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Published in:
IEEE Journal of Photovoltaics

Link to article, DOI:
10.1109/JPHOTOV.2016.2603841

Publication date:
2017

Document Version
Peer reviewed version

Link back to DTU Orbit

Citation (APA):

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Application of photocurrent model on polymer solar cells under forward bias stress

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Abstract—We performed constant current stress at forward bias on organic heterojunction solar cells. We measured current voltage curves in both dark and light at each stress step to calculate the photocurrent. An existing model applied to photocurrent experimental data allows the estimation of several parameters such as generation, recombination, dissociation rate and nearly zero field voltage within the active layer as a function of the stress time. The analysis of extrapolated parameters shows that the stress mainly affects the recombination rate of the polaron charge transfer states.

Index Terms—Heterojunctions, Organic Semiconductors, Annealing, Stress, Current, Solar energy, Photovoltaic cells, Roll-to-Roll.

I. INTRODUCTION

The device efficiency and the speed of fabrication process of polymer solar cells were significantly improved during the last few years and many research group are today looking at them with a growing interest as a low-cost and eco-sustainable alternative to common solar cells in some applications [1]-[4]. In order to extract the performance parameters (efficiency, fill factor, short circuit current and open circuit voltage) of samples under accelerated stress, the most common way is to carry out periodic current-voltage (I-V) measurements [5]-[8]. However, even though these common figures of merit are immediate indicators of the cell performance, they cannot give a comprehensive picture of the several physical parameters, which are critical for the cell energy conversion efficiency. Among them, are the mobility, the polaron separation efficiency, the built-in potential, etc. A more advanced analysis is therefore needed in order to have better understanding of the complex behavior of such parameters. The accurate extrapolation and analysis of photocurrent [9]-[11] and the study of the impedance spectroscopy [12],[13] – for example – represent further investigation tools in organic heterojunction solar cells that can reveal the behavior of important physical parameters such as generation rate, polaron charge transfer states separation and recombination rate, built-in potential and carrier lifetime.

During the operational life of a photovoltaic module, several factor may concurrently contribute in the loss of the cell performances. For example, light exposure, high temperature, non-optimal electrical operative conditions and electrostatic discharge (ESD) are just a few of the possible reasons that lead to the cell degradation during its operating conditions. In particular, light exposure is especially critical in flexible organic photovoltaic. In fact, in standard solar cell module, clouds and dust are the main source of shading; however, in organic photovoltaic module also the architectonic application on curved surfaces is responsible for partially shadowing cells. Thus, illumination conditions might be not optimal and not uniform over the whole module, due to architectonic constrictions. These conditions may force the shaded or partially shaded cells in the module to operate in forward or reverse bias. This may negatively affects the reliability of the whole panel.

In this work, we analyzed the evolution of the above cited parameters during accelerated electrical stress in forward bias condition. We estimated them by applying an existing photocurrent model and we investigated the parameters behavior during the stress. Forward bias stress emulates the situation of a partially shaded module, when a cell is brought to forward bias due to the module connections.

II. EXPERIMENTAL AND DEVICES

We assembled the 1-cm² active area cells in roll-to-roll compatible process with a mini-roll coater [14]. The front electrode (Flextorex) is composed of an Ag grid, PEDOT:PSS and ZnO, and the back electrode consists of PEDOT:PSS and the Ag grid encloses the blend of P3HT:PCBM

We applied forward bias accelerated stress at 70mA/cm², 100mA/cm², and 150mA/cm² constant currents (CCS) in dark and under illumination. We systematically paused the stress to monitor devices conditions by means of I-V measurements in both light and dark. We performed I-V with a voltage from -2.5V to 1V. The total stress time was 7h. An Agilent E5263A Parameter analyzer was used for both the I-V measurements and the stress. We illuminated the cells by using a white LED because the measurement noise floor generated by white LED is much lower, compared to a xenon solar simulator. Besides, we used white LEDs because of its very low content in UV wavelengths and low power.
dissipation. These properties of the LEDs allow a reduction of the degradations induced by the light source (UV and thermal effects) so that we could better isolate the sole effect of the CCS on the devices. We calibrated the LED intensity to reach a cell illumination level equivalent to that obtained by a solar simulator at 1 sun. We verified that the short circuit current under LED illumination and solar simulator illumination at 1 sun have the same values, as well as all other important figure of merits (fill-factor, efficiency, etc). Finally, we used a PVE300 spectral responsivity analyzer to perform External Quantum Efficiency (EQE) measurements.

