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Evaluation of the Tracking Accuracy of Parabolic-Trough Collectors in a Solar Plant for District Heating

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Abstract. The solar tracking system is a device which orients solar concentrating systems in order to allow the focusing of the solar radiation on the receiver along the day. The accuracy of the solar tracker is a key parameter when compared to the acceptance angle of the concentrator in order to maximize the optical efficiency. The Taars solar heating plant was put into operation in Denmark in summer 2015 with a PTC solar field. The accuracy of the tracking system of the 6 PTC rows has been studied.

INTRODUCTION

Denmark is the country with the highest use of solar plants for district heating applications[1]. Most of the collectors used in existing large solar heating systems are flat plate collectors (FPC). Meanwhile, parabolic-trough collectors (PTC) are the most mature and prominent technologies for solar thermal power plants. A novel solar heating plant was put into operation in July 2015 in Taars, Denmark, combining 4039 m² of parabolic-trough collectors (PTC) with 5960 m² of flat plate collectors (FPC). Previous studies show the performance of the plant, both the PTC and FPC collectors [2-4].

![FIGURE 1. Scheme of the tracking error analysis](image-url)
In the present study only the PTCs were studied. Many studies done in the last decade have already characterized the PTC efficiency [5-8], but few on site efficiency studies focused on the tracking error estimation of the PTC trackers [9-11]. Fig. 1 presents a summary of the acceptance angle as described in [11] as the angle until which the tracking errors do not have a significant impact on the PTC efficiency.

Previous studies also give the state-of-the-art of the methodologies available to characterize the tracking error of concentrating-tracking collectors and its influence on the solar collector efficiency [12-13].

The acceptance angle is a key parameter of the concentrator. The suitability between the acceptance angles with the tracking angles was checked and the tracker was determined to be accurate.

MATERIAL

A solar heating plant with 4039 m² PTC, in series with FPC collector field, has been constructed by Aalborg CSP A/S in Taars, in the northern part of Denmark [3,4] (longitude 10.12ºE, latitude 57.39ºN). This study analyses the tracking error of this PTC solar field. See Fig. 2 for a general view of the plant and the PTC collectors. The PTCs are manufactured by Aalborg CSP A/S, using receiver tubes manufactured by Archimede Solar Energy [14], and reflectors manufactured by Rioglass [15]. The receiver model is the product name HCEOI-12, with a nominal length of the receiver tube of 4060 mm (at ambient temperature); an absorber tube outer diameter of 70 mm, and a glass tube thickness of 2 mm. The reflector type is Mirror Type LS-3. Each collector length is 12 m, each row length is 124.457 m, and the collector aperture width is 5.774 m (See Fig. 2 for a view of the collectors and Table 1 for more specifications).

The PTCs track the sun in the transversal direction of the tube, and are oriented close to North-South direction. The orientation of the PTCs is slightly deviated from the North-South direction by 13.35º-13.37º. The exact orientation of each PTC row was estimated by topography study with a precision of ±0.001º. The inclinometer used to measure the PTC rotation is manufactured by Gemac. The data for the position of each of the 6 collectors were registered every 2 minutes by an inclinometer, positioned on the collector structure at the drive station in the center of the row.

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Absorber tube outer diameter (d) (m)</td>
<td>0.070</td>
</tr>
<tr>
<td>Absorber tube inner diameter (m)</td>
<td>0.066</td>
</tr>
<tr>
<td>Absorber tube solar absorptance (%)</td>
<td>96.0</td>
</tr>
<tr>
<td>Glass tube with anti-reflective solar transmittance (%)</td>
<td>96.5</td>
</tr>
<tr>
<td>Glass envelope outer diameter (m)</td>
<td>0.125</td>
</tr>
<tr>
<td>Glass envelope inner diameter (m)</td>
<td>0.119</td>
</tr>
<tr>
<td>Parabola width (w) (m)</td>
<td>5.77</td>
</tr>
<tr>
<td>Reflectors reflectance (%)</td>
<td>94.5</td>
</tr>
<tr>
<td>Numbers of modules per row</td>
<td>10</td>
</tr>
<tr>
<td>Mirror length in each module (m)</td>
<td>12</td>
</tr>
<tr>
<td>Geometrical concentration ratio (C_{geo} = w/(\pi d))</td>
<td>26.24</td>
</tr>
</tbody>
</table>
METHODOLOGY

This study presents an analysis of the accuracy of six single-axis solar trackers of the PTC field in a solar plant for district heating.

