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Subsolidus phase relations of the $\text{CoO}_x - \text{CuO} - \text{SrO}$ system

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Abstract

The subsolidus phase relations of the $\text{CoO}_x - \text{CuO} - \text{SrO}$ system were investigated in air. The samples were equilibrated at 900°C . The pseudo-ternary section contains three stoichiometric binary oxide phases (Sr_2CuO_3 , SrCuO_2 and $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41-\delta}$) and a binary oxide solid solution: $\text{Sr}_{6+x}\text{Co}_5\text{O}_{15+\delta}$ ($0 \leq x \leq 0.36$). Two binary phases extend into the ternary system forming solid solutions, i.e. $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ ($0 \leq x \leq 5$) and $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ ($0 \leq x \leq 0.36$, $0 \leq y \leq 1.0$). The $\text{Sr}_{6+x}\text{Co}_5\text{O}_{15+\delta}$ solid solution was found to undergo a phase separation into a mixture of $\text{Sr}_6\text{Co}_5\text{O}_{15-\delta}$ and $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ upon annealing at 600°C . This transformation is reversible.

Keywords: Experimental phase equilibria, isothermal section, oxide systems, pseudoternary

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Introduction

The sensational discovery of high-temperature superconductivity in $\text{La}_{2-x}\text{Ba}_x\text{CuO}_{4-\delta}$ in 1986 [1], induced tremendous research activity to find new cuprate compounds with higher transition temperatures. Among other strategies, the phase equilibria of many pseudo-ternary phase diagrams including CuO and an alkaline earth oxide (mostly BaO, SrO or CaO) have been screened. However, while combinations of those oxides with rare-earth oxides have been systematically studied ([2] and references therein), combinations consisting of CuO, SrO and oxides of transition metals (TM) are still poorly investigated. The published phase diagrams of CuO – SrO – TM-oxide systems are limited to TM = V [3], Nb [4,5], Fe [6], Ti [7,8], Zr and Hf [8], Ta [9] and W [10]. Cobalt, being magnetic, is not in principle expected to be favourable for the appearance of superconductivity. However, mixing elements such as Cu and Co in ternary oxide compounds or solid solutions could result in interesting effects. It was therefore important to study the possibility of reciprocal doping in the binary oxides of the Co-Sr-O and Cu-Sr-O systems and to assess the occurrence of ternary oxide compounds in the CoO_x – CuO – SrO system. The equilibration conditions (i.e. 900°C in air) were selected, because they correspond to conditions similar to those employed for preparing compounds that exhibit high superconducting transition temperatures, i.e. reaction at 865°C – 910°C in air [11,12].

Previous work

(1) CuO – SrO

This pseudo-binary system has been studied in detail, in particular in relation to the advent of high-temperature superconductors [13-18]. In air, three intermediate phases are stable: Sr_2CuO_3 , SrCuO_2 and $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$, the latter being sometimes referred to as $\text{Sr}_3\text{Cu}_5\text{O}_8$. All three are stable at 900°C. An additional binary oxide phase with SrCu_2O_2 composition is stable under low oxygen partial pressure conditions only (p_{O_2}

< 0.06 at 900°C) [17,18]. The SrCu_2O_3 and $\text{Sr}_2\text{Cu}_3\text{O}_5$ phases were synthesised under high pressure (1.7GPa – 8GPa) [19].

(2) $\text{CoO}_x - \text{CuO}$

Two early experimental studies on this system have been published [20,21]. In both, the samples were equilibrated in air. However, Landolt and Muan [21] only reported the phase equilibria between 1000°C and 1120°C. In contrast, the work by Driessens et al [20] covers the 600°C to 1150°C range. More recently, Zabdyr and Fabrichnaya [22] reassessed the system between 727°C and 1127°C by means of calculations based on previously published data as well as a set of new EMF measurements performed on 8 compositions and further included a description of the liquidus as part of a study of the Co – Cu – O – Si system [23]. At 900°C, these authors found that Co can dissolve into the monoclinic CuO tenorite phase up to a little less than 5 at.%, i.e. $\text{Cu}_{1-x}\text{Co}_x\text{O}_{1+\delta}$ ($x \approx 0.05$) [22]. Co substitution in CuO was also reported in [21], although the solubility limit was closer to $x = 0.03$ at 1000°C and appeared to decrease with temperature. In contrast, Driessens et al. [20] found no measurable Co solubility in CuO.

