



## Highly Subwavelength, Superdirective Cylindrical Nanoantenna

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**Highly Subwavelength, Superdirective Cylindrical Nanoantenna**Samel Arslanagić<sup>1</sup> and Richard W. Ziolkowski<sup>2,3</sup><sup>1</sup>*Technical University of Denmark, Lyngby DK-2800, Denmark*<sup>2</sup>*University of Technology Sydney, Ultimo, New South Wales 2007, Australia*<sup>3</sup>*The University of Arizona, Tucson, Arizona 85721, USA*

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A superdirective cylindrical nanoantenna is demonstrated with a multilayered cylindrical metamaterial-inspired structure. Targeting specific scattering coefficients for the dipole and higher-order modes, the ideal limit of needle radiation is demonstrated. A five-layer system is optimized to demonstrate its approach to the theoretical directivity bound. While the resulting structure is scalable to any frequency regime, its highly subwavelength overall size ( $\lambda_0/10$ ) takes advantage of combinations of positive and negative permittivity materials in the optical regime.

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The ability to control passive and active nanosystems has far-reaching importance in several emerging fields of science and engineering, as well as to applications with high societal benefit. Significant interest has thus emerged in developing optical nanoantennas to control light-matter interactions [1]. Highly directive optical elements have been shown to have many impactful applications, for example, enhanced Raman spectroscopy [2], emission enhancement of single photons [3,4], ultrasensitive sensing [5,6], enhanced photodetection [7], remote sensing [8], and wireless power transmission [9]. Several classic antenna approaches [10] to achieving higher directivity at optical frequencies have been reported. These include Yagi-Uda nanoantennas [11,12] and nanoantenna arrays [13,14]. A variety of electric and magnetic dipolar and multipolar approaches have also been considered [15–23]. The former yield electrically large systems. The latter yield higher maximum directivity values or higher front-to-back ratios (FTBRs) but have multiple large sidelobes or broad radiation patterns. In contrast, we have developed a highly subwavelength, single element with needlelike radiation performance.

This goal was achieved by combining the metamaterial-inspired paradigm [24] that employs near-field resonant parasitic (NFRP) elements to enhance and control the emissions from a driven source with the concept of having those elements generate higher-order modes (HOMs) [25]. However, in contrast to the array of elemental Huygens multipole radiators investigated in Ref. [25], we consider herein the use of a single multilayered cylindrical highly subwavelength structure as the NFRP element driven by a line source to achieve the desired needlelike performance. Since the objective is to demonstrate its superdirective (i.e., directivity larger than that of a reference antenna system of the same size excited with a uniform amplitude and phase) capabilities, both the source and the structure are assumed

infinite to simplify the analysis and design. Through the simultaneous excitation of its dipole and HOMs at the desired frequency in a single, properly designed multilayered structure, superdirective radiation is demonstrated; i.e., the cylindrical waves emitted by the source are transduced into a highly collimated beam.

The multilayer scattered field coefficients are developed based on both Dirac-delta and binomial distributions to illustrate being able to tailor the characteristics of the resulting radiation performance by design in analogy with classical array theory [10]. We demonstrate that those multielement array behaviors can be emulated with these multilayered structures. In contrast to previous superdirective studies, e.g., Refs. [15,20,22], that considered higher directivity from spherical single-layer plasmonic or all-dielectric core-shell structures by exciting individual electric and magnetic dipole or HOMs, it is demonstrated herein that a Dirac-delta-based multilayer NFRP nanoantenna can produce not only high directivity but needlelike radiation patterns with very low sidelobe levels by combining properly weighted combinations of the dipole and several HOMs whose availability is facilitated by the thicknesses and material properties of those multilayers. Moreover, the cylindrical geometry and its natural polarization selectivity enable applications not accessible with their highly symmetric spherical counterparts. A five-layer, metamaterial-inspired structure is optimized to demonstrate approaching the theoretical directivity bound in practice.

