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# Model-based interpretation of groundwater arsenic mobility during in-situ reductive transformation of ferrihydrite

Lucien Stolze<sup>1</sup>, Di Zhang<sup>2</sup>, Huaming Guo<sup>2</sup>, Massimo Rolle<sup>\*1</sup>

<sup>1</sup> Department of Environmental Engineering, Technical University of Denmark, Miljøvej,

Building 115, 2800 Kgs. Lyngby, Denmark

<sup>2</sup> School of Water Resources and Environment, China University of Geosciences, Beijing 100083,

China

\*Corresponding author phone: +45 45252257; email: masro@env.dtu.dk



#### Abstract

1 Arsenic (As) release and mobility in groundwater is coupled to the iron (Fe) cycling and the 2 associated transformation of Fe-oxides present in sediments. Recent in-situ experiments have 3 provided observations on arsenic mobilization and co-occurring reductive mineral transformation 4 when placing As-loaded ferrihydrite-coated sand for 80 days in wells of an As-contaminated 5 aquifer of Northern China. However, the complex temporal change in solid-associated arsenic and the multiple geochemical processes occurring when the flowing groundwater contacts the 6 As-loaded ferrihydrite-coated sand hamper a detailed evaluation of the experimental dataset. In 7 8 this study, we develop a modeling approach that allows a quantitative interpretation of arsenic release and ferrihydrite transformation observed during the in-situ experiments. The model 9 accounts for the interplay of abiotic and biotic geochemical processes (i.e., surface complexation, 10 reductive dissolution, formation of secondary iron minerals and arsenic sequestration into the 11 12 newly formed minerals) involved in the transformation of Fe-oxides and controlling arsenic mobility. The results show the capability of the proposed approach to reproduce the temporal 13 trends of solid arsenic and ferrihydrite concentrations, as well as the spatial variability of mineral 14 transformation, observed in different wells using a common set of surface complexation 15 parameters and kinetic rate constants. The simulation outcomes allowed us to disentangle the 16 specific contribution of the different mechanisms controlling the release of arsenic. It was 17 possible to identify an initial rapid but minor release of As (13-23% of the initial surface 18 concentration) due to desorption from ferrihydrite, as well as the reduction of adsorbed As(V) to 19 As(III) upon contact with the flowing anoxic groundwater. Successively, reductive dissolution of 20 ferrihydrite caused the decrease of the amount of the Fe mineral phase and led to a major 21 depletion of solid-associated arsenic. The produced Fe(II) catalyzed the ferrihydrite conversion 22

into more crystalline Fe(III) oxides (i.e., lepidocrocite and goethite) through Ostwald ripening, and resulted in the formation of siderite and mackinawite upon reaction with carbonates and sulfides naturally present in the groundwater. The model results also showed that, whereas the decrease in surface sites during reductive dissolution of ferrihydrite promoted arsenic mobilization, the mineral transformation limited As release through its sequestration into the newly formed secondary mineral phases.

29

### 30 Introduction

Prolonged exposure to arsenic (As) contaminated groundwater affects the health of millions of 31 32 individuals in various parts of the world (1-3). This problem is particularly severe in South East Asia (4) where arsenic contamination primarily results from the reducing conditions prevailing in 33 the aquifers, triggering the dissolution of iron oxides present in the sediments and the 34 simultaneous release of As (5-8). The mobility of arsenic in groundwater is controlled by iron 35 minerals through sorption onto the mineral surfaces (9-13). Other important processes, such as 36 the reduction of arsenate to arsenite, can change the affinity for mineral surfaces and affect 37 38 arsenic mobility (14-16).

Significant effort has been devoted to the investigation of the cycling of iron oxides and its 39 fundamental implications on arsenic release and transport. Ferrihydrite, which has a high 40 41 capacity in hosting arsenic (17), has been detected in sediments of Bangladesh (18-19) and nearsurface sediments in the Mekong Delta (20) where groundwater arsenic contamination occurred. 42 This poorly crystalline oxide is reactive and can undergo microbially-mediated reductive 43 dissolution (21-22). Furthermore, ferrihydrite can adopt, over time, a more crystalline structure 44 (e.g., goethite), which causes a decrease in the As sequestration potential of the sediments (13). 45 The ferrous iron produced during the reductive dissolution of ferrihydrite can (i) abiotically 46 catalyze the crystallization of the Fe(III) oxide phases (23-26) and/or (ii) precipitate into Fe(II)-47 bearing mineral phases such as siderite, mackinawite, vivianite (12, 21, 27). Depending on the 48 type of secondary mineral phases, significant amount of arsenic can be sequestered through 49 adsorption and reincorporation leading to a disparity between the disintegration of ferrihydrite 50 and the arsenic release (28-32). 51

The interpretation and prediction of arsenic fate in the subsurface is particularly challenging as it 52 requires the consideration of the complex interplay between flow, reactive transport processes 53 and the hydrochemistry of the groundwater. Despite the large number of studies on arsenic 54 release and transport mechanisms an apparent research gap still exists between the level of 55 understanding of arsenic mobility under controlled laboratory conditions and under natural field 56 conditions. Laboratory studies typically limit the number of geochemical processes under 57 investigation using simplified aqueous composition and mineral assemblage. In contrast, natural 58 systems have a higher level of complexity due to the large number of geochemical factors and 59 co-occurring mechanisms. Hence, pilot-scale experiments, directly conducted in aquifer systems, 60 are of primary importance to bridge such knowledge gap between simplified laboratory setups 61 and complex field investigations. Recently performed pilot-scale experiments, injecting reactive 62 organic compounds to stimulate microbial activity in the subsurface, have provided insights on 63 the transformation of naturally-occurring mineral phases and their interactions with arsenic (33-64 34). Another experimental approach that has been adopted in pilot scale experiments consists in 65 assessing the change of known mineral phases exposed to natural groundwater conditions (33, 66 36-38). Furthermore, important insights and quantitative understanding of arsenic release and 67 68 transport processes are obtained when experimental observations are interpreted with numerical modelling both at laboratory (39-42) and at field scales (34, 43-45). 69