III. RESULTS AND DISCUSSIONS

A. Figures of merit degradation during CCS

The devices we build reach an average efficiency of 1.2-1.3% with an open voltage of 0.55V and an average short circuit current density of 5 mA/cm² [2]. Although the efficiency is lower than other polymeric organic solar cell devices reported in literature [15]-[18], we underline that we do not process these devices under controlled environment. Indeed, we use a semi-automatic mini-roll coater under environmental air. The usage of a glove-box and a spin-coater would probably increase such efficiency, allowing the reaching of higher performances. However, glove-box processing and devices spin-coating are not the real conditions applied during roll-to-roll mass production. Thus, both the uncontrolled environment and the not fully automatized process may lead to a efficiency reduction. On the other hand, such devices are closer to the cells built on real photovoltaic modules since they undergo the same processing [1].

Figs. 1a and 1b show the evolution of the short circuit current density ($J_{SC}$) and normalized efficiency ($\eta$) as a function of the stress time, respectively. In Fig. 1a we notice that, independent of the applied stress current, all the CCS induced a monotonic decrease of the $J_{SC}$ and the rate of decay was increasing with the stress current. Noticeably, for the larger stress current value (150 mA/cm²) under illumination (open red triangles), the decay rate seems to slow down during the last stress steps, likely due to an annealing process, which partially compensates the CCS-induced degradation. In fact, the cells temperature reached up to 90°C at 150 mA/cm² [8]. The self-heating induced by power dissipation during the stress, induced a partial recovery of the short circuit current density, at least for a stress as long as 25000 seconds.

The efficiency shows a behavior similar to the short circuit current. In Fig. 1b we plot the efficiency evolution normalized to the fresh value. Although efficiency generally decreases with increasing the stress time and current, there is a small recovery during the last stress steps for high stress current values (150 mA/cm²), more accentuated under illumination, due to the additional temperature increase induced by the light exposure. This is due to the high temperature reached during the stress, which results in partial annealing of the damage generated in the first part of the stress.

![Fig. 1. Short circuit current density (a) and normalized efficiency (b) as a function of stress time, during CCS.](image_url)

B. Photocurrent model description

To further investigate the mechanisms behind the degradation/recovery during CCS, we calculated the photocurrent as the difference of light and dark currents:

$$ J_{PH} = J_{LIGHT} - J_{DARK} \quad (1) $$

Where $J_{PH}$ is the photocurrent, $J_{LIGHT}$ is the current density measured under illumination and $J_{DARK}$ the current measure in dark. In order to obtain an accurate value of the photocurrent we also corrected the experimental data to account for the parasitic series resistance. The series resistance value was calculated by means of impedance spectroscopy [19], and it was continuously monitored during the stress. In all the devices, the series resistance ranges between 10Ω and 15 Ω, and it is almost constant during the stress. Remarkably, the current measured in our cells may approach 8mA, which may produce a voltage drop as large as 0.12V in the non-active regions (contacts, zinc oxide layer, etc.) This means that for a given voltage, the actual voltage drop across the active layer might be significantly different when the I-V is measured in dark and light conditions. For this reason, we corrected the I-V curves before subtracting $J_{DARK}$ to $J_{LIGHT}$. Fig. 2 shows the effect of the series resistance in the dark and the light I-V and the extrapolated photocurrent.
After series resistance correction, in order to fit to the experimental data we adopted the model proposed in [9], which expresses the photocurrent as the superposition of two contributions:

\[ J_{PH} = qGL \left[ \coth \left( \frac{V-V_{ZF}}{2VT} \right) - \frac{2VT}{V-V_{ZF}} \right] P \left( \frac{V-V_{ZF}}{L} \right) + J_D \]  

