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Investigation of effective media applicability for ultra-thin multilayer structures

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Multilayer hyperbolic metamaterials (HMMs) are highly anisotropic media consisting of alternating metal and dielectric layers with their electromagnetic properties defined by the effective medium approximation (EMA). EMA is generally applied for a large number of subwavelength unit cells or periods of a multilayer HMM. However, in practice, the number of periods is limited. To the best of our knowledge, a comparison between rigorous theory, EMA and experiments to investigate the minimum number of layers that allow for low error of EMA results has not yet been investigated. In this article, we compared the reflectance response of the effective anisotropic HMMs predicted by the scattering matrix method (SMM) and EMA with optical characterization data, having the unit cell twenty times smaller than the vacuum wavelength in the visible range. The fabricated HMM structures consist up to ten periods of alternating 10 nm thick Au and Al₂O₃ layers deposited by sputtering and atomic layer deposition, respectively. The two deposition techniques enable us to achieve a high quality HMM with low roughness: the root mean square (RMS) is less than 1 nm. We showed that the multilayer structure behaves like an effective medium from the fourth period onwards as the EMA calculation and experimental results agree well having below 4% the mean square standard deviation of reflectance (MSDR) for the wavelength range from 500 to 1750 nm with a wide incident angle range. These results could have an impact on the design and development of active metamaterials applications ranging from imaging to nonlinear optics and sensing.

1 Introduction

Hyperbolic metamaterials (HMMs) can play a key role in nanophotonics due to their controllability and tunability of the propagation of light. They are highly anisotropic media which have indefinite or hyperbolic dispersion and their properties are determined by their effective electric permittivity or magnetic permeability. Their main property is that they behave like metals in one direction and dielectric in the other direction in a broad-band wavelength range of operation^{1,2}. HMMs have shown various phenomena and applications in engineering photonic density of states³, enhanced spontaneous decay and recombination rates^{4,5}, super lens beating diffraction limit^{6–8}, extremely high biosensing sensitivity⁹, polarization selectivity¹⁰. They can be realized in the visible to mid-infrared wavelength region by a combination of metal and dielectric in the form of multilayers^{11–13},

trenches^{14–16}, nanorods¹⁷. The different suitable materials to design HMMs depending on the applications for various wavelength ranges have been studied in detail^{18,19}.

Au is the most practical plasmonic material to fabricate HMMs in the visible and near-infrared wavelength range due to its chemical stability^{11,20,21}. However, Au does not adhere well on dielectric substrates and thus the films are fully formed only above 15 nm when not using any adhesion layers. The percolation threshold limit for Au films ranges from a thickness of around 8 to 15 nm²² depending on the deposition technique used and deposition parameters.

Ti and Cr are the standard adhesion layers used for Au²³. The influence of Ti and Cr adhesion layers on ultra thin Au films has been studied morphologically using electron microscopy and found that Cr inter-diffuses within the Au layer forming a Cr–Au alloy with a partially oxidized adhesion layer²⁴. Moreover, the introduction of a few nanometer thick metallic adhesion layers has shown to increase the broadening of surface plasmon polariton (SPP) resonance due to the extra absorption and scattering from the metal²⁵. As an alternative to Ti and Cr, we recently reported that the silane based adhesion promoter (3-Aminopropyl)

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trimethoxysilane (APTMS) is a better adhesion layer between oxide and Au in comparison with metals regarding support of highly confined surface plasmon modes²⁶.

The propagating bulk plasmon modes in HMMs are due to the coupling of short range surface plasmon polaritons (SR-SPPs) in each metal-dielectric interface of the multilayer HMMs.^{27,28} This coupling implies that the electric field is localized at the interfaces, thus making adhesion layer's contribution even more significant. Therefore, using nonmetallic adhesion like APTMS is the favorable option for the fabrication of high quality Au based HMMs.

The electromagnetic properties of HMMs are routinely predicted by EMA, which is generally applied when the vacuum wavelength of light is much larger than the unit cell or period of the hyperbolic metamaterial^{29–32}. In ref.32, the authors analyse the applicability of EMA when the number of periods varies and show theoretically that the EMA can be applied only from a certain number of periods. Since we use a ZnSe prism to excite high-k waves in the system, we believe that the limits we find are stricter than the ones obtained in the cited work. However, it is a natural question whether the EMA is applicable on a fabricated structure with a limited number of periods. The minimum thickness or number of periods for a structure sufficient to behave like an effective medium is still unclear. Understanding this limit could help in designing of the HMM structures needed for various applications.