A cross section of the two-dimensional (2D) based canonical configuration of interest is depicted in Fig. 1. As an  $N + 1$  region configuration, it is the general case. It consists of a circularly cylindrical core of radius  $r_1$  (region 1) covered with  $N - 1$  concentric layers, region  $j$  with outer radius  $r_j$ ,  $j = 2, \dots, N$ . These  $N$  layers are embedded in an infinite ambient host medium (region  $N + 1$ ). A cylindrical

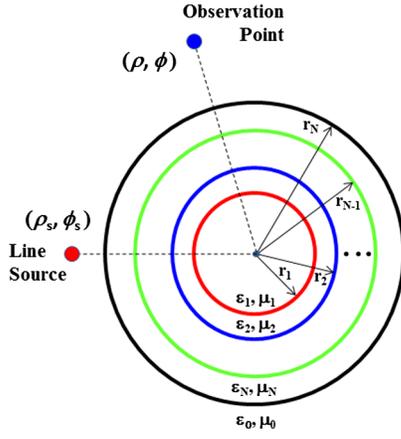


FIG. 1. Line source excited  $N$  layer,  $N + 1$  region, 2D concentric cylinder structure.

coordinate system,  $(\rho, \phi, z)$ , is introduced. The axes of the cylinders coincide with the  $z$  axis. Region  $i$ , with  $i = 1, 2, \dots, N$ , is characterized by a permittivity and a permeability. Assuming the  $\exp(j\omega t)$  time dependence throughout, they are denoted by  $\epsilon_i = \epsilon'_i - j\epsilon''_i$  and  $\mu_i = \mu'_i - j\mu''_i$ , respectively, and a wave number  $k_i = \omega\sqrt{\epsilon_i}\sqrt{\mu_i}$ . The host medium, region  $N + 1$ , without any loss of generality is taken to be free space with permittivity  $\epsilon_0$  and permeability  $\mu_0$ . The cylindrical regions are excited by an infinite,  $z$ -oriented line source located in region  $N + 1$ . Thus, the wave number in the source region is the free-space wave number  $k_{N+1} = k_0 = \omega\sqrt{\epsilon_0\mu_0}$ . In the time harmonic case, the source is characterized by the

frequency  $f_0$  and the corresponding free-space wavelength  $\lambda_0 = c/f_0$ , where  $c$  is the speed of light in a vacuum:  $c = 1/\sqrt{\epsilon_0\mu_0}$ . Consequently, the free-space wave number is also  $k_0 = 2\pi/\lambda_0$ .

The excitation is taken to be a magnetic line source (MLS). Consequently, only  $TE^z$  polarized fields and dielectric layers are considered. A more general discussion is provided in Ref. [26]. The coordinates of the line source are  $(\rho_s, \phi_s)$ , while those of the observation points are  $(\rho, \phi)$ . The MLS is defined by the constant magnetic current  $I_{MLS} = 1.0$  [V].

Fields in a cylindrical geometry can be decomposed into cylindrical harmonics. Because of the restriction to two dimensions and the azimuthal symmetry, only three of the six electromagnetic field components ( $H_z, E_\rho, E_\phi$ ) are needed to characterize any given  $TE^z$  field. In fact, only the  $H_z$  component of the field and derivatives of it are needed to characterize the  $TE^z$  source and scattered fields. The main steps of the analytical solution of this canonical scattering problem are reviewed in Ref. [26] and outlined in general, e.g., in Ref. [34]. Since only the total magnetic field in the exterior region is needed for the directivity outcome, the source ( $E_\rho^{MLS}, E_\phi^{MLS}$ ) and scattered ( $E_\rho^{scat}, E_\phi^{scat}$ ) electric field components, which are readily obtained from these magnetic fields, are not included here. They are provided for completeness along with the solution process for determining the unknown expansion coefficients in Ref. [26].

The magnetic source and scattered field pieces in the exterior region are explicitly

$$\mathbf{H}_{MLS}(\rho, \phi) = -\hat{z}I_{MLS}(\omega) \frac{\omega\epsilon_{N+1}}{4} \begin{cases} \sum_{m=0}^{\infty} \tau_m J_m(k_{N+1}\rho) H_m^{(2)}(k_{N+1}\rho_s) \cos[m(\phi - \phi_s)] & \text{for } \rho \leq \rho_s, \\ \sum_{m=0}^{\infty} \tau_m J_m(k_{N+1}\rho_s) H_m^{(2)}(k_{N+1}\rho) \cos[m(\phi - \phi_s)] & \text{for } \rho \geq \rho_s, \end{cases} \quad (1)$$