Equation (2) includes the Sokel-Hughes model for photoconductivity in insulators [20], the Braun-Onsager dissociation probability of polarons charge transfer states (P) [21] and a diffusion current contribution (J_D) firstly introduced by Ooi et al. [10],[11] and then employed also by Limpinsel et al. [9]. In (2), G is the average generation rate of polaron pairs (assumed constant all over the active layer); q is the elementary charge; L is the thickness of the active layer; V_T is the thermal voltage; V is the actual voltage drop across the active layer; V_{ZF} is the voltage corresponding to the nearly zero electric field within the active layer. The function P accounts for the separation probability of a bound polaron pair into two free polarons and it is electric field dependent. Finally, J_D is the current density contribution, which correspond to the current at V=V_{ZF}. V_{ZF} substitution to the built-in voltage and J_0 current density account for the non-ideal contacts and the non-constant electric field in the close proximity of the electrodes. Indeed, the Sokel-Hughes model considers photoconductivity in insulator where there is no charge accumulation. Thus, Ooi and Limpinsel included J_D and V_{ZF} terms in their models to take account for bend bending due to charge accumulation at interfaces. We invite the reader to refer to reference [9]-[11] for further details.

Following the adopted model, Fig. 3 represents a qualitative band diagram that helps understanding the carrier dynamics within the active layer at different operating voltages. Contact interfaces bend due to non-ideal alignment between the blend and the electrodes Fermi levels. The band bending generates two barriers at the contact interfaces preventing electrons flow toward the anode and holes flow toward the cathode. In other words, we may figure the electrodes as partially selective contacts [11]. The higher the barrier, the stronger is the selectivity of the contact. Fig. 3a describes the situation that occurs when the external applied potential keeps the bulk of the active layer at a nearly zero-field condition. We refer to this applied bias as V_{ZF}. In other words, within the active layer there is a quasi-flat band condition. Then, dissociated charges (electrons/holes) flow to the electrodes by drift in the region close to the contacts and by diffusion in the bulk of the active layer [9][10]. However, since there are selective interfaces that generate barriers, they do not flow equally to anode and cathode but they mostly reach the electrode with lower potential barrier. Thus, the photocurrent generated at V_{ZF} is not zero, giving raise to J_D. The absolute value of J_D relates to both the amount of free carriers generated and the height of the barriers. Fig. 3b shows the band bending when the photocurrent is zero. We refer as V_{PH0} to the voltage at which the photocurrent is zero. In this case, the model predicts that the band bending within the active layer compensates the barriers height. Thus, by applying V_{PH0}, electrons and hole can equally flow to both cathode and anode, resulting in a zero photocurrent. Although a more sophisticated modeling could improve the accuracy of V_{PH0} and V_{ZF}, as a first approximation, we can figure that the additional potential (defined \( \Phi_B \) in Fig. 3) required to move from the quasi flat band (Fig. 3a) to the zero-photocurrent condition (Fig. 3b) is correlated to the sum of the band bending at the two interfaces. We may estimate \( \Phi_B \) as the difference between V_{PH0} and V_{ZF}.

C. Parameter extraction

By fitting the photocurrent with (2), we extrapolated the parameters: J_D, V_{ZF}, \( \Phi_B \), G, k_{REC} and k_{SEP} as a function of the stress time, with k_{REC} and k_{SEP} the polaron recombination and separation rates respectively affecting the separation probability P as described by the Braun-Onsager theory [21].

Fig. 4 shows an example of the fitting results on a cell that underwent CCS at 70mA/cm^2 under light. We observe that when (2) is applied to photocurrent, it gives a very good fit of experimental data in both forward and reverse bias voltages. In Fig. 4, the series resistance used to account for contacts interfaces and other drops is 12Ω · cm^2 (measured by impedance spectroscopy), and it is compatible with the series resistance measured by other research groups [13], [22].