For higher Co contents, references [22] and [20] agree on the existence of a two-phase region with equilibrium between CuO and a Co-rich cubic rock-salt phase. The maximum Cu solubility in this $\text{Co}_{1-x}\text{Cu}_x\text{O}_{1-\delta}$ rock-salt solid-solution at 900°C is $x \approx 0.33$ [20] or $x \approx 0.38$ [22]. Whereas the composition range of this phase at 900°C extends all the way to pure CoO according to Zabdyr and Fabrichnaya [22], Driessens et al. [20] report a lower value of $x \approx 0.17$ at 900°C in $\text{Co}_{1-x}\text{Cu}_x\text{O}_{1+\delta}$.

According to Driessens et al. [20], for lower Cu content, the cubic rock-salt phase co-exists with the cubic spinel Co_3O_4 phase, which itself admits Cu substitution up to nearly 10 at.% for Co at 865°C. However, at 900°C, the solubility limit is reduced to

about 1 at.%. Finally, the transition between Co_3O_4 and CoO for the pure cobalt-oxygen system is given as 920°C in [20] versus 877°C in [22].

(3) CoO_x - SrO

The phase equilibria of the SrO - CoO_x system in air have recently been reported by Jankovský et al. [24]. Earlier, several distinct binary oxide compounds had already been described, all being members of a general family with general formula $\text{Sr}_{n+2}\text{Co}_{n+1}\text{O}_{3n+3}$ ($n = 1, 2, 3, 4, \dots$). The Co-richest known phase is the $n = \infty$ member: SrCoO_{3-x} , also described as $\text{Sr}_2\text{Co}_2\text{O}_5$ [24]. This phase adopts the brownmillerite structure [25,26] and was reported to undergo a structural transformation at lower temperatures [25]. More recently, Harrison et al. [27] first demonstrated that the $\text{Sr}_2\text{Co}_2\text{O}_5$ phase is in fact unstable in air below 900°C and decomposes into a mixture of $\text{Sr}_6\text{Co}_5\text{O}_{15}$ and Co_3O_4 when annealed at 875°C . This fact is confirmed in the detailed study of Jankovský et al. [24], who found that $\text{Sr}_2\text{Co}_2\text{O}_5$ is only stable between 903°C and 1269°C .

The $n = 1$ member of the $\text{Sr}_{n+2}\text{Co}_{n+1}\text{O}_{3n+3}$ series, i.e. $\text{Sr}_3\text{Co}_2\text{O}_6$ (orthorhombic, space group Immm) is also a high temperature phase stable between 984°C and 1335°C [24]. According to Takami et al. [28], the $n = 2$ member, i.e. $\text{Sr}_4\text{Co}_3\text{O}_9$ (trigonal, space group P321), can be synthesized by reaction of Co_3O_4 and SrCO_3 at 800°C – 940°C in air. This phase is not present in the SrO – CoO_x phase diagram [24].

On the other hand, the $n = 3$ and $n = 4$ members ($\text{Sr}_5\text{Co}_4\text{O}_{12}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$), crystallising in the space groups P3c1 and R32 respectively, have been reported as being stable at room temperature [27,29]. While $\text{Sr}_5\text{Co}_4\text{O}_{12}$ is not present in the Sr - Co - O diagram of Jankovský et al. [24], $\text{Sr}_6\text{Co}_5\text{O}_{15}$ is reported to be stable up to 914°C , whereas another phase described as $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ is stable up to 1035°C . The latter was first mentioned by Boulahya et al. [30], who rather describe the Sr - Co - O

phases as members of a $(A_3Co_2O_6)_\alpha(A_3Co_3O_9)_\beta$ family, in which they also identified a compound with $Sr_{21}Co_{17}O_{51}$ composition.

(4) $CoO_x - CuO - SrO$

No study of this system appears to have been published so far. It is nevertheless known that 20 at.% Cu in the $Sr_{14}Cu_{24}O_{41-\delta}$ phase can be replaced by Co [31], while $SrCoO_2$ may also allow some limited Co substitution on Cu sites [32]. In contrast, there seems to be no report on Cu substitution in the binary Sr-Co oxide phases.

Experimental details

70 different nominal compositions were studied. Co_3O_4 (Alfa Aesar 99.7%) , $SrCO_3$ (Aldrich 99.9%) and CuO (Aldrich 99.99%) were used as starting reagents. The powders were thoroughly mixed in an agate mortar and calcined at $900 \pm 5^\circ C$ for 25h. After grinding, 1 g pellets with 12 mm diameter were pressed under a pressure of 1.8 kbar and sintered at least twice at $900 \pm 5^\circ C$ for 60h with intermediate grinding and repressing. The samples were air-quenched at the end of each sintering step. All manipulations and heat treatments were performed in air.