In this study, we develop a model to simulate the reductive transformation of synthetic ferrihydrite and concomitant release of pre-loaded arsenic exposed to natural groundwater conditions during in-situ experiments performed in an As-contaminated sedimentary aquifer of Northern China *(37)*. Such experiments have shown complex dynamics between arsenic release from ferrihydrite-coated sand and ferrihydrite dissolution/transformation at different spatial 75 locations. Using the implemented modeling framework, we provide a quantitative interpretation of the experimental datasets comprising (i) time series of total Fe and As solid-associated 76 concentrations, (ii) mineral composition at the end of the experiments and (iii) groundwater 77 hydrochemical data. The modeling outcomes highlight the distinct contribution and the 78 interactions of different geochemical processes controlling the mobilization of arsenic at the field 79 site. Such processes include surface complexation reactions, microbially-mediated reductive 80 dissolution, mineral transformation through Ostwald ripening, formation of secondary mineral 81 phases and As sequestration in the newly formed minerals, and determine the complex trends of 82 arsenic and iron observed at the field site. 83

#### 84 Materials and Methods

#### 85 Experiments and datasets description

The in-situ experiments were conducted in monitoring wells screened in a shallow reducing As-86 contaminated aquifer in the Hetao Basin (Inner Mongolia, China) and consisted in placing As-87 loaded synthetic iron mineral phases at screen depth (i.e., [18.5 - 26.2] m) for 80 days in order to 88 observe the effect of the continuous groundwater flow on the As retention and iron mineral 89 90 transformation. The ferrihydrite coated sand was synthetized according to the method of Schwertmann and Cornell (46) and the As loading was performed in the laboratory by using a 91 solid-to-solution ratio of 50 g/L and equilibrating the solid phase with a 500 mg/L As(V) 92 solution. The As-loaded coated sand had a porosity of 0.5, a Fe content of 2.71 mg/g coated sand 93 (i.e., 27 g ferrihydrite/L) and an As content of 213  $\mu$ g/g coated sand. 94

95 The coated sand was divided into amounts of 0.5 g before being deployed in the field, where water could flow homogeneously through the highly permeable porous medium. Periodic 96 sampling of the solid phase allowed measuring the temporal change in solid-associated As and 97 98 total Fe content after total digestion of the sample, using the microwave-assisted method of Link et al. (47). Reductive dissolution of ferrihydrite and release of arsenic occurred incongruently in 99 all wells as shown by the monitored transient decrease in Fe and As. Synchrotron X-Ray 100 diffraction (XRD) indicated that goethite formation occurred in all wells whereas presence of 101 lepidocrocite was less pronounced and differed among the wells. The difference in mineral phase 102 composition was confirmed by the scanning electron microscopy (SEM) exhibiting varying 103 degree of crystallization. In order to characterize the mineral phase composition and the As 104 oxidation at the end of the experiments, Fe and As K-edge X-Ray absorption spectroscopy 105 106 (XANES) was conducted at the BL14W beamline of the Shanghai Synchrotron Radiation Facility (SSRF) operated in the energy range [-50; 150 eV] with a Si(111) monochromator. Fe 107 K-edge XANES indicated significant formation of siderite and mackinawite during the 108 109 experiments. As K-edge XANES showed that the oxidation state of As adsorbed onto the ferrihydrite surface partially changed from As(V) to As(III). During the in-situ experiments, the 110 chemical composition of the groundwater was measured at 0, 30 and 80 days in each well. In this 111 study, we consider the datasets collected in 3 wells placed along the main groundwater flow 112 direction and separated by a distance of 2.5 km. The datasets include the average groundwater 113 composition for each well, the temporal change in solid-associated As and Fe, as well as the 114 quantification of the secondary mineral phases at the end of the experiments. Details about the 115 monitoring wells and field data are provided in the Supporting Information, whereas an extensive 116 117 description of the in-situ experiments is given by Zhang et al. (37).

#### 118 Modeling approach

The model simulates the groundwater flow through the ferrihydrite-coated sand leading to a 119 change from aerobic to anaerobic conditions, the continuous supply of dissolved groundwater 120 species, the mineral transformation, and the As release/sequestration. Figure 1 displays the 121 122 location of the 3 considered wells, and a visual representation of the conceptual framework for the proposed approach and of the key biogeochemical processes. The model accounts for a series 123 of processes triggered by the dynamic change in the hydrochemistry: the microbially-driven 124 reductive dissolution of ferrihvdrite, the formation of secondary Fe(II) and Fe(III) oxides mineral 125 126 phases, the change in As redox state, as well as the uptake of As through sorption onto iron oxide surfaces and sequestration into secondary mineral phases. 127



Figure 1. Illustration of the modeling approach for reductive transformation of ferrihydrite and As mobilization/sequestration during the in-situ experiments: (a) conceptual model; (b) location of the observation wells and simultaneous calibration approach through parallelization of simulations with a common set of parameters for the different spatial locations.