$$\mathbf{H}^{scat}(\rho, \phi) = -\hat{z}I_{MLS}(\omega) \frac{\omega\epsilon_{N+1}}{4} \times \sum_{m=0}^{\infty} \tau_m A_m^{N+1} H_m^{(2)}(k_{N+1}\rho) \cos[m(\phi - \phi_s)], \quad (2)$$

where  $H_m^{(2)}(\cdot)$  is the Hankel function of the second kind of order  $m$ , and  $A_m^{N+1}$  are the expansion coefficients of the scattered field and where  $\tau_0 = 1$  and  $\tau_m = 2$  for  $m \neq 0$ . Once the source and scattered field coefficients are known, a variety of figures of merit can be derived. The exact infinite series solution is truncated to a finite number of modes in practice after justifying that the higher-order ones have little impact on those outcomes.

The directivity is the quantity of major interest here. It is defined as the ratio of the radiation intensity in a given direction to the radiation intensity averaged over all

directions. With  $\mathbf{H}_{tot}^{ff} = [\mathbf{H}_{MLS} + \mathbf{H}_{scat}]^{ff}$  being the total magnetic far field in the exterior region [26], the directivity for the MLS-excited  $N$ -layered cylinder is

$$D_N(\phi) = \frac{2\pi\rho |\mathbf{H}_{tot}^{ff}(\rho, \phi)|^2}{\int_0^{2\pi} |\mathbf{H}_{tot}^{ff}(\rho, \phi)|^2 \rho d\phi} = \frac{|\sum_{m=0}^{\infty} \tau_m j^m [J_m(k_0\rho_s) + A_m^{N+1}] \cos[m(\phi - \phi_s)]|^2}{\sum_{m=0}^{\infty} \tau_m |J_m(k_0\rho_s) + A_m^{N+1}|^2}. \quad (3)$$

It is emphasized that the exterior region scattered field coefficients  $A_m^{N+1}$  depend on the field coefficients associated with each of the  $N$  layers.

Let  $\psi = \phi_{max} - \phi_s$ , where  $\phi_{max}$  is the direction into which one would like to have the maximum directivity. Then the parameters of the material layers (their thickness

and permittivities) will be tailored to produce scattering coefficients yielding a desired directivity pattern. We begin with the choices that lead to a Dirac-delta outcome in a specified direction. Recall from the theory of distributions [35] that

$$\delta(x - a) = \frac{1}{2\pi} + \frac{1}{\pi} \sum_{m=1}^{\infty} \cos[m(x - a)]. \quad (4)$$

This suggests setting the Dirac-delta-based coefficients  $A_{m,\delta}^{N+1}$  to

$$\begin{aligned} A_{0,\delta}^{N+1} &= \frac{1}{2\pi} - J_0(k_0\rho_s), \\ A_{m,\delta}^{N+1} &= \frac{1}{\tau_m \pi j^m} \cos(m\psi) - J_m(k_0\rho_s) \quad \text{for } m > 0. \end{aligned} \quad (5)$$

The directivity for the  $N$ -layer problem with the sum truncated to  $N + 1$  terms then becomes

$$D_N(\phi) \approx \frac{|1 + 2 \sum_{m=1}^N \cos(m\psi) \cos[m(\phi - \phi_s)]|^2}{1 + 2 \sum_{m=1}^N |\cos(m\psi)|^2}. \quad (6)$$

With the desire to have the cylinder system convert the line source field into a directive beam, it is natural and most effective to have the beam direction pointed away from the source. The angles which finalize the scattering coefficients (5) are thus explicitly set to  $\phi_s = \pi$  and  $\phi_{\max} = 0$  without any loss of generality. Since  $\psi = -\pi$ , one then has  $1 + 2 \sum_{m=1}^N |\cos(-m\pi)|^2 = 1 + 2N$ , and the directivity becomes

$$D_N(\phi) \approx \frac{|1 + 2 \sum_{m=1}^N \cos(m\phi)|^2}{1 + 2N}. \quad (7)$$

One recognizes immediately from (4) that, as  $N \rightarrow \infty$  in (7), needle radiation in the  $\phi = 0$  direction is obtained; i.e.,  $D_{N \rightarrow \infty}(\phi) \propto \delta(\phi)$ . The maximum directivity for a finite number of layers  $N$  is

$$D_{N,\max}(\phi = 0) \approx \frac{|1 + 2 \sum_{m=1}^N 1|^2}{1 + 2N} = 2N + 1, \quad (8)$$

which, as derived in Ref. [26], is the theoretical maximum for two dimensions. A comparison of the directivities (in decibel units) as functions of the observation angle  $\phi$  exhibited by the  $N = 5, 10, 100$ , and  $1000$  layer cases is shown in Fig. 2. The maximum directivity in each case is confirmed to be 11, 21, 201, and 2001, i.e.,  $2N + 1$ . The FTBR, i.e.,  $D_N(\phi = 0^\circ)/D_N(\phi = 180^\circ)$ , for each case is, respectively, 20.83, 26.44, 46.06, and 66.02 dB. The  $N = 1000$  case clearly demonstrates its needlelike behavior.

