>
<td>1.74</td>
<td>-12.62%</td>
</tr>
<tr>
<td>WT07</td>
<td>9.50</td>
<td>1.80</td>
<td>1.64</td>
<td>-11.62%</td>
</tr>
<tr>
<td>WT08</td>
<td>9.97</td>
<td>1.54</td>
<td>1.41</td>
<td>-11.32%</td>
</tr>
<tr>
<td>WT09</td>
<td>9.74</td>
<td>1.80</td>
<td>1.64</td>
<td>-11.62%</td>
</tr>
<tr>
<td>WT10</td>
<td>2.39</td>
<td>2.38</td>
<td>-0.42%</td>
<td></td>
</tr>
</tbody>
</table>

**TABLE IV**

<table>
<thead>
<tr>
<th>Scenario</th>
<th>Type</th>
<th>DEL (CON) in MNm</th>
<th>DEL (OPT) in MNm</th>
<th>Percentage</th>
</tr>
</thead>
<tbody>
<tr>
<td>Scenario 1</td>
<td>$T_s$</td>
<td>21.94</td>
<td>22.20</td>
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<td></td>
<td>$M_t$</td>
<td>404.16</td>
<td>350.34</td>
<td>-13.32%</td>
</tr>
<tr>
<td>Scenario 2</td>
<td>$T_s$</td>
<td>18.46</td>
<td>18.07</td>
<td>-2.11%</td>
</tr>
<tr>
<td></td>
<td>$M_t$</td>
<td>269.39</td>
<td>238.78</td>
<td>-11.36%</td>
</tr>
<tr>
<td>Scenario 3</td>
<td>$T_s$</td>
<td>14.86</td>
<td>14.82</td>
<td>-0.27%</td>
</tr>
<tr>
<td></td>
<td>$M_t$</td>
<td>213.19</td>
<td>187.63</td>
<td>-11.99%</td>
</tr>
</tbody>
</table>

$P_{wfc}^{ave}$ and $P_{wfc}^{ref}$ for Scenario 5.

The variations of $M_t$ with the two algorithms are shown in Fig. 14(a). Compared with the CON, the variation of $\Delta M_t$ is reduced with the OPT. According to the cumulative rainflow cycles in Fig. 14(b), less cycles are found in the large tower moment for the OPT, which implies less fatigue loads experienced by the WT.

The calculated DELs of $T_s$ and $M_t$ for all WTs are listed in Table VI and VII, respectively. As shown in Table VI, compared with the CON, all the DELs are reduced with the OPT. The reduction values are from 0.00% to 39.62%. From
the whole wind farm point of view, the total DEL of $T_s$ is reduced by 14.88%. Similarly, as shown in Table VII, most DELs are reduced. The reduction of the total DEL of $M_t$ is 21.19%.

**TABLE VI**

DELS OF WTs ($T_s$) FOR SCENARIO 5

<table>
<thead>
<tr>
<th>No.</th>
<th>$V_{\text{ave}}$ in m/s</th>
<th>DEL (CON) in MNm</th>
<th>DEL (OPT) in MNm</th>
<th>Percentage</th>
</tr>
</thead>
<tbody>
<tr>
<td>WT01</td>
<td>12.85</td>
<td>1.44</td>
<td>1.21</td>
<td>-15.97%</td>
</tr>
<tr>
<td>WT02</td>
<td>13.09</td>
<td>1.37</td>
<td>1.19</td>
<td>-13.14%</td>
</tr>
<tr>
<td>WT03</td>
<td>13.46</td>
<td>1.35</td>
<td>1.11</td>
<td>-17.78%</td>
</tr>
<tr>
<td>WT04</td>
<td>13.10</td>
<td>1.52</td>
<td>1.43</td>
<td>-5.92%</td>
</tr>
<tr>
<td>WT05</td>
<td>13.75</td>
<td>0.53</td>
<td>0.32</td>
<td>-39.62%</td>
</tr>
<tr>
<td>WT06</td>
<td>13.09</td>
<td>0.61</td>
<td>0.45</td>
<td>-26.23%</td>
</tr>
<tr>
<td>WT07</td>
<td>13.50</td>
<td>0.36</td>
<td>0.32</td>
<td>-11.11%</td>
</tr>
<tr>
<td>WT08</td>
<td>13.97</td>
<td>0.57</td>
<td>0.57</td>
<td>0.00%</td>
</tr>
<tr>
<td>WT09</td>
<td>13.24</td>
<td>0.45</td>
<td>0.36</td>
<td>-20.00%</td>
</tr>
<tr>
<td>WT10</td>
<td>13.45</td>
<td>1.21</td>
<td>1.05</td>
<td>-13.22%</td>
</tr>
<tr>
<td>Summary</td>
<td></td>
<td>9.41</td>
<td>8.01</td>
<td>-14.88%</td>
</tr>
</tbody>
</table>