133 The first modeling steps consist in loading the arsenic onto the mineral surface by equilibrating ferrihydrite with the As concentrated solution used for the preparation of the reactive samples, 134 and defining the hydrochemical composition of the groundwater according to the field 135 136 measurements. Subsequently, the solution in contact with the As-loaded ferrihydrite is iteratively replaced by the groundwater solution to simulate the flushing of the pores due to groundwater 137 advection. The flow rates defined through the advective time steps were based on values found in 138 Stolze et al. (45) showing decreasing flow velocity along the flow line from the mountains 139 towards the flat plain (Supplementary Information, Table SI7). Following the transport step, the 140 surface complexation reactions and aqueous speciation are calculated assuming local equilibrium, 141 whereas the reductive dissolution of ferrihydrite, the transformation and precipitation of mineral 142 phases, and the change in As speciation were described as kinetic processes. Therefore, the 143 144 feedback/interaction of the flow and transport processes with the reaction network is directly taken into account in the description of the flow-through system. 145

The model was implemented by coupling the geochemical code PHREEQC-3 (48) with the software MATLAB<sup>®</sup> (49-50) using the IPhreeqc model (51-52). Such coupling results in a flexible modeling approach that combines the capabilities of PHREEQC to model solute transport, kinetic and equilibrium reactions with the advanced capability and functions of MATLAB<sup>®</sup> for data analysis, model calibration and optimization. We used the WATEQ4F thermodynamic aqueous reactions database, amended with the aqueous speciation reactions of arsenic from Dixit and Hering (17) (Table 1).

153

## 154 **Reaction network**

The model includes a series of abiotic and microbially-mediated reactions that aimed at describing the geochemical transformations taking place during the in-situ experiments. Table 1 lists the key reactions considered in the model. Ferrihydrite was represented with its simplified stoichiometry  $Fe(OH)_3$  for computational ease *(21)*. Secondary Fe(III) phases (i.e., goethite and lepidocrocite) were represented as a generic Fe(III) oxide (FeOOH).

160 Table 1: Aqueous speciation and geochemical reactions included in the reactive transport model

Aqueous speciation log K		
$AsO_4^{3-} + 3H^+ = H_3AsO_4$		20.06 <sup>(a)</sup>
$AsO_4^{3-} + 2H^+ = H_2AsO_4^{-}$		18.35 <sup>(a)</sup>
$AsO_4^{3-} + H^+ = HAsO_4^{2-}$		11.60 <sup>(a)</sup>
$A_{s}O_{3}^{3-} + 3H^{+} = H_{3}A_{s}O_{3}$		34.74 <sup>(a)</sup>
$AsO_3^{3-} + 2H^+ = H_2AsO_3^{-}$		25.52 <sup>(a)</sup>
$A_{s}O_{3}^{3-} + H^{+} = HA_{s}O_{3}^{2-}$		13.41 <sup>(a)</sup>
Reactive minerals	Name	log K
$Fe(OH)_3 + 3H^+ = Fe^{3+} + 3H_2O$	Ferrihydrite	4.891 <sup>(b)</sup>
$FeOOH + 3H^+ = Fe^{3+} + 2H_2O$	Fe(III) oxide	-1 <sup>(c)</sup>
$\mathrm{FeS} + \mathrm{H}^+ = \mathrm{Fe}^{2+} + \mathrm{HS}^-$	Mackinawite	-2.95 <sup>(d)</sup>
$FeCO_3 = Fe^{2+} + CO_3^{2-}$	Siderite	-10.89 <sup>(c)</sup>
Reductive dissolution of ferrihydrite		
$CH_2O + 4Fe(OH)_3 + 7H^+ \rightarrow HCO_3^- + 4Fe^{2+} + 10H_2O$		
Redox change in As speciation		
$0.5\text{CH}_2\text{O} + \text{HAsO}_4^{2\text{-}} + 1.5\text{H}^+ \rightarrow \text{H}_3\text{AsO}_3 + 0.5\text{HCO}_3^{\text{-}}$		
$0.5$ CH <sub>2</sub> O + Hfo <sub>w</sub> AsO <sub>4</sub> <sup>-2</sup> + $1.5$ H <sup>+</sup> $\rightarrow$ Hfo <sub>w</sub> H <sub>2</sub> AsO <sub>3</sub> + $0.5$ HCO <sub>3</sub> <sup>-2</sup>		
<sup>(a)</sup> (17), based on MINEQL+ database (53); <sup>(b)</sup> (54), <sup>(c)</sup> (55), <sup>(d)</sup> (56)		

161 *Dissolution and precipitation kinetics.* The mineral transformation reactions were controlled by 162 kinetics rate expressions defined by means of thermodynamic constraints and hydrochemical 163 composition (57). We considered the dissimilatory reductive dissolution of ferrihydrite by 164 oxidation of organic matter leading to the release of Fe(II) and HCO<sub>3</sub> (2, 21, 23). The kinetic rate 165 of the reaction was expressed as function of the abundance of the electron acceptor (i.e., the 166 ferrihydrite) with a Monod type rate equation *(41, 57, 58)*. Additional terms allowed us to 167 account for: (i) the decrease in accessibility for reactive surface sites during ferrihydrite 168 dissolution *(59)*, and (ii) the passivation of ferrihydrite via the adsorption of charged species *(60-169 61)*.