The phase content of the pellets was checked after each sintering step by X-ray diffraction in a STOE diffractometer using CuK_α radiation. In some cases, additional heat treatments were performed in order to reach equilibrium, which was considered as achieved when no differences were detectable in the XRD patterns after two consecutive heat treatments. Si powder was added as an internal standard for lattice parameter determination.

Electrical resistivity measurements were performed with a current of 1 mA by the 4 contacts method on samples cut into parallelepiped shapes with $1.5 \times 1.5 \text{ mm}^2$ cross-section and 8 mm length. Gold wires were attached with silver paste cured at $200^\circ C$.

Results and discussion

(1) $CuO - SrO$

In this system, the three binary oxide phases Sr_2CuO_3 , SrCuO_2 and $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41-\delta}$ were formed in full agreement with previous studies of the binary $\text{SrO} - \text{CuO}$ phase diagram [13-18] as well as pseudo-ternary systems containing SrO and CuO for which phase equilibria have been established in air at $900^\circ\text{C} - 930^\circ\text{C}$ [7,9,33-38].

(2) $\text{CoO}_x - \text{CuO}$

The XRD patterns of the samples with Cu-rich nominal compositions $\text{Cu}_{1-x}\text{Co}_x\text{O}_{1+\delta}$ ($0.00 \leq x \leq 0.06$) are shown in Fig. 1. They reveal a single phase up to $x = 0.04$ with progressive shift of most reflections as the Co content is increased. The lattice parameters are listed in Table 1. The β angle and the c-axis length are not changing significantly, contrary to the a and b lattice parameters. The variation of these last two is illustrated in Fig. 2. While the a-axis length increases, the b-axis length decreases and both reach a constant value when impurity phases appear in the XRD patterns. From these data, it can be estimated that the solubility limit of Co in the tenorite CuO lattice is situated between 4 at.% and 5 at.% of Cu, probably closer to 4 at.%. This supports the results of Zabdyr and Fabrichnaya [22].

For $0.05 \leq x \leq 0.64$, the $\text{Cu}_{0.96}\text{Co}_{0.04}\text{O}_{1+\delta}$ composition is in equilibrium with the rock-salt Cu-Co-O solid solution. The upper solubility limit of Cu in the latter phase corresponds to 36 ± 2 at.% substitution for Co, in close correspondence to the values published by Driessens et al. [20] (≈ 33 at.%) as well as Zabdyr and Fabrichnaya [22] (≈ 38 at.%) at 900°C . As illustrated in Fig.3, the rock-salt solid-solution extends from $x \approx 0.65$ to $x \approx 0.92$ in $\text{Cu}_{1-x}\text{Co}_x\text{O}_{1+\delta}$. The cubic lattice parameter of this solid solution (Table 1) is not dependant on the Cu:Co ratio within the accuracy of the calculations. For Co-rich compositions, a two-phase equilibrium appears at $x \approx 0.94$ in $\text{Cu}_{1-x}\text{Co}_x\text{O}_{1+\delta}$, involving the rock-salt solid-solution and a cubic-spinel $\text{Co}_{3-y}\text{Cu}_y\text{O}_{4+\delta}$ phase. This is in agreement with the data of Driessens et al. [20] for the temperature of 900°C , although these authors reported a significantly lower x value for the

transition between the two-phase equilibrium and the single rock-salt solid-solution (0.83 versus ≈ 0.94 in the present work. Close to the pure cobalt oxide edge, Driessens et al. [20] reported Cu solubility up to 9 at.% for Co in the cubic-spinel phase at about 865°C, which decreases for increasing temperature and amounts to 1 -2 at.% at 900°C. In the present study the presence of a tiny single-phase field in the Co-rich corner could be confirmed by comparing the XRD patterns of samples with $\text{Co}_{98}\text{Cu}_1\text{Sr}_1$ and $\text{Co}_{96}\text{Cu}_2\text{Sr}_2$ nominal cation ratio (Fig. 4), which shows the appearance of $\text{Sr}_6\text{Co}_5\text{O}_{15}$ in the latter sample only. This is further supported by the slight reduction of the unit cell of the Co_3O_4 host lattice in the sample with $(\text{Co}_{0.99}\text{Cu}_{0.01})_3\text{O}_{4-\delta}$ nominal composition (Table 1).