Sometimes, it might be more beneficial to sacrifice $P_{\text{wfc}}^{\text{ref}}$ to reduce the damages to the WTs. How to evaluate the economical benefit of the DEL reduction and strike a balance between the DEL reduction and wind power generation will be studied in the future work.

**TABLE VII**

DELS OF WTs ($M_t$) FOR SCENARIO 5

<table>
<thead>
<tr>
<th>No.</th>
<th>$V_{\text{ave}}$ in m/s</th>
<th>DEL (CON) in MNm</th>
<th>DEL (OPT) in MNm</th>
<th>Percentage</th>
</tr>
</thead>
<tbody>
<tr>
<td>WT01</td>
<td>12.85</td>
<td>57.75</td>
<td>45.07</td>
<td>-21.96%</td>
</tr>
<tr>
<td>WT02</td>
<td>13.09</td>
<td>48.66</td>
<td>46.41</td>
<td>-4.62%</td>
</tr>
<tr>
<td>WT03</td>
<td>13.46</td>
<td>46.16</td>
<td>44.13</td>
<td>-4.40%</td>
</tr>
<tr>
<td>WT04</td>
<td>13.10</td>
<td>41.88</td>
<td>42.09</td>
<td>0.50%</td>
</tr>
<tr>
<td>WT05</td>
<td>13.75</td>
<td>61.38</td>
<td>27.65</td>
<td>-54.95%</td>
</tr>
<tr>
<td>WT06</td>
<td>13.09</td>
<td>49.60</td>
<td>26.56</td>
<td>-46.45%</td>
</tr>
<tr>
<td>WT07</td>
<td>13.50</td>
<td>27.31</td>
<td>24.39</td>
<td>-10.69%</td>
</tr>
<tr>
<td>WT08</td>
<td>13.97</td>
<td>51.74</td>
<td>48.97</td>
<td>-5.35%</td>
</tr>
<tr>
<td>WT09</td>
<td>13.24</td>
<td>32.40</td>
<td>28.54</td>
<td>-11.91%</td>
</tr>
<tr>
<td>WT10</td>
<td>13.45</td>
<td>54.32</td>
<td>37.54</td>
<td>-30.89%</td>
</tr>
<tr>
<td>Summary</td>
<td></td>
<td>371.35</td>
<td>237.35</td>
<td>-21.19%</td>
</tr>
</tbody>
</table>

**TABLE VIII**

COMPARISON OF DELS FOR DIFFERENT SCENARIOS

<table>
<thead>
<tr>
<th>Scenario</th>
<th>Type</th>
<th>DEL (CON) in MNm</th>
<th>DEL (OPT) in MNm</th>
<th>Percentage</th>
</tr>
</thead>
<tbody>
<tr>
<td>Scenario 4</td>
<td>$T_s$</td>
<td>10.67</td>
<td>9.5</td>
<td>-10.97%</td>
</tr>
<tr>
<td>Scenario 5</td>
<td>$T_s$</td>
<td>471.20</td>
<td>371.35</td>
<td>-21.19%</td>
</tr>
<tr>
<td>Scenario 6</td>
<td>$T_s$</td>
<td>431.44</td>
<td>321.99</td>
<td>-30.72%</td>
</tr>
</tbody>
</table>

Fig. 14. $M_t$ of WT05 for Scenario 5.

Fig. 15. Relation between DEL and $P_{\text{wfc}}^{\text{ref}}$. 