It is well known that the amplitude and/or phase distributions between the elements of an antenna array can be designed to control its radiation characteristics [10].

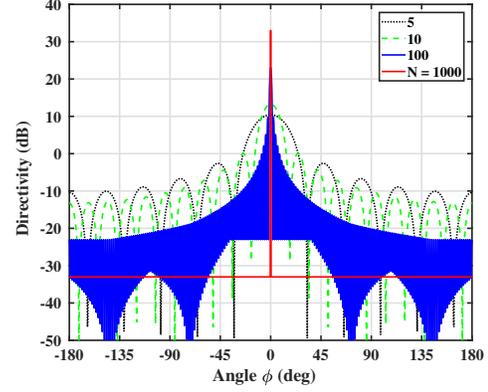


FIG. 2. Comparison of the directivity generated by the Dirac-delta coefficients associated with the  $N = 5$ ,  $N = 10$ ,  $N = 100$ , and  $N = 1000$  layer structures.

Common amplitude distributions for broadside radiating, uniformly spaced arrays are uniform (largest directivity), Dolph-Tschebyscheff (specified flat sidelobe level), and binomial (few or no sidelobes). To demonstrate that the scattering coefficients of the multilayer structure can be weighted to produce other beams tailored by choice, a binomial distribution was also considered. The weights of a binomial configuration with  $N$  modes are

$$p_m^N = \frac{(N-1)!}{m!(N-1-m)!}, \quad m = 0, 1, \dots, N-1, \quad (9)$$

which correspond to the expansion coefficients of the polynomial  $(1+x)^{N-1}$  [10]. Proceeding as we did with the Dirac-delta-based coefficients, the radiation intensity of the line source-multilayered cylinder system will have a binomial-distribution behavior if the scattered field coefficients are

$$A_{m,\text{binom}}^{N+1} = j^{-n} \frac{p_m^N}{\max p_m^N} \cos m\psi - J_m(k_0\rho_s), \quad (10)$$

where each term has been normalized by the largest one:  $\max \{p_m^N/\tau_m\}$ .

The directivities associated with the Dirac-delta- and binomial-distribution-based scattered field coefficients for  $N = 10$  layers are compared in Fig. 3(a). The Dirac-delta coefficients produce a more directive, more tightly confined main beam [first null appears at  $\phi_{\text{null}} = 2\pi/(2N+1)$ ] with lower sidelobes. On the other hand, the binomial case is broader but has fewer sidelobes. The corresponding maximum directivity as the number of layers  $N$  (hence, modes) increases, which was obtained by calculating the directivity (3) with those coefficients and finding the maximum value, is shown in Fig. 3(b). The  $D_{N,\max}$  values achieve their upper bounds  $2N + 1$  in each Dirac-delta case. The directivity of the binomial coefficient-based beam clearly begins to saturate as the number