$$R_{\text{ferri}} = -k_{\text{ferri}} \left( \frac{\left[ \text{Fe(OH)}_3 \right]}{K_{\text{m}}^{\text{ferri-org}} + \left[ \text{Fe(OH)}_3 \right]} \right) \left( \frac{A_{\text{Fe(OH)}_3}}{A_{0, \text{Fe(OH)}_3}} \right) \left( \frac{S_{\text{tot}} - S_{\text{occupied}}}{S_{\text{tot}}} \right) L(t) \quad \begin{cases} L(t < t_{i, \text{ ferri}}) = 0\\ L(t \ge t_{i, \text{ ferri}}) = 1 \end{cases}$$
(1)

where  $k_{ferri}$  is the rate constant,  $K_m^{ferri-org}$  is the half-saturation constant,  $A_{Fe(OH)_3}$  and  $A_{0, Fe(OH)_3}$ 170 are the total surface areas of ferrihydrite at time t and t=0, respectively,  $S_{tot}$  is the total amount of 171 ferrihydrite surface sites, and Soccupied is the amount of ferrihydrite surface sites occupied by 172 Fe(II) (60), phosphate (61), As(V) (14, 16), silicates, and carbonates. As(III) was not included in 173 the surface site passivation term since it rather favors ferrihydrite dissimilatory reduction (14). 174 Quantities in brackets, [], represent the molar concentration of the indicated species. K<sub>m</sub><sup>ferri-org</sup> 175 was defined proportional to the amount of Fe(III) crystalline oxide formed during the in-situ 176 experiment, since this can limit ferrihydrite reactivity (23): 177

$$K_{m}^{\text{ferri-org}} = K_{m,0}^{\text{ferri-org}} \frac{[\text{FeOOH}]}{[\text{Fe(OH)}_{3}] + [\text{FeOOH}]}$$
(2)

178 where  $K_{m,0}^{\text{ferri-org}}$  is a calibrated variable.

L(t) expresses the inhibition of the reductive dissolution of ferrihydrite for each well over a time period t<sub>i, ferri</sub>, as the dataset indicated a lag phase preceding the decrease in the solid-associated Fe content. The abiotic reduction of ferrihydrite by sulfide was not considered in the model as it was not possible to distinguish its effect from the microbial reductive dissolution of ferrihydrite. The consumption of organic carbon was simulated according to the reactions and stoichiometry reported in Table 1. Organic carbon was not considered as limiting factor for the reaction kinetics due to its abundance in the flowing groundwater and to its reactivity in the area of the insitu experiment *(62)*.

The Fe(II)-catalyzed conversion of ferrihydrite into a more crystalline Fe(III) oxide phase (comprising goethite and lepidocrocite) occurs via Ostwald ripening (*16, 24, 63-64*). The kinetic rate,  $R_{Ostwald}$  considers the Fe(II) surface coverage (*21, 30, 65-67*), the dissolved Fe(II) concentration (*25-26, 68*), and the effect of chloride, sulfate, and bicarbonate concentrations since these ions have been shown to significantly slow down the crystallization of ferrihydrite (*69*):

$$R_{Ostwald} = -\left(k_1 \left(\frac{S_{Fe(II)}}{S_{tot}}\right) + k_2 \frac{[Fe^{2+}]}{[Fe(OH)_3]}\right) \left(\frac{[Fe(OH)_3]}{K_m^{ferri-ost} + [Fe(OH)_3]}\right) \left(\frac{1}{[CI^-] + [SO_4^{2-}] + [HCO_3^-]}\right)^x (3)$$

where  $k_1$  and  $k_2$  are rate constants,  $S_{Fe(II)}$  is the amount of ferrihydrite surface sites occupied by Fe(II), and x is a calibrated exponent. The abiotic dissolution of ferrihydrite resulting from electron transfer from aqueous Fe(II) is inhibited when the electrochemical potential of the redox couple Fe(II)/Fe(III) exceeds the absolute energy of the conduction band of ferrihydrite (i.e.,  $E_{Fe(OH)_3} = -5.00 \text{ eV}$ ) (25-26, 68). All produced Fe<sup>3+</sup> was turned into a single Fe(III) crystalline phase. Furthermore, the formation of magnetite was not considered as this mineral was not detected during the in-situ experiments.

200 Siderite and mackinawite were allowed to precipitate as products of the reaction of Fe(II) from 201 the reactive dissolution of ferrihydrite and dissolved carbonate and sulfide species present in the 202 flowing groundwater. The precipitation of these secondary minerals was controlled by the kinetic rate expressions: 203

$$R_{\text{sid-pptn}} = k_{\text{sid-pptn}} \max\left(0, \left[1 - \frac{K_{\text{sp(sid)}}}{IAP_{\text{sid}}}\right]\right)$$
(4)  
$$R_{\text{mack-pptn}} = k_{\text{mack-pptn}} \max\left(0, \left[1 - \frac{K_{\text{sp(mack)}}}{IAP_{\text{mack}}}\right]\right)$$
(5)

(5)

where K<sub>sp</sub> is the solubility product and IAP is the ion activity product. 204