At 900°C, the Co_3O_4 phase was found to be stable, a result which is in good agreement with published temperatures for the $\text{Co}_3\text{O}_4 \leftrightarrow 3\text{CoO} + 0.5\text{O}_2$ equilibrium in air ranging from 897°C to 920°C [20,24,39-42].

(3) CoO_x - SrO

After equilibration at 900°C for a total of 145h, the sample with SrCoO_{3-x} nominal composition was found to consist of a mixture of $\text{Sr}_6\text{Co}_5\text{O}_{15}$ and Co_3O_4 , confirming the results published in [20,22,24,27]. Similarly, the $\text{Sr}_3\text{Co}_2\text{O}_{6.33}$ nominal composition resulted in a two-phase sample containing $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and SrO , supporting the fact that $\text{Sr}_3\text{Co}_2\text{O}_{6.33}$ is only stable above 900°C [24]. A similar result was obtained for the $\text{Sr}_4\text{Co}_3\text{O}_9$ nominal composition. In contrast, both the $\text{Sr}_6\text{Co}_5\text{O}_{15}$ and the $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ phases were formed at 900°C. These compounds correspond to the $\alpha:\beta = 3:3$ and $9:5$ members of the $(\text{A}_3\text{Co}_2\text{O}_6)_\alpha(\text{A}_3\text{Co}_3\text{O}_9)_\beta$ family in the notation of Boulahya et al. [30].

Two samples with compositions intermediate between $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ (= $\text{Sr}_{6.36}\text{Co}_5\text{O}_{15+\delta}$) and $\text{Sr}_6\text{Co}_5\text{O}_{15}$ (i.e. $\text{Sr}_{6.25}\text{Co}_5\text{O}_{15+\delta}$ and $\text{Sr}_{6.13}\text{Co}_5\text{O}_{15+\delta}$) have been prepared to assess the presence of a two-phase equilibria between those 2 compositions. Fig. 5 shows a detail of the XRD pattern of these samples and of those

with $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ as well as $\text{Sr}_6\text{Co}_5\text{O}_{15}$ compositions after equilibration at 900°C and air quenching. This 2θ interval contains one of the most intense, non-overlapping reflections of the $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$ XRD patterns. From this figure, it can be concluded that there is in fact a single-phase solid solution region between the $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$ compositions, because the intermediate nominal stoichiometries do not result in superposition of the two individual diffraction patterns. Instead, a progressive shift of the reflection appears, with intermediate values for the $\text{Sr}_{6.25}\text{Co}_5\text{O}_{15+\delta}$ and $\text{Sr}_{6.13}\text{Co}_5\text{O}_{15+\delta}$ compositions and therefore variations of the lattice parameters. This seems at first sight to contradict the results of Jankovský et al. [24], who found a two-phase region between two crystallographically distinct stoichiometric compounds: $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$. This discrepancy is however only apparent. There is indeed a significant difference in the preparation conditions between the present work, where the samples were rapidly cooled by air-quenching and the study of Jankovský et al. [24], who performed slow cooling at 1°C/min.

In order to demonstrate that the processing conditions have a non-negligible influence on phase equilibria in this area of the pseudo-binary $\text{CoO}_x - \text{SrO}$ system, the $\text{Sr}_{6.13}\text{Co}_5\text{O}_{15+\delta}$ sample was post-annealed at 600°C for 60 h and furnace cooled. Fig. 6 shows that the full width at half maximum of the XRD peak centred at 44.2° in this sample after initial equilibration at 900°C and air-quenching, has increased from 0.23° (initial state, XRD pattern a in Fig.6) to 0.35° after the post-annealing treatment at 600°C (XRD pattern b in Fig. 6). Furthermore, we note a splitting of the (208) and (205) reflexions belonging to the $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$ phases respectively after annealing at 600°C. A peak displacement and separation into two reflections ((128) and (125) from $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$ respectively) is also observed. This shows that a two-phase equilibrium has been achieved. However, performing a new

annealing at 900°C on the same sample and cooling it fast by air-quenching restores the initial XRD pattern. It can thus be concluded that at 900°C, there is a continuous solid-solution between the $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$ compositions (that shall be denoted as $\text{Sr}_{6+x}\text{Co}_5\text{O}_{15+\delta}$ ($0 \leq x \leq 0.36$ in the following)), whereas a two-phase equilibrium reflects a lower temperature state. A phase separation must thus take place at a temperature lower than 900°C.