First, the estimation is based on the measurement of inclinometers $\alpha$ mounted on the collector structure, as defined in Standard IEC 62862-3-2 [17]. The data analyzed are for more than one year (10/08/2015 to 17/11/2016) with a large range of incidence angles. For all data points the transversal and the longitudinal angles were calculated based on the sun position using the algorithm given by Blanco-Muriel [18]. A filter was applied to select the daily data (solar elevation $h_s>0^\circ$; $\alpha>-100^\circ$; $\theta_T<20^\circ$; DNI > 0 W/m$^2$).

In order to check the accuracy of the solar tracker with a solar concentrator a definition of the acceptance angle should be defined. As for an ideal concentrating system, all the solar radiation entering with an incident angle smaller than this acceptance angle goes directed towards the receiver; whereas in a real solar collector, some optical losses exist due to optical properties, imperfections of materials, the size of the sun, the intercept factor, and the geometric imperfections. For this reason, using an accurate enough solar tracker is of high interest for the solar concentrator. The beam radiation IAM $K_b(\theta_T)$ crosses a limit threshold when exceeding the acceptance angle $\theta_a$. The theoretical acceptance angle $\theta_a$ is defined for a PTC as described in Eq. 1, where $\Phi_r$ is the rim angle of the parabola and $C_{geom}$ is the geometric concentration ratio [19]. The defocus angle $\theta_d$ is defined as the limit angle at which all the rays will miss the receiver, and is calculated by Eq. 2

$$\theta_a = \frac{\sin(\Phi_r)}{\pi C_{geom}}$$  \hspace{1cm} (1)

$$\theta_d = \sin^{-1}\left(\frac{2 \cdot \tan\left(\frac{\Phi_r}{2}\right)}{\pi C_{geom}}\right)$$  \hspace{1cm} (2)

Thus, the dependency of tracking error angle on the optical efficiency has also been determined by ray-tracing simulations. A ray-tracing model was implemented in the software Tonatiuh, previously presented and validated experimentally [20]. Thus, the transversal and longitudinal incidence angle modifier IAM, $K_d(\theta_T, \theta_L)$, are estimated using a ray-tracing program. See Fig. 3 for a view of the PTC of the collector and its model in Tonatiuh.

In the ray-tracing program developed, the geometry of the solar concentrator is described by discrete elements with triangular surfaces. In this program four kinds of surfaces have been introduced: specular surfaces, opaque surfaces, interface surfaces (to implement glasses) and absorber surfaces (the receiver). The program calculates ray trajectories from one source (called the sun window) that emits to all the surfaces of the system, and only beam radiation is taken into account. The angular size of the sun has been modeled according to the Buie equations [21],
and Fresnel effects are handled using a Monte Carlo approach. This program can calculate the optical efficiency and the radiation flux distribution on the absorber.

For the estimation of the optical efficiency of the collector, first angle dependencies of optical properties are considered. The collector is simulated fixing the longitudinal angle and changing the transversal angle, in order to see how these dependencies affect the efficiency. The angular dependencies of the optical properties are calculated with the next expressions. The transmittance of the cover $\tau(\theta)$ dependence curve of the incidence angle is according to [22], and the normal value according to manufacturer $\tau(0^\circ)=0.99$, as in Eq. 3.

$$\frac{\tau(\theta)}{\tau(0^\circ)} = 1 - \tan^{5.1}\left(\frac{\theta}{2}\right)$$

(3)

The reflectance of the reflectors dependence curve of the incidence angle is according to [23], and the normal value according to manufacturer $\rho(0^\circ)=0.94$. The absorptance of the receiver dependence curve of the incidence angle is according to [24], and the normal value according to manufacturer $\alpha(0^\circ)=0.94$, as in Eq. 4.

$$\frac{\alpha(\theta)}{\alpha(0^\circ)} = 1 - 0.017\left(\frac{1}{\cos \theta}\right)^{1.8}$$

(4)

The collector behaviour is simulated for angles from $0^\circ$ to $90^\circ$ in intervals of $10^\circ$ in the longitudinal angle axis and from $0^\circ$ to $2^\circ$ in intervals of $0.2^\circ$ in the transversal angle axis and the simulation is made with 10 million rays per iteration. The results are calculated with the information about photons that intersect with the receiver.

The optical efficiency is calculated with Eqs. 5 and 6:

$$\eta_{opt} = \frac{P_{receiver}(\theta_i)}{P_{incident}(\theta_i)}$$

(5)

$$P_{incident}(\theta_i) = G \cdot A_G \cdot \cos(\theta_i)$$

(6)

The IAM for any incidence angles, transversal and longitudinal $K_b(\theta_t, \theta_L)$, is calculated with Eq. 7:

$$K_b(\theta_t, \theta_L) = \frac{\eta_{opt}(\theta_t, \theta_L)}{\eta_{opt}(0^\circ, 0^\circ)}$$

(7)

RESULTS

From the PTC dimensions, and according to the theoretical formulas Eqs. 1 and 2, the acceptance angle $\theta_a$ is 3.8 mrad (0.22°) and the defocus angle $\theta_d$ is 6.1 mrad (0.35°). The distribution of different incidence angles (tracking/transversal angle versus longitudinal angles) are presented in Fig. 4 with green dots, and the acceptance angle and defocus angle are shown with un-continuous lines. The longitudinal incidence angle change along the day from values from $0^\circ$ to more +/-80°.