Arsenic release and sequestration. The change in speciation of arsenic, from As(V) to As(III), 205 occurring when the reduced groundwater contacted the As-loaded ferrihydrite-coated sand, was 206 described as a linear kinetically-controlled mechanisms with a rate coefficient  $k_{\mbox{\scriptsize As}}.$  Sorption 207 reactions were assumed to be instantaneous and were modeled for ferrihydrite and the secondary 208 Fe(III) oxide using the diffuse double layer (DDL) model (70). Ferrihydrite was defined with a 209 specific surface area of 600  $m^2/g$  and with weak and strong adsorption sites (i.e., Hfo<sub>w</sub> and Hfo<sub>s</sub>, 210 respectively) (70). The secondary Fe(III) oxide was assumed to have the surface complexation 211 properties of goethite and was represented with a specific surface area of 54  $m^2/g$  and a single 212 type of surface sites (i.e., Goe) (71). The densities of surface sites Hfow and Goe were calibrated 213 within the range [0.05 - 0.31] mol/mol Fe (17, 72) and [0.011 - 0.018] mol/mol Fe (71), 214 respectively. The density of Hfos sites was set to 0.005 mol/mol Fe (70). Since the number of 215 surface sites are stoichiometrically linked to the mol of mineral phases, reductive transformation 216 of the mineral phases lead to a change in sorption capacity. The set of surface reactions for 217 218 ferrihydrite was taken from the (70) database and amended with arsenic (17, 73), silica (74), carbonates, and ferrous iron (75) surface reactions. Ferrihydrite and goethite surface reactions 219

included in the model with respective equilibrium constants are listed in Tables SI4 and SI5 of
 the Supplementary Information. The affinity constants for ferrihydrite were re-optimized through
 calibration using their 95% confidence intervals reported in the literature.

In addition to complexation onto Fe(III) mineral phases, As reincorporation into the crystalline oxides *(32, 76)* and/or adsorption onto siderite *(29)* were considered. These mechanisms were described through the uptake of total aqueous As (i.e., considering the relative proportion of As(III) and As(V)) by a linear sequestration rate stoichiometrically proportional to the amount of produced siderite and secondary Fe(III) oxide defined as:

$$R_{As-seq} = \alpha \left( R_{sid-pptn} + R_{Ostwald} \right)$$
(6)

where  $\alpha$  is the molar ratio of As sequestration. We assumed that no significant amount of As was sequestered by mackinawite (56, 77-78).

Calibration strategy. The modeling framework aimed at describing the reductive mineral 230 transformations and the As release at different spatial locations during the in-situ experiments. 231 We used a common set of parameters between the different spatial locations. Therefore, 232 calibration of the model parameters was performed simultaneously by parallelizing the 233 simulations of the considered observation wells (Figure 1b). The model parameters were 234 calibrated in the MATLAB<sup>®</sup> environment with an automated procedure minimizing the root 235 mean squared error (RMSE) between simulated and measured solid-associated species (i.e., total 236 As and total Fe) throughout the duration of the experiments. Also the secondary mineral 237 composition representative of the samples at the end of the in-situ experiments and determined 238 by Fe K-edge XANES measurements was included in the calibration. Due to the high number of 239

parameters and the non-linearity of the problem, the heuristic, global-search particle swarm
optimization (PSO) method was chosen to minimize the objective function (41, 79).

242

# 243 **Results and discussion**

*Model-based interpretation of the field observations.* The comparison between modeling results and field datasets, displayed in Figure 2, was performed in the three observation wells by considering the temporal change in total solid-associated arsenic (Figures 2a-c), the temporal change in total Fe content (Figures 2d-f), and the amount of iron oxides present in the mineral assemblage at 80 days (Figures 2g-i).



Figure 2. Comparison between experimental data and simulation results. (a)-(c) Dynamic change in total As (note that no sequestered As was predicted in well 2-4); (d)-(f) dynamic change in total Fe and mineral composition; (g)-(i) mineral composition at the end of the experiment: the

full and empty bars represent simulated and experimental results determined by XANES,
respectively. The error bars show 10% uncertainty on quantified mineral fractions for the
XANES data available for wells 5-2 and 4-5.

The field data suggest that multiple geochemical processes occurring over different time scales 256 257 control the As mobilization during the in-situ experiments. Indeed, the solid-associated As concentrations exhibit a complex behavior characterized by a significant and rapid release of 258 arsenic at early time followed by a plateau, particularly visible in wells 2-4 and 4-5, and a 259 subsequent more gradual release. In contrast, decrease in solid-associated Fe did not start when 260 261 the reactive mineral was exposed to the groundwater but after an initial delay, which was most pronounced in well 4-5. There is a clear consistency between the patterns of As and Fe contents 262 at the different monitoring locations. In particular, the onset of Fe reductive dissolution 263 corresponds to the time at which the arsenic trend shows a change in its slope and starts the 264 265 gradual decrease which continues throughout the duration of the experiments. The gradual decrease in solid-associated As and the disintegration of the iron mineral phase appears to 266 proceed congruently in wells 2-4 and 4-5. In contrast, in well 5-2 the Fe-content reaches steady 267 state after 40 days whereas the solid-associated As continues to decrease over the whole duration 268 of the in-situ experiments. This difference suggests that the As release cannot be linearly 269 associated with the Fe content. Synchrotron Fe K-edge XANES spectra, available for the 270 samples collected in wells 4-5 and 5-2 at the end of the experiments, show that ferrihydrite was 271 converted into Fe(III) oxide (lepidocrocite, goethite), siderite and mackinawite. In particular, 272 conversion into a more crystalline Fe(III) mineral phase was significantly different in the two 273 wells. Specifically, ferrihydrite was completely consumed and a high amount of Fe(III) oxide 274

was found in well 5-2, whereas high ferrihydrite and a small amount of Fe(III) oxide wereobserved in 4-5.