To study the applicability of EMA, we fabricated a set of multilayer structure with various periods of HMMs samples: 1, 2, 3, 4, 6, 8, 10 consisting of 10 nm thick Au and Al₂O₃ layers respectively, using APTMS as adhesion promoter in between each Au and Al₂O₃ interface. In terms of quality of the fabricated multilayer structure, the HMM with four periods has a RMS roughness of 0.40 nm and the final RMS roughness of the 10th period sample is 0.80 nm. We characterized the samples optically using the prism coupling scheme to study their reflectance spectra. Experimental results were then compared with EMA calculations. We used the mean square deviation of reflection (MSDR) to compare the reflection difference between EMA with multilayer and experiment using mean square deviation calculation as shown in equation (1) and (2), respectively. Comparison certifies that the reflection spectra in this multilayer case start matching the effective medium predictions from the 4th period having as low as 4% MSDR.

Although our results are obtained in specific HMM configuration, the general message remains: the EMA has a lower limit of applicability and one should take that into account when using it for describing the behavior of HMMs. This may prove of utmost importance for designing HMM-based devices since their characteristics may differ significantly from the ones calculated using the EMA theory. Most of the applications of HMMs in waveguiding^{33–35}, refractive index sensing¹¹, optical cavity design³⁶, hyperlens for sub-diffraction imaging³⁷ and so on are based on EMA. Therefore, it is important to know its range of applicability in order to design the needed devices. If EMA is applied outside its confidence interval, the performance of the HMM structures for these, and other, applications will deviate from the desired

ones.

Fig. 1 Schematic illustration of metal-dielectric multilayer structure, excitation and detection of SPPs using the Otto configuration. Symmetric plasmonic waveguide structures are made of SiO₂–adhesion layer–Au–adhesion layer–SiO₂. The adhesion layers under consideration are 1.0 nm thick APTMS layers.

2 Results and Discussion

2.1 Theoretical Study

$d_d:d_m$ [nm]	1	2	3	4	5	6	7	8	9	10
10:10	4.1	4.3	2.7	2.3	2.2	2.0	1.6	1.4	1.2	1.2
15:15	10.2	4.3	3.3	2.9	2.3	1.9	1.8	1.8	1.8	1.8
20:20	10.5	4.7	3.8	2.8	2.5	2.5	2.5	3.0	3.3	3.8

Table 1 Table of mean-square error reflectance, MSDR < 2.5 % , between multilayer structures and EMA-based HMM structures. Green shaded area represents MSDR < 2.5 % where EMA approximately holds and red shaded area is where behavior of HMMs are different from EMA.

We numerically studied the influence of the thickness of layers (d_m and d_d , $\Lambda = d_m + d_d$) and number of periods on the behavior of multilayer HMMs properties (reflectance) in comparison with the ones predicted by EMA. For simplicity we consider a HMM composed of Au and Al₂O₃ with metal filling factor of 0.5, without APTMS adhesion layer. Table 1 shows the summary of numerical analysis of reflectance difference between of the multilayer HMM calculated by 1D SMM and 1D EMA. We considered TM-polarized incident light with the magnetic field parallel to the plane of interface to calculate the reflectance. The reflectance calculated by 1D SMM and 1D EMA is based on the model in Figure 1. The details of the procedure are presented in Numerical Simulation section in Method. Here, we define the criteria for the applicability of EMA as the standard deviation of reflectance MSDR < 2.5 %. The MSDR is defined as

$$MSDR = \sqrt{\frac{1}{N} \sum_{\phi, \lambda} [R(\lambda, \phi)_{multilayer} - R(\lambda, \phi)_{EMA}]^2}, \quad (1)$$

where reflectance is a function of two variables, namely angle of incidence and wavelength as shown in equation 1. The angle of incidence is varied between 27° and 81° and the vacuum wavelength spans from 500 to 1750 nm. $R(\lambda, \phi)_{\text{multilayer}}$ and $R(\lambda, \phi)_{\text{EMA}}$ are the simulated reflectance spectra and $N = 57600$ is the number of points used for the simulation. The analysis results shown in table 1, imply that in the case of Au and Al_2O_3 films of 10 nm each, multilayer structures behave close to effective medium from 4 periods (total thickness of 80 nm). For 15 nm thick films the applicability criteria is satisfied from 5 periods onwards. In the case of 20 nm thick layers for Au and Al_2O_3 , the HMM structures behave different from EMA counter part and do not satisfy the standard deviation condition $\text{MSDR} < 2.5\%$ until at least 10 periods. To be noted that even the generally accepted condition of $\lambda > 10 * (d_d + d_m)$ is still fulfilled, the EMA condition, as defined by maximum admissible deviation, is not.