Figs. 5 and 6 show the evolution of J_D and \( \Phi_B \) respectively.
$J_D$ keeps decreasing until last step of stress. We must correlate the decrease of $J_D$ with the decreasing behavior of $Φ_B$, which is the difference between $V_{PHO}$ and $V_{ZE}$. The higher is $Φ_B$ the larger are the band benging – and in turn the sum of voltage drops – at the interfaces. The reduction of $Φ_B$ is a clear signature that the voltage drops and the barrier height near the contact are reducing. In turn, this contributes to reduction of the intensity of the diffusion current.

Of course, such a reduction could originate also from the mobility reduction, which affects the diffusion constant by the Einstein relation. However, we extrapolated the evolution of the mobility from the dark current, assuming a Space Charge Limited conduction through the organic layer, and we verified that mobility remains practically unchanged during stress with a value of $μ = 7.6 \cdot 10^3$ cm$^2$V$^{-1}$s$^{-1}$. For this reason, we can neglect the effect of mobility in the diffusion current.

Fig. 7 shows the correlation between the diffusion current $J_D$ and the potential $Φ_B$. Each correlation curve is a straight line. All curves are enclosed into a well-defined band, confirming that higher $Φ_B$ corresponds to higher $J_D$. Furthermore, as $Φ_B$ decreases during the stress, there is a corresponding reduction of $J_D$. In particular during CCS at 150 mA/cm$^2$ in dark (filled red triangles), when $Φ_B$ tends towards zero during last stress steps, $J_D$ gets close to zero as well. In fact, the disappearing of the barrier generates a non-selective contact and, in turn, the diffusion current at nearly zero-field voltage ($V_{ZE}$) vanishes.

Fig. 4. Photocurrent experimental data (symbols) and fitting results of model (2) (lines) corrected with a series resistance of 12Ω·cm$^{-2}$. The shown stress steps are from a CCS performed at 70mA/cm$^2$ in light.

Fig. 5. Diffusion current $J_D$ normalized to fresh value as a function of stress time.

Fig. 6. Potential $Φ_B$ as a function of the stress time.

Fig. 7. Correlation graph between the diffusion current $J_D$ and the voltage $Φ_B$ with stress time.
We related the variation of $V_{ZF}$ required to set the CCS current. This, in turn, slightly decreases the power dissipation, partially compensating the additional heating induced by illumination.

The decrease of $\Phi_B$ must be associated with the increase of $V_{ZF}$ shown in Fig. 8. We related the variation of $V_{ZF}$ during stress to the oxidation of P3HT [23], [24]. In fact, it has been already observed in literature, that the exposure of P3HT to oxygen increases the p-type doping, shifting the P3HT Fermi level toward the HOMO band. In turn, this reduces the band bending in proximity of the anode, as qualitatively described by the sketch in Fig. 9. Among the causes for the increase in P3HT doping, oxygen and moisture embedded during the fabrication process can be the primary candidates. In addition, they may also permeate the encapsulation layers reaching the active layer during device operation [25], [26]. The electrical stress may accelerate the oxidation process, increasing the effective doping and thus increasing the $V_{ZF}$ value. In fact, the higher the CCS current the higher the oxidation rate is. This may come from both the increase of the applied voltage required to maintain the imposed forward current and the temperature increase due to self-heating that can thermally assist the chemical reactions. Incidentally, in a previous work we measured that temperature may increase up to 90 °C during CCS at 150mA/cm$^2$ in dark [8].

The illumination during CCS produces only marginal changes, despite the additional device heating expected from the illumination. However, the presence of light during stress decreases the voltage required to set the CCS current. This, in turn, slightly decreases the power dissipation, partially compensating the additional heating induced by illumination.
Fig. 10 shows the voltage corresponding to the zero of the photocurrent as a function of the stress time. V_{PH0} = V_{ZF} + \Phi_b decreases with stress time due to the higher decrease of the potential \Phi_b compared to the increase of V_{ZF}.