The existence of multiple surface complexation and mineral transformation mechanisms, which 277 significantly differ among the wells, complicates the interpretation of the processes controlling 278 279 the As release directly from the experimental datasets. The proposed model allowed us to reproduce the field observations in the three wells with a common set of surface complexation 280 parameters and kinetic parameters for mineral transformation (Tables SI4-6). In particular, the 281 sequential release of As from the solid, occurring at different rates, is captured well by the 282 performed simulations. The modeling results show that the sharp decrease in As at early time is 283 due to desorption as no significant transformation of ferrihydrite was taking place. The duration 284 of the lag phase preceding the reductive microbial dissolution of ferrihydrite (i.e., t<sub>i</sub> ferri) was 285 found to vary among the wells (Table SI6). This difference could suggest spatial heterogeneity of 286 287 this reaction in the field (20, 80). Interestingly, the observed lag phase increases along the selected flow line (i.e. from the mountain towards the flat plain). The model calibrated lag phase 288 appears to scale inversely with the flow velocity and allowed us to reproduce the onset of 289 290 ferrihydrite disintegration with a similar number (~300) of flushed pore volumes in the three wells. During the reductive dissolution/transformation of ferrihydrite, the solid-associated As 291 concentration becomes function of the As adsorbed onto ferrihydrite and sequestered into the 292 secondary mineral phases. Differences in the calibrated molar ratio of As sequestration  $\alpha$  (Table 293 SI6) suggests that this process differs among the wells. In particular, the model predicts that 23, 294 0, and 38 µg As/g coated sand were sequestered at 80 days in wells 5-2, 2-4, 4-5, respectively 295 even though the amount of crystalline Fe oxides is higher in well 5-2 than 4-5. Furthermore, the 296 model allowed us to reproduce the measured mineral composition for the two wells in which 297

these measurements were performed. Good agreement was achieved between the observed and simulated amounts of Fe(III) mineral phase, as well as of siderite whereas the model underestimates the amount of mackinawite in well 4-5. The outcomes of the calibrated model are also helpful to visualize the temporal trends of secondary mineral formation and ferrihydrite consumption (Figure 2d-f).

**Processes controlling arsenic release.** The calibrated model was used to distinguish the contributions of different mechanisms controlling the mobilization of arsenic observed during the in-situ experiments. Here, we assess the effects of arsenic change in speciation, sorption, dissolution of ferrihydrite, and arsenic sequestration into secondary Fe oxides. Figure 3a shows the comparison between simulated solid-associated arsenic for well 4-5 using the calibrated model when individually inhibiting these processes by defining 5 scenarios:

309	•	Scenario A: calibrated model including reduction of adsorbed As(V) to As(III), sorption,
310		reductive dissolution of ferrihydrite, Ostwald ripening, precipitation of ferrous oxides,
311		and arsenic sequestration into the newly formed minerals;
312	•	Scenario B: only sorption processes and reduction of adsorbed As(V) to As(III);
313	•	Scenario C: as Scenario A but without As sequestration into secondary minerals;
314	•	Scenario D: as Scenario A but without the reduction of As(V) to As(III);
315	•	Scenario E: as Scenario A but the change of As(V) to As(III) occurs in the aqueous
316		phase.

Figure 3b displays the simulated temporal change of fractional site occupancy occurring to illustrate the sorption competition mechanism taking place during the in-situ experiments. The

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analysis for the other wells has yielded similar results and is reported in the SupportingInformation (Figure SI1).



321

Figure 3. (a) Temporal change in total solid-associated arsenic concentration predicted for well 4-5 when considering different mechanisms of As sequestration and change of speciation. (b) Simulated temporal change in composition of the weak sites (i.e., Hfo\_w) of ferrihydrite in well 4-5 obtained with the calibrated model.

When discarding the iron mineral transformation and only considering As desorption (i.e. Scenario A), the model captures well the first experimental observations but simulates significantly higher As surface concentration after 25 days when ferrihydrite dissolution becomes relevant. This scenario yields a concentration of 133.2  $\mu$ g As/g coated sand at the end of the experiments that is more than twice the observed value 60.4  $\mu$ g As/g coated sand (Figure 3a). This difference shows that the As release from ferrihydrite surface is primarily determined 332 by the decrease in available sorption sites induced by the disintegration of ferrihydrite whereas sorption competition is of lower importance when reductive dissolution takes place in agreement 333 with the observations of Root et al. (9) on artificially deposited ferrihydrite-rich sediments of the 334 North Haiwee Reservoir (Olancha, CA, USA). Conversely, the model scenario that does not 335 include uptake of arsenic into newly formed minerals predicts higher release of arsenic and, thus, 336 lower As concentration at the end of the experiments (i.e., 24.2 µg As/g coated sand at 80 days). 337 These simulation results underpin the importance of As sequestration into secondary minerals for 338 the observed behavior at the field site. 339

Direct microbially-mediated reduction of aqueous and/or adsorbed As(V) has been extensively 340 observed during transition from aerobic to anaerobic conditions (30-31). However, the sequential 341 order in which the biotic reduction of Fe(III) oxide minerals and As(V) occur has been debated 342 (14, 30, 81-83). Furthermore, it remains unclear whether bacteria can directly transform the 343 344 As(V) into As(III) on the surface or initially requires the desorption of As(V). Here, the speciation change of surface-associated  $A_{s}(V)$  led to the best agreement with the field dataset. In 345 particular, this mechanism is predicted to limit the release of As from ferrihydrite as a stronger 346 initial As release that is predicted when reduction of surface As(V) is not considered (Scenarios 347 D and E in Figure 3a). When analyzing the simulated temporal change in surface composition 348 (Figure 3b), the adsorbed As(V) becomes As(III) at early times of the in-situ experiments 349 preceding the reductive dissolution of ferrihydrite (e.g., 7 days in well 4-5). 350

The solid-associated As at the end of the experiment days was predicted as As(III) whereas the speciation determined by K-edge XANES measurements indicated As(V) as the dominant species (Table SI3). This discrepancy may result from the oxidation of As(III) via interaction and/or sequestration into the formed crystalline iron phases as observed by Amstaetter et al. (76).
Indeed, the model indicates that the main part of the solid-associated As (i.e., 80% and 62% in
wells 5-2 and 4-5, respectively) is sequestered by the secondary iron oxides at the end of the insitu experiments.