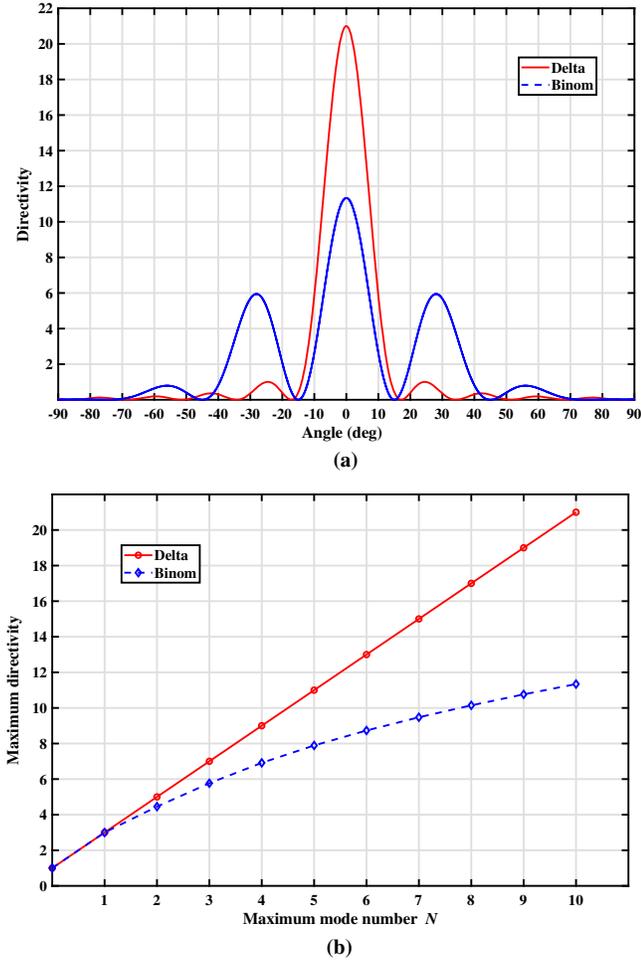


FIG. 3. Directivity obtained for the Dirac-delta- and binomial-distribution-based scattered field coefficients. (a) Patterns for  $N = 10$ . (b) Maximum directivity as the maximum mode number  $N$  varies (linear scales).

of layers (hence, modes) increases. In contrast to the equal power weighting associated with each Dirac-delta mode, the binomial weights decrease as the mode number increases. These coefficient choices clearly demonstrate the ability to customize the output beam of the system simply by tailoring the scattering coefficients through the geometry and material choices in analogy with amplitude tapering in a classic antenna array.

Several multilayered cylinder configurations were explored to illustrate their potential to achieve these highly directive behaviors. Considering the degrees of freedom in the system, the number of modes that one can generate on demand and control is directly tied to the number of layers of the structure and the materials from which it is made. In principle,  $N$  layers can be optimized to generate at least  $N + 1$  modes of significance with the desired amplitudes and phases. As demonstrated in Ref. [26], the remaining modes contribute little to the overall scattering, since they are not designed to resonate with the source in any way. The

mode sums are then truncated and limited to the  $m = 0, 1, \dots, N$  terms.

A highly subwavelength, MLS-excited,  $N = 5$  layer, lossless structure, whose exterior radius was fixed to be  $r_5 = \lambda_0/10$ , was investigated. This electrically small system has a transverse effective width  $W_{\text{eff}} = 2r_5 = \lambda_0/5$ . The MLS is located at  $(\rho, \phi) = (1.05r_5, 180^\circ)$ , far enough away from the origin to produce several HOMS. As derived in Ref. [26], the directivity of the analogous uniformly excited two-dimensional antenna system is  $D_{2D} = 2\pi W_{\text{eff}}/\lambda_0$ . Consequently, any five-layered configuration that yields a directivity greater than  $D_{2D} = 1.257$  is superdirective [10]. If it approaches the maximum  $D_{N=5, \text{max}} = 11 = 8.75D_{2D}$ , it is needlelike. Since the structure and results are defined in terms of  $\lambda_0$ , they scale to any frequency. In particular, for an optical source with  $\lambda_0 = 500$  nm, the cylindrical nanoantenna has a 50 nm radius.

The optimization process is detailed in Ref. [26]. The material choices take advantage of the known miniaturization capabilities associated with the juxtaposition of positive and negative material regions [36] which naturally are available in the optical regime. The relative permittivities in the five-layer structure were determined to be  $\epsilon_{1r} = 6.618$ ,  $\epsilon_{2r} = -6.651$ ,  $\epsilon_{r3} = -4.622$ ,  $\epsilon_{r4} = 39.864$ , and  $\epsilon_{r5} = -49.979$ , when the radii of the layers were specified to be  $r_1 = 0.015\lambda_0$ ,  $r_2 = 0.030\lambda_0$ ,  $r_3 = 0.070\lambda_0$ ,  $r_4 = 0.085\lambda_0$ , and  $r_5 = 0.10\lambda_0$ . The corresponding  $m = 0, 1, \dots, 5$  scattering coefficients were obtained and used to calculate (6). A comparison of the directivity determined with these numerically obtained scattering coefficients and the Dirac-delta-based ones (5) for this MLS-excited five-layer cylindrical scattering structure is given in Fig. 4. The maximum  $D_{N=5, \text{max}} = 10.686 = 8.5D_{2D}$  occurs along the  $\phi = 0^\circ$  direction and the associated FTBR = 54.83 = 17.39 dB. These results demonstrate that this multilayered