When comparing the evolution of J_sc in Fig. 1a and J_o in Fig. 5 during stress, we observe a very different behavior. For instance, during CCS at 150 mA/cm² under illumination J_o keeps always decreasing down to almost zero, while J_sc slowly decreases with a saturating behavior after 10000 seconds. This clearly indicates that the decay of the short circuit current density cannot originate only from J_o, but also the generation rate and dissociation probability play important roles. However, the generation rate of polaron pairs G extrapolated from photocurrent is constant with stress time, independently on the CCS current or illumination conditions. We calculated that G = 1.08 \pm 0.07 \times 10^{21} \text{ cm}^{-3}\text{s}^{-1}. EQE measurements further confirms that G is constant. Fig. 11 shows the EQE as a function of radiation wavelength normalized on its area, for both fresh and stressed cells. No significant variations are observed, indicating that the absorption spectrum shape of the blend is constant during CCS. It is worth clarifying again that the reader should bear in mind that the absolute EQE for degraded sample is lower than for the fresh sample and here the normalized data is presented instead for better indication of no changes in the curve shape and thus in the absorption. This is a signature that no changes occur to the generation rate of bounded polaron pairs, confirming the idea that the stress does not affect G.

Since G is almost constant, the variation of the short circuit current must derive from the change of polaron recombination and/or separation rates. Following the Braun-Onsager theory the separation rate is [21]:

\[
k_{SEP} = k_{SEP0} \frac{j_1(2\sqrt{-2}\mathcal{F})}{2\sqrt{-2}}
\]

\[
k_{SEP0} = \frac{3q(\mu)}{4\alpha a^2\varepsilon} e^{-\frac{\Delta E}{kT}} b = \frac{q^3}{8\pi\varepsilon_0 kT^2} \tag{3}
\]

Where J_1 is the first order Bessel function, q is the elementary charge, a is the average molecular distance, \(\langle \mu \rangle\) is the average mobility \((7.6 \times 10^{-3} \text{cm}^2\text{V}^{-1}\text{s}^{-1} \text{ in our case}), \varepsilon \) is the electric permittivity, \(\Delta E\) is the exciton binding energy, kT is the thermal energy potential, F is the electric field. k_{SEP0} represents the charge transfer exciton separation rate at zero electric field.

Because k_{SEP} is primarily dependent on the mobility, we assumed k_{SEP0} almost constant. Its value obtained for all the CCSs at different currents is k_{SEP0} = 9.94 \pm 2.5 \times 10^{3} \text{ s}^{-1} calculated with \(a=1 \text{ nm} \) and \(\varepsilon=3 \varepsilon_0\). Instead, Fig. 12 shows the evolution of k_{REC}, i.e. the polaron recombination rate, which increases by increasing stress time in most of the samples. In some cases, such as during the CCS at 150 mA/cm² under illumination, k_{REC} start decreasing after 10000 seconds, i.e., the same time when the short circuit current saturates to the minimum value and the efficiency starts experiencing a partial recovery. Tentatively, we may ascribe the decrease of the recombination rate with the annealing of some morphological defects responsible for the exciton quenching, due to the high temperature reached during stress.

Again, this confirms that the recombination rate severely affects the cells performances, and it is one of the dominant effects driving the variation of the short circuit current and the cell efficiency, as well.

IV. CONCLUSIONS

In this work, we showed that the polaron recombination rate is one of the major reasons for the cell degradation during constant current stress in forward bias condition. Besides, our data and the model show that a correlation exists between the band bending at the interfaces and the photocurrent, and these banding contribute to cell performances together with the polaron recombination rate.

Even though the applied model is very simple and qualitative, it is still suitable for finding a relation between the cell degradation and the variation of some parameters, such as the exciton separation probability or the contact barrier heights. Of course, some limits still exist. For instance, it is impossible to extract the cumulative effects of the barrier height at the contacts, but it is not possible to distinguish and separate the contribution of the single barrier. For sure, the development of a more quantitative and complete model is worthy for a more detailed and accurate analysis, for quantifying better the role of interface degradation and the mechanisms behind the photocurrent generation. This will be our next step in future works.

REFERENCES


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