As will be shown in the next sub-section, this binary solid-solution extends into the ternary diagram by admitting Cu substitution and will be denoted as $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$.

(4) $\text{CoO}_x - \text{CuO} - \text{SrO}$

The tie-line compatibilities of phases in the $\text{CoO}_x - \text{CuO} - \text{SrO}$ system at 900°C are shown in Fig.7. This pseudo-ternary section consists of 6 three-phase regions and 6 two-phase fields. There are 2 solid solutions extending into the ternary system. The $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ solid solution dominates the system by being in equilibrium with all other phases and involved in most two-phase and three-phase fields.

There is no evidence for sizable Co solubility in Sr_2CuO_3 and SrCuO_2 under the present processing conditions. In contrast, Co can be substituted for Cu in the $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41-\delta}$ phase. Fig.8 shows the XRD patterns of the samples with $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ ($x = 0; 5$ and 6) nominal compositions. Up to $x = 5$, the samples exhibit a single phase diffraction pattern with displacement of the peak positions towards higher angles. However, reflections belonging to CuO and the $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ solid-solution appear for the $\text{Sr}_{14}\text{Cu}_{18}\text{Co}_6\text{O}_{41-\delta}$ nominal stoichiometry. The lattice parameters of the $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ phase are listed in Table 1 and plotted in Fig.9. These data show that the solubility limit of Co in the $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41-\delta}$ lattice is in fact close to $\text{Sr}_{14}\text{Cu}_{19}\text{Co}_5\text{O}_{41-\delta}$. Low temperature resistivity measurements performed on the samples with $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41-\delta}$ and $\text{Sr}_{14}\text{Cu}_{19}\text{Co}_5\text{O}_{41-\delta}$ compositions (Fig.10) show that

Co doping results in a lowering of the resistivity by nearly 2 orders of magnitude. Nevertheless, even the maximum Co content is not enough to induce a metallic behaviour. This confirms the results published by Yoshimitsu et al. [31].

The lattice parameters of a series of samples with $\text{Sr}_{6.25}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ nominal compositions are listed in Table 1 and plotted in Fig. 11). Their behaviour shows that up to about 22 at.% Cu can be introduced. Furthermore, the presence of a solid-solution rather than a two-phase equilibrium between $\text{Sr}_6\text{Co}_{5-x}\text{Cu}_x\text{O}_{15-\delta}$ and $\text{Sr}_{14}\text{Co}_{11-x}\text{Cu}_x\text{O}_{33-\delta}$ all the way up to the Cu solubility limit is evidenced by the single reflection around 44.2° in the XRD patterns of samples with $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ compositions ($0 \leq x \leq 0.36$; $0 \leq y \leq 1.0$) as illustrated in Fig. 12). Electrical resistivity measurements show that the $\text{Sr}_{6+x}\text{Co}_5\text{O}_{15+\delta}$ solid-solution is characterised by a semi-conducting behaviour similarly to data published for the undoped $\text{Sr}_5\text{Co}_4\text{O}$ (= $\text{Sr}_{6.25}\text{Co}_5\text{O}_{15+\delta}$) [28], while Cu doping results in a clear increase of the resistivity (Fig.10).

Defining the range of δ values in these two solid solutions is not straightforward. For $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$, assuming a $\delta = 0$ in $\text{Sr}_6\text{Co}_5\text{O}_{15}$ gives an average valency of +1.8 for Co. Rewriting this composition as $(\text{Sr}_3\text{Co}_2\text{O}_6)_3(\text{Sr}_3\text{Co}_3\text{O}_9)_3$ [30], it can be realized that the change in oxygen content resulting from the substitution of Cu will depend on the distribution of this element in the two non-equivalent Co sites. If all substituting Cu atoms are in the +2 oxidation state, as expected at 900°C in air, for the maximum solubility of $y = 1.0$ in $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$, the overall oxygen content will decrease by $\delta = -0.75$ at least and by $\delta = -1.0$ at most. Since the Sr (2+) content in this phase can vary between $x = 0$ and $x = 0.36$, it can be estimated that δ can vary between +0.36 ($x = 0.36$, $y = 0$) and -1.0 ($x = 0$, $y = 1.0$). For the $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ solid solution, the situation is more intricate, because “ $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41-\delta}$ ” corresponds in fact to an average cell made of the incommensurate superposition of CuO_2 and $\text{Sr}_2\text{Cu}_2\text{O}_3$ planes, with Cu in an average oxidation state greater than +2 [43]. The

effect of Co substitution on the oxygen content of this phase and thus on δ probably depends on the Cu sites (chains or ladders) on which Co substitutes. A realistic estimation of the δ range for the $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ solid solution will require specific measurements and/or accurate refinement of XRD diffraction patterns, which are beyond the scope of the present work.