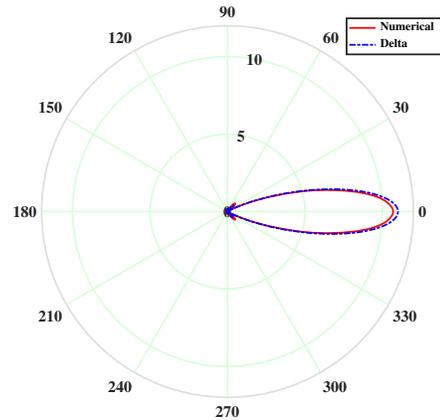


FIG. 4. Comparisons of the directivity obtained with only the  $m = 0, 1, \dots, 5$  numerically obtained and the Dirac-delta-based scattering coefficients for the MLS-excited, five-layer highly subwavelength cylinder (linear scale).

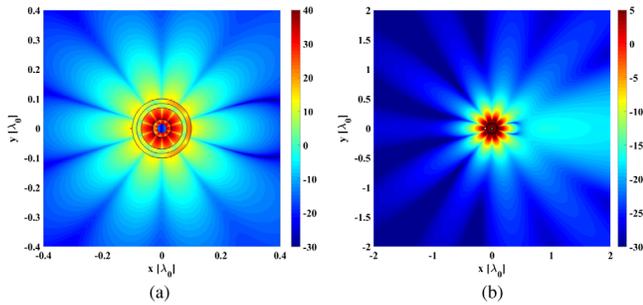


FIG. 5. Plots of  $10 \log_{10} |H_z(x, y)|$  for the MLS-excited, five-layer highly subwavelength cylinder. (a) Near field (the red dot denotes the source location). (b) Far field (the white dot denotes the source location).

cylinder acts as a superdirective lens element that transduces the cylindrical waves from the MLS into a highly directive beam.

The near- and midfield distributions of the magnitude of the total magnetic field,  $10 \log_{10} |H_z^{\text{tot}}(x, y)|$  (i.e., in decibel units), of the optimized five-layer structure are shown in Figs. 5(a) and 5(b), respectively. From the near-field plot, one immediately recognizes that the  $N = 5$  mode is quite dominant in the vicinity of the structure and the total field is strongly excited around the  $\phi = 0$  direction in layer 5. Furthermore, one begins to see in the midrange results that the main beam is becoming dominant and the sidelobes are beginning to disappear. Thus, while the  $N = 5$  mode is necessary for the large  $D_{\text{max}}$  value, the lower-order modes are necessary with the correct weighting to significantly reduce the sidelobe levels. Furthermore, the superdirective behavior is obtained with only one set of field modes; the complementary  $\text{TM}^z$  set is not present. These results reaffirm similar conclusions given in Ref. [25].

It is again noted that only the modes  $N = 0, 1, \dots, 5$  were superimposed to obtain all of these results. More HOMs would be required only if more layers were included in the configuration. It is further illustrated in Ref. [26] that, as the overall size of the structure is allowed to be larger, one can demonstrate not only this highly directive behavior with only positive material layers, but even superbackscattering [37].

Large epsilon-negative and positive permittivity values are naturally available at optical frequencies from both metals and resonant polaritonic materials. However, these optical materials are generally very lossy. While they do not impact the ratio of the radiated powers, large losses have detrimental effects on a structure's ability to promote the presence of the HOMs. Hence, losses negatively impact the overall directivity. Nevertheless, by introducing gain into an optical structure, these deleterious loss effects can be mitigated. Consequently, a practical demonstration of these superdirective outcomes should be focused on those frequencies. The resulting highly directive optical nanoantennas would have many potential photonics applications

ranging from sensors and microscopy to integrated optical circuits. On the other hand, many natural and artificially realized very small and large positive and negative permittivity, low loss materials are now available at microwave and millimeter wave frequencies. The ability to achieve superdirective beams from electrically small systems would have many practical applications in current and future wireless systems. Thus, the reported developments are also very relevant to those lower-frequency bands.

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