358 At the beginning of the in-situ experiment, a significant part of the As(V) rapidly desorbs (i.e., 49 to 35 % surface sites occupancy; Figure 3b). A sensitivity analysis assessing the effect of the 359 aqueous species on the surface composition of ferrihydrite indicates that this desorption is 360 induced by the rapid drop in surface charge primarily due to the re-equilibration of the 361 362 ferrihydrite surface with the groundwater and, to a lower extent, to the competitive sorption effects of dissolved bicarbonate and silica (see Supplementary Information, Figure SI4). Due to 363 the local hydrochemical conditions and the high As(III) concentrations in the groundwater, none 364 of the aqueous species seems able to substantially compete for As(III) sorption sites as shown by 365 366 the steady As(III) fractional site occupancy (Figure 3b) leading to a plateau regime in the As surface concentration until As(III) mobilization is triggered by the disintegration of ferrihydrite 367 (Figure 3a). In particular, the As(III) surface site occupancy remains steady at the onset of 368 369 microbial dissolution of ferrihydrite (i.e., 20 days) characterized by an abrupt change in surface composition due to the strong adsorption of Fe(II) concomitant to a sharp desorption in Mg and 370 Si. Similar behavior of As adsorbed onto ferrihydrite is predicted in the other wells even though 371 the sequestration of As into secondary mineral phases spatially differ (Supporting Information, 372 Figure SI1 and Table SI6). 373

*Reductive transformation of ferrihydrite.* The reductive transformation of ferrihydrite
significantly controls the As release through the dissolution of the solid phase. This leads to a

reduction of sorption sites and to the formation of new mineral phases that can potentially sequester arsenic. The model allowed us to assess the relative contribution of the reductive dissolution, Fe(II)-catalyzed transformation, and precipitation of Fe(II)-mineral phases on the change in the total Fe content and in the composition of the mineral assemblage. Figure 4 displays the simulation results obtained when considering individually these iron mineral transformation mechanisms through the definition of four different modeling scenarios:

• Scenario 1: calibrated model (same as Scenario A above);

Scenario 2: only reductive dissolution of ferrihydrite with no further Fe(II) reactions (i.e.,
 no Ostwald ripening and no Fe(II) precipitation with carbonate and sulfide);

• Scenario 3: as Scenario 2 but including Fe(II) precipitation with carbonate and sulfide;

Scenario 4: Fe(II) allowed to react with ferrihydrite through Ostwald ripening but without
 reductive dissolution.



Figure 4. (a) Temporal change in total Fe content assessed through the different model scenarios;
(b) composition of the mineral assemblage at 80 days predicted for well 4-5 using the model and
considering the contributions of the different transformation mechanisms studied in Scenario 1-4.

Figure 4a shows that the observed pattern of Fe content measured in well 4-5 is captured well by 392 the calibrated model (Scenario 1). When only defining the reductive dissolution of ferrihydrite 393 (Scenario 2) the Fe-content is significantly underestimated (e.g., 0.49 mg Fe/g coated sand 394 compared to the experimental observation of 1.37 mg Fe/g coated sand at 80 days). The 395 formation of ferrous iron minerals limits the decrease in solid-associated Fe and improves the 396 agreement with the field data as illustrated by Scenario 3 (e.g., 1.01 mg Fe/g coated sand at 80 397 days). However, this scenario does not include Ostwald ripening and results in a slight 398 underestimation of the Fe content. Finally, Scenario 4 that only considers the effect of Ostwald 399 400 ripening does not capture the observed behavior. This scenario predicts a constant Fe content,

and only minimal conversion of ferrihydrite into Fe(III) oxide compared to Scenario 1. These 401 results suggest that, under the investigated field conditions, the Fe(II) groundwater 402 concentrations are not sufficient to promote significant recrystallization of ferrihydrite and that 403 404 the reductive dissolution of ferrihydrite is a prerequisite to generate the local Fe(II) concentrations necessary to substantially convert ferrihydrite into Fe crystalline phases. In 405 particular, the comparison between Scenario 1 and Scenario 3 shows that Ostwald ripening 406 improves the agreement with the experimental data, through the preservation of solid-associated 407 Fe, when it is considered together with the reductive dissolution of ferrihydrite and the formation 408 of Fe(II) secondary minerals. 409

*Fe(II)-induced mineralization pathways.* The type of secondary minerals, as well as the extent 410 and the kinetics of the conversion of ferrihydrite into more crystalline Fe(III) oxides, are 411 primarily controlled by the supply rate and the magnitude of the aqueous Fe(II) concentration (21, 412 413 84). However, significant differences in the crystallization of ferrihydrite can be observed between the wells despite similar surface and aqueous Fe(II) concentrations simulated upon 414 ferrihydrite dissolution (Figure SI3). This suggests that other mechanisms influence the Fe(II)-415 416 induced transformation of ferrihydrite and ultimately the As mobility. Adsorbed trace elements and/or the presence of major ions are known to determine the choice of the Fe(II)-induced 417 mineralization pathway from ferrihydrite (69, 85). In particular, the lower crystallization of 418 ferrihydrite predicted in well 2-4 (Figure 2) might be ascribed to the relatively higher chloride, 419 sulfate and bicarbonate concentrations in that well directly considered in the kinetic rate 420 expression controlling the Ostwald ripening reaction (Equation 2, Table SI2), which is in 421 agreement with previous studies (69). Furthermore, the presence of magnetite that forms through 422 topotactic transformation during Fe(II)-induced crystallization of ferrihydrite was not observed 423