(5) Comparison with related systems

Few systems including SrO, CoO_x and a transition metal oxide have been assessed. At 900°C, Fossdal et al. [44] only found $\text{SrCoO}_{3-\delta}$ as binary Sr-Co oxide phase in air. It forms a complete solid solution by substitution of Fe for Co up to $\text{SrFeO}_{3-\delta}$. In contrast, in the same system but at 1100°C in air, Aksenova et al. [45] report Fe solubility neither in $\text{SrCoO}_{2.5}$ nor in $\text{Sr}_3\text{Co}_2\text{O}_7$. This is different to the case of the $\text{CoO}_x - \text{NiO} - \text{SrO}$ phase equilibria at 1100°C in air, where Ni can be substituted for Co up to 15 at % in $\text{SrCoO}_{2.5+\delta}$ and 55 at.% in $\text{Sr}_3\text{Co}_2\text{O}_{7-\delta}$ [46]. SrCoO_x was also the only binary Sr-Co oxide phase reported by Surat et al. [47] at 600°C in a study of the $\text{CoO}_x - \text{SrO} - \text{V}_2\text{O}_5$ system. No vanadium can be introduced in SrCoO_x . In contrast to transition metal elements, which tend to substitute for Co in Sr-Co oxide phases, lanthanides appear to preferentially substitute for Sr, as shown e.g. by Volkova et al. [47] in the $\text{Sm}_2\text{O}_3 - \text{SrO} - \text{CoO}$ system.

An isothermal section of the $\text{CaO} - \text{CoO}_x - \text{CuO}$ system at 920°C was published by Miyazaki et al. [49]. It shows a ternary oxide phase with $[\text{Ca}_2(\text{Co}_{0.65}\text{Cu}_{0.35})_2\text{O}_4]_{0.62}\text{CoO}_2$ composition, which has no Sr-equivalent in the $\text{CoO}_x - \text{CuO} - \text{SrO}$ system at 900°C in air. Both Ca – Co binary oxide phases that are stable in pure O_2 at 920°C admit some Cu substitution for Co: 6 at.% in $\text{Ca}_3\text{Co}_2\text{O}_6$ and 12 at.% in $[\text{Ca}_2\text{CoO}_3]_p\text{CoO}_2$.

The $\text{CoO}_x - \text{CuO} - \text{BaO}$ system doesn't seem to have been explored in details but might be more complicated than the $\text{CoO}_x - \text{CuO} - \text{SrO}$ and $\text{CaO} - \text{CoO}_x - \text{CuO}$

systems in view of the numerous binary-oxide phases that are stable in the CuO – BaO pseudo-binary system in the 800°C – 1000°C temperature range [50,51].

Summary

The subsolidus relationship and phase formation of compounds in the CoO_x – CuO – SrO system were established at 900°C in air. The pseudo-ternary phase diagram is divided into 6 three-phase regions and 6 two-phase fields. No ternary oxide phase was found. Instead, two binary phases extend into the ternary system forming solid solutions. One is based on the $\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41-\delta}$ phase, in which up to 20 at.% Cu can be replaced by Co, which induces a significant decrease of the electrical resistivity, however without resulting in a transition to a metallic behaviour. The other can be described as $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ ($0 \leq x \leq 0.36$; $0 \leq y \leq 1.0$, with $-1.00 \leq \delta \leq 0.36$). In that case, the introduction of Cu into the host $\text{Sr}_{6+x}\text{Co}_5\text{O}_{15+\delta}$ lattice results in an increase of the electrical resistivity. Annealing a sample with $\text{Sr}_{6.13}\text{Co}_5\text{O}_{15+\delta}$ composition (i.e. within the $\text{Sr}_{6+x}\text{Co}_5\text{O}_{15+\delta}$ solid solution range) at 600°C followed by slow cooling resulted in a phase separation into $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$ and $\text{Sr}_6\text{Co}_5\text{O}_{15}$. The processing conditions thus appear to have a strong effect on the phase equilibria in the CoO_x – CuO – SrO system, because the $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ solid solution is involved in most two-phase and three-phase fields so that slow cooling may affect the topology of a significant area of the system.