As seen in Fig. 4, the green dots are within the limit of the defocus angle lines, which means that for the 6 trackers, the tracking error (transversal angle) are mostly within the defocus angle $\theta_d$ (0.35°). However, some tracking errors higher than $\theta_d$ and up to 1° were observed (in the part top left of each graph inside the red ellipse). But those points were detected to be for days before 18/09/2015 when some tracking adjustment were done. It was observed that the behaviour of trackers nº 1–4 was similar, and that the trackers nº 5 and 6 had a similar behaviour too. Comparing to previous studies [16, 24], the tracking error lower than 0.5° is in line with normal PTC trackers behaviour.
FIGURE 4. Tracking error distribution for the six solar trackers

Tracker n° 1

Tracker n° 2

Tracker n° 3

Tracker n° 4

Tracker n° 5

Tracker n° 6

FIGURE 4. Tracking error distribution for the six solar trackers
Table 2 gives an overview of the maximum, minimum, mean and standard deviation of the tracker error along the day. From the standard deviation, it is seen than the tracking error is mostly lower than ±0.5º.

<table>
<thead>
<tr>
<th>Tracker nº</th>
<th>Min ( \theta ) [°]</th>
<th>Max ( \theta ) [°]</th>
<th>Mean ( \theta ) [°]</th>
<th>Stand. dev. ( \theta ) [°]</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>-0.55</td>
<td>0.48</td>
<td>-0.25</td>
<td>0.47</td>
</tr>
<tr>
<td>2</td>
<td>-1.47</td>
<td>1.30</td>
<td>-0.26</td>
<td>0.31</td>
</tr>
<tr>
<td>3</td>
<td>-0.49</td>
<td>0.67</td>
<td>-0.23</td>
<td>0.49</td>
</tr>
<tr>
<td>4</td>
<td>-0.53</td>
<td>0.20</td>
<td>-0.24</td>
<td>0.49</td>
</tr>
<tr>
<td>5</td>
<td>-0.51</td>
<td>0.87</td>
<td>-0.22</td>
<td>0.52</td>
</tr>
<tr>
<td>6</td>
<td>-0.62</td>
<td>0.50</td>
<td>-0.25</td>
<td>0.50</td>
</tr>
</tbody>
</table>

From the optical simulation with Tonatiuh, the values of IAM of different longitudinal and transversal angles were calculated and shown in Fig.5.

IAM is represented as functions of the longitudinal and transversal angle independently for a clearer view of the IAM variation.

![3D view of the longitudinal and transversal IAM obtained by ray-tracing](image1.png)

![View of the IAM as function of transversal incidence angle for different longitudinal angles](image2.png)

**FIGURE 5.** (a) 3D view of the longitudinal and transversal IAM obtained by ray-tracing (b) View of the IAM as function of transversal incidence angle for different longitudinal angles

The simulated transversal IAM \( K_s(\theta_t) \) is presented in Fig. 5b and it can be seen that it decreases for transversal angles \( \theta_t \) between 0.5º and 1º, which is a much larger range than the theoretical defocus angle calculated from Eq. 2. From this curves and the value from Fig. 4 it is estimated that the optical losses due to tracking error would be neglected.

Fig. 6 shows the power flux diagram on the perimeter of the receiver tube. It is seen in Fig. 6b how the distribution of the flux is moving around the tube perimeter while the transversal incidence angle is increasing.
CONCLUSIONS

Six PTCs rows with solar tracker used for district heating in Denmark were analyzed. The IAM was determined by optical simulation, in particular for transversal incidence angles in order to estimate the impact of the missfocusing of the tracker on the collector efficiency. The results show that the tracking error was most of the time lower than $\pm 0.2^\circ$ which is lower than the theoretical defocus angle of the concentrator. But, in some cases, the tracking error reaches more than $1^\circ$, which could cause some optical losses reducing the PTC performance.

ACKNOWLEDGEMENTS

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REFERENCES


17. Standard draft IEC 62862-3-2 “Solar thermal electric plants - Part 3-2: Systems and components - General requirements and test methods for parabolic-trough collectors” (publication planned in 2017).