424 during the in-situ experiments. Magnetite is typically observed in presence of high ferrous iron 425 concentrations that impede the release of Fe(II) from the mineral and result in a mix Fe(II)-Fe(III) solid (23-24, 65, 21, 66, 69). Despite relatively low dissolved Fe(II) concentration simulated by 426 427 the model (always less than 1 mM, Figure SI3), the ratio between ferrous iron and ferrihydrite concentrations at which formation of magnetite is typically observed (i.e., 1 mmol Fe(II)/g Hfo 428 (39)) was exceeded upon reductive dissolution of ferrihydrite (i.e., [2 - 10] mmol Fe(II)/g Hfo). 429 However, magnetite was not observed during the in-situ experiments. This result can be 430 explained by the relatively low groundwater concentration of Fe(II) that was maintained during 431 the initial phase preceding the onset of ferrihydrite reduction. Over this initial period, 432 accumulation of small amounts of lepidocrocite and/or goethite favored by the action of Fe(II) on 433 ferrihydrite could have led to surface site passivation preventing the formation of magnetite 434 despite the high concentration of Fe(II) occurring upon ferrihydrite reductive dissolution. A 435 similar effect has been observed in controlled laboratory experiments (64). 436

*Implications.* The reductive dissolution of poorly crystalline iron oxides has been recognized as 437 one of the predominant pathways leading to As contamination of groundwater (7, 20). However, 438 439 the complex interplay of geochemical processes in natural groundwater systems hampers a detailed description of the mechanisms controlling the fate and evolution of mineral phases and 440 As release from the sole analysis of water chemistry and mineral characterization data. This 441 study has highlighted the importance of multiple mechanisms (i.e., surface complexation, 442 reductive dissolution, formation of secondary iron minerals and arsenic sequestration into the 443 newly formed minerals), occurring at different time scales and with significant spatial variability, 444 when groundwater contacts ferrihydrite and triggers the release of arsenic. The model-based 445 interpretation of the in-situ experiments was instrumental to disentangle the roles of the different 446

447 geochemical processes on the evolution of the mineral assemblage and arsenic in the flowthrough system. While part of the arsenic rapidly desorbed from ferrihydrite, most of the 448 mobilization of solid-associated arsenic was controlled by the reductive dissolution of the 449 450 primary mineral and sequestration (i.e., sorption and reincorporation) into secondary iron oxides in agreement with previous laboratory studies (30). Formation of these more crystalline phases 451 was found to be induced by the Fe(II) generated from the disintegration of ferrihydrite triggering 452 further mineral crystallization. The model highlights important implications of different 453 geochemical mechanisms on the evolution of solid-associated iron and, thus, on the release of 454 arsenic. The kinetics of the transformation of ferrihydrite was particularly influenced by the 455 dissolved groundwater species (e.g., charged solutes) through chemical and electrostatic 456 interactions, and by mineral assemblage composition and transformation. The absence of 457 magnetite formation during the in-situ experiment, despite the high level of generated Fe(II), 458 contrasts with previous laboratory studies which extensively reported magnetite formation upon 459 reductive dissolution of ferrihydrite. This calls for further investigation on the mechanisms 460 461 controlling the mineralization pathway during Fe(II)-catalyzed transformation of ferrihydrite. The outcomes of this modeling study emphasize the importance of detailed experimental 462 observations able to capture the temporal dynamics and the spatial variability of geochemical 463 controls on arsenic mobilization. The determination of solid-associated arsenic and iron 464 concentrations, together with the microscopic and spectroscopic characterization of primary and 465 secondary minerals and the chemistry of the groundwater, contributed to underpin the model-466 based interpretation. 467

468 The performed model-based analysis was carried out using a one-dimensional flow-through 469 approach at specific spatial locations where experimental observations were available. The

understanding gained on the temporal dynamics and kinetic parameters for the different 470 471 geochemical processes could be exported and tested in multidimensional flow-through domains, which have additional degrees of freedom whose effects cannot be easily extrapolated from 1-D 472 473 setups (86-87). The integration of the knowledge on arsenic release and iron transformation in multidimensional reactive transport models of groundwater flow systems will allow the joint 474 consideration of the geochemical complexity, highlighted in this investigation, with the physical 475 and chemical heterogeneity of groundwater flow system (88-91). This will contribute to improve 476 our capability to describe and predict the release, transport, and fate of arsenic in complex, 477 heterogeneous aquifer systems. Such approach based on mechanistic description of physical and 478 biogeochemical processes also represents a promising design tool for remediation strategies 479 based on amendments injection and enhanced reactive mineral transformation. 480

481

# 482 Associated content

# 483 Supporting Information

Field data: wells technical information, measured groundwater aqueous composition used as 484 input parameters in the reactive transport model, measured time series of total Fe and As, the 485 mineral composition and solid-associated arsenic speciation measured at 80 days. Tables 486 summarizing literature and optimized values of the affinity constants used in the surface 487 488 complexation models as well as the optimized model parameters. Model results showing the change in surface composition and aqueous composition simulated in other wells. Results of a 489 sensitivity analysis performed to assess the effects of hydrochemical composition on the surface 490 composition of ferrihydrite. 491

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