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Figure captions

Figure 1: XRD patterns (detail) of samples with $\text{Cu}_{1-x}\text{Co}_x\text{O}_{1+\delta}$ ($0.00 \leq x \leq 0.06$) nominal compositions. Vertical arrows at the bottom of the figure indicate reflections from CuO.

Figure 2: a and b lattice parameters of the tenorite $\text{Cu}_{1-x}\text{Co}_x\text{O}_{1+\delta}$ solid-solution.

Figure 3: XRD patterns (detail) of samples with nominal compositions within and around the $\text{Cu}_{1-x}\text{Co}_x\text{O}_{1+\delta}$ rock-salt solid solution.

Figure 4: XRD patterns (detail) of samples with compositions in the Co-rich corner of the pseudo-ternary system.

Figure 5: Detail of the XRD patterns of samples with nominal compositions varying from $\text{Sr}_6\text{Co}_5\text{O}_{15}$ to $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$. This area of the XRD patterns includes several non-overlapping peaks and reveals that there is a solid solution between these two compositions. a: $\text{Sr}_6\text{Co}_5\text{O}_{15+\delta}$, b: $\text{Sr}_{6.13}\text{Co}_5\text{O}_{15+\delta}$, c: $\text{Sr}_{6.25}\text{Co}_5\text{O}_{15+\delta}$, d: $\text{Sr}_{6.36}\text{Co}_5\text{O}_{15+\delta}$ (= $\text{Sr}_{14}\text{Co}_{11}\text{O}_{33}$). The Miller indices correspond to the $\text{Sr}_6\text{Co}_5\text{O}_{15}$ structure [26]. The shoulder on the high-angle side of the (223) peaks is due to the $K_{\alpha 2}$ radiation, which was not subtracted to avoid possible artefacts that might arise as a result of mathematical manipulation of the data.

Figure 6: Detail of the XRD patterns of a sample with $\text{Sr}_{4.9}\text{Co}_4\text{O}_{12-\delta}$ nominal composition after equilibration at 900°C and air-quench (a); after further annealing at 600°C for 60h and furnace cooling (b); final equilibration at 900°C for 60h and air-quench (c). Miller indices in italic characters refer to the $\text{Sr}_5\text{Co}_4\text{O}_{12}$ reference XRD pattern [89-8305], whereas Miller indices in normal characters refer to the $\text{Sr}_6\text{Co}_5\text{O}_{15}$ reference XRD pattern [86-614].

Figure 7: Phase diagram of the $\text{CoO}_x - \text{CuO} - \text{SrO}$ pseudo-ternary system at 900°C in air. The studied compositions are marked by symbols: ● = single phase, ○ = two phases; ⊙ = three phases.

Figure 8: XRD patterns (detail) of the samples with $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ ($x = 0; 5$ and 6) nominal compositions. ● = $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$; ▼ = CuO.

Figure 9: Lattice parameters of the $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ phase versus Co-doping level.

Figure 10: Low temperature electrical resistivity of samples belonging to the $\text{Sr}_{14}\text{Cu}_{24-x}\text{Co}_x\text{O}_{41-\delta}$ solid solution (a) as well as to the $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ solid solution (b).

Figure 11: Lattice parameters of samples with the $\text{Sr}_{6.25}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ nominal compositions.

Figure 12: XRD patterns (detail) of samples with composition lying within the $\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ solid solution. a: $\text{Sr}_{6.00}\text{Co}_{4.75}\text{Cu}_{0.25}\text{O}_{15+\delta}$, b: $\text{Sr}_{6.12}\text{Co}_{4.75}\text{Cu}_{0.25}\text{O}_{15+\delta}$, c: $\text{Sr}_{6.25}\text{Co}_{4.69}\text{Cu}_{0.31}\text{O}_{15+\delta}$, d: $\text{Sr}_{6.00}\text{Co}_{4.50}\text{Cu}_{0.50}\text{O}_{15+\delta}$, e: $\text{Sr}_{6.12}\text{Co}_{4.50}\text{Cu}_{0.50}\text{O}_{15+\delta}$, f: $\text{Sr}_{6.25}\text{Co}_{4.38}\text{Cu}_{0.62}\text{O}_{15+\delta}$, g: $\text{Sr}_{6.00}\text{Co}_{4.25}\text{Cu}_{0.75}\text{O}_{15+\delta}$, h: $\text{Sr}_{6.25}\text{Co}_{4.06}\text{Cu}_{0.94}\text{O}_{15+\delta}$.

Table captions

Table 1: Phases observed in selected samples after equilibration and crystallographic data for the majority phases.