Fig. 15. Relation between DEL and $P_{\text{wfc}}^{\text{ref}}$. 

The simulation results of Scenario 4—6 are summarized in Table VIII. Compared with the CON, the DELs of both $T_s$ and $M_t$ with the OPT are reduced significantly. Specifically, for $T_s$, the reduction values range from 10.97% to 20.77%. For $M_t$, the reduction values range from 16.24% to 25.37%.

3) Discussion: The relation between the DEL value and $P_{\text{wfc}}^{\text{ref}}$ is analyzed. By taking the DEL value of $P_{\text{wfc}}^{\text{ref}} = 45$ MW as the reference, different $P_{\text{wfc}}^{\text{ref}}$ are sampled and the corresponding DELs in p.u. are calculated. According to these points, the fitted curve can be derived based on the nonlinear least square algorithm, as shown in Fig. 15. It can be observed that the DEL can be reduced by decreasing the wind power generation. However, with smaller $P_{\text{wfc}}^{\text{ref}}$, the reduction sensitivity becomes smaller. For the wind farm operator, the damage to the WTs might be also considered to decide $P_{\text{wfc}}^{\text{ref}}$. 

**Fig. 14.** $M_t$ of WT05 for Scenario 5.
VIII. CONCLUSION

In this paper, an optimal dispatch algorithm based on fatigue load sensitivity is developed for the active power control of wind farms. The load sensitivity and feasible range of the power reference for individual WTs are used to formulate the optimal dispatch problem, which are calculated locally. With this configuration, most computation tasks are distributed to the local WT controllers. The complicated wind farm model is not required and the computation burden of the wind farm controller is largely reduced. Moreover, the explicit analytical equations of the load sensitivity are derived to improve the computation efficiency of the local controller. The proposed dispatch algorithm is suitable for real-time control of large-scale wind farms. Case studies show the developed algorithm can achieve good performances of power tracking. Moreover, the fatigue loads experienced by WTs are largely alleviated.

APPENDIX

The parameters of 5 MW wind turbine model are listed in Table IX.

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
<th>value</th>
</tr>
</thead>
<tbody>
<tr>
<td>η</td>
<td>Multiplier ratio</td>
<td>97</td>
</tr>
<tr>
<td>R</td>
<td>Rotor blade length (m)</td>
<td>63</td>
</tr>
<tr>
<td>H</td>
<td>Height of the rotor center (m)</td>
<td>87.6</td>
</tr>
<tr>
<td>Jp</td>
<td>Rotor inertia (kg·m²)</td>
<td>3.544 · 10⁷</td>
</tr>
<tr>
<td>Jg</td>
<td>Generator inertia (kg·m²)</td>
<td>534.116</td>
</tr>
<tr>
<td>kth</td>
<td>Drive train spring constant (N-m/rad)</td>
<td>8.676 · 10⁸</td>
</tr>
<tr>
<td>cth</td>
<td>Drive train damping constant</td>
<td>6.215 · 10⁶</td>
</tr>
<tr>
<td>Mcow</td>
<td>Integrated tower mass (kg)</td>
<td>3.475 · 10⁵</td>
</tr>
<tr>
<td>ωg,imated</td>
<td>Rated generator speed (rad/s)</td>
<td>122.91</td>
</tr>
<tr>
<td>ωr,imated</td>
<td>Rated rotor speed (rad/s)</td>
<td>1.26</td>
</tr>
<tr>
<td>θmax</td>
<td>Max. pitch angle (deg)</td>
<td>90</td>
</tr>
<tr>
<td>θmin</td>
<td>Min. pitch angle (deg)</td>
<td>0</td>
</tr>
<tr>
<td>Kp</td>
<td>Proportional gain of the pitch control</td>
<td>0.2143</td>
</tr>
<tr>
<td>Ki</td>
<td>Integral gain of the pitch control</td>
<td>0.0918</td>
</tr>
<tr>
<td>Kg</td>
<td>Gain scheduling coefficient</td>
<td>1</td>
</tr>
<tr>
<td>Kgh</td>
<td>Gain scheduling coefficient</td>
<td>2.1323</td>
</tr>
</tbody>
</table>

REFERENCES

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