Figure 1

Figure 2

Figure 3

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Figure 11

Figure 12

Nominal cation ratio Co : Sr : Cu	Phases (XRD)*	Space group**	Lattice parameters***			
			a [Å]	b [Å]	c [Å]	β [°]
0 : 0 : 100	CuO	C2/c	4.686(2)	3.424(1)	5.132(2)	99.43(3)
1 : 0 : 99	CuO	C2/c	4.696(3)	3.410(2)	5.129(4)	99.68(6)
2 : 0 : 98	CuO	C2/c	4.705(2)	3.400(1)	5.129(2)	99.85(3)
3 : 0 : 97	CuO	C2/c	4.714(2)	3.392(1)	5.129(2)	100.02(3)
4 : 0 : 96	CuO	C2/c	4.724(2)	3.381(1)	5.128(2)	100.18(3)
5 : 0 : 95	CuO (Cu _{1-x} Co _x O _{1+δ} rock-salt ss)	C2/c	4.727(2)	3.379(1)	5.128(2)	100.11(3)
6 : 0 : 94	CuO (Cu _{1-x} Co _x O _{1+δ} rock-salt ss)	C2/c	4.728(2)	3.378(1)	5.128(2)	100.22(3)

60 : 0 : 40	Cu _{1-x} Co _x O _{1+δ} rock-salt ss (CuO)	Fd-3m	4.258(2)	-----	-----	-----
70 : 0 : 30	Cu _{1-x} Co _x O _{1+δ} rock-salt ss	Fd-3m	4.257(1)	-----	-----	-----
80 : 0 : 20	Cu _{1-x} Co _x O _{1+δ} rock-salt ss	Fd-3m	4.257(2)	-----	-----	-----
90 : 0 : 10	Cu _{1-x} Co _x O _{1+δ} rock-salt ss	Fd-3m	4.256(2)	-----	-----	-----
94 : 0 : 6	Cu _{1-x} Co _x O _{1+δ} rock-salt ss (Co ₃ O ₄)	Fd-3m	4.254(2)	-----	-----	-----

100 : 0 : 0	Co ₃ O ₄	Fm-3m	8.0848(9)	-----	-----	-----
99 : 0 : 1	Co ₃ O ₄ (Cu _{1-x} Co _x O _{1+δ} rock-salt ss)	Fm-3m	8.0826(9)	-----	-----	-----

Table 1

Table 1 (Cont.)

0.0 : 14.0 : 24.0	$\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$	Cccm	11.474(3)	13.408(3)	27.658(7)	-----
1.0 : 14.0 : 23.0	$\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$	Cccm	11.473(1)	13.398(1)	27.603(3)	-----
2.0 : 14.0 : 22.0	$\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$	Cccm	11.472(1)	13.384(1)	27.596(2)	-----
3.0 : 14.0 : 21.0	$\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$	Cccm	11.469(2)	13.378(2)	27.629(5)	-----
4.0 : 14.0 : 20.0	$\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$	Cccm	11.471(1)	13.369(1)	27.653(3)	-----
5.0 : 14.0 : 19.0	$\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$	Cccm	11.471(3)	13.356(3)	27.709(8)	-----
6.0 : 14.0 : 18.0	$\text{Sr}_{14}\text{Cu}_{24}\text{O}_{41}$ (CuO, $\text{Sr}_{6+x}\text{Co}_y\text{Cu}_y\text{O}_{15+\delta}$)	Cccm	11.453(2)	13.358(2)	27.754(3)	-----

5.00 : 6.25 : 0.00	$\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$	P3c1	9.471(14)	-----	20.106(15)	-----
4.69 : 6.25 : 0.31	$\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$	P3c1	9.466(20)	-----	20.193(31)	-----
4.38 : 6.25 : 0.62	$\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$	P3c1	9.469(15)	-----	20.257(17)	-----
4.06 : 6.25 : 0.94	$\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$	P3c1	9.460(11)	-----	20.302(16)	-----
3.75 : 6.25 : 1.25	$\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$	P3c1	8.448(25)	-----	20.329(39)	-----
3.44 : 6.25 : 1.56	$\text{Sr}_{6+x}\text{Co}_{5-y}\text{Cu}_y\text{O}_{15+\delta}$ (Sr_2CuO_3 , SrCuO_2)	P3c1	8.444(39)	-----	20.337(62)	-----

* Phases between brackets are minority phases

** Space group of the majority phase

*** The lattice parameters are those of the majority phase

Table 1 (end)