Additionally, we observe an unexpected feature of the EMA vs. rigorous theory comparison. For the 20 nm : 20 nm case, the MSDR seems to increase after 8 periods, hinting towards the possibility that, for big number of periods, the applicability criteria might not be satisfied. However, this observation is not fully verified. Thereafter, we proceed experimental demonstration with multilayer HMM of $d_d : d_m = 10 \text{ nm} : 10 \text{ nm}$.

2.2 Experimental Study

Fig. 2 Images of various HMM samples with 1, 4, 8 and 10 periods denoted by the roman numerals. Each sample is a quarter of a 4-inch wafer in size.

To carry out the experiment, different HMM samples having 10 nm:10 nm (Au : Al_2O_3) as a unit cell were fabricated. Each sample had different number of periods, from 1 to 10, on 4 inch glass wafers as shown in Figure 2. Due to the poor adhesion between the oxide and noble metals, we used an APTMS adhesion layer in between the Au and Al_2O_3 to obtain smooth and continuous films. The fabrication routine consisting of a combination of two deposition techniques, sputtering for Au and atomic layer deposition for Al_2O_3 , was used to maintain a roughness as low as possible, thus keeping it below 1 nm even after the 10th period. The details of the fabrication procedures of the HMMs are presented in the HMM Fabrication under Methods Section.

We investigated the surface morphology of the Au nanofilms for each period using atomic force microscope (AFM). The surface roughness of each Au layer is shown in Table 2. The roughness

Fig. 3 Topological characterization of the 10th period Au layer of the HMM. (a) SEM image showing a continuous layer with no interruptions. (b) AFM image for quantifying the roughness.

of the multilayer sample increases with the number of periods thus putting a practical limit on the maximum number of periods achievable. The films will form pin holes and defects if the roughness is more than 1. The scanning electron microscope (SEM) and AFM images of the final 10th period Au layer are shown in Figure 3a-b. The images confirm that the Au layer is continuous without any defects or pin holes. The final Au layer has a RMS roughness of 0.80 nm. The increase in the surface roughness from 8th period to 10th period is due to the accumulation of roughness by more periods. Since the roughness is below 1 nm in this work, the effect of scattering is not visible in the optical characterization of the samples even after 10th period.

Table 2 RMS roughness of Au layers of various periods of the HMM

Periods	1	2	3	4	6	8	10
Roughness (nm)	0.30	0.32	0.36	0.40	0.50	0.54	0.80

We conducted a series of reflection measurements on structures with different number of periods using the Otto configuration setup with a TM-polarized light as schematically described in Figure 1. We used TM-polarized light to excite the plasmon modes supported by the multilayer hyperbolic metamaterial. On top of the HMMs we sputtered a 50 nm SiO_2 layer to maintain the symmetry of the modes and also to allow for excitation of high order modes. TM-polarized light is used to excite the modes. This way, we can identify the SPP-type modes and analyze their behavior. The reflection measurements are shown in Figure 4d-f and Figure 4j-l for periods 1, 2, 3 and 4, 8 and 10, respectively. The noise close to 1100 nm visible in the experimental dispersion diagram is due to normalization errors arising from the spectral characteristics of the light source and not related to sample's response.

We performed 3D simulations of the reflectance of the multilayer HMMs of the various periods as described in Numerical Simulations in Methods section to compare with the experimental reflection measurements. In our 3D simulations, we also considered the APTMS adhesion layers. The simulation results are shown in Figure 4a-c for the periods 1, 2, 3 and Figure 4g-i for 4, 8, and 10, respectively.

For the first period as shown in Figure 4 (a,d), the low reflection region beneath 35° is due to the violation of total internal reflection (TIR) condition between the ZnSe prism and 50 nm SiO_2 layer. For single period structure, the experimental reflec-

Fig. 4 Dispersion diagram of HMM modes for ZnSe prism-SiO₂ (50 nm)-HMM-SiO₂ (500 μm) structures. 3D EMA simulations (a-c),(g-i) and measurements (d-f),(j-l) with HMMs of periods 1, 2, 3 and 4, 8, 10, respectively. The roman numerals represent the number of periods of the HMM.

tion dip is observed at lower wavelengths between 900 – 1100 nm for the same angle of incidence between 60° to 80° as compared to the broad reflection dip between 1300 – 1600 nm from simulation. This leads to a mean square reflection difference between effective medium prediction and experimental data to be 16% MSDR. We used MSDR to calculate the reflection difference between simulation and experiment as defined in numerical simulations as shown in Table 3. The MSDR between experiment and simulation in Table 3 was calculated by

$$MSDR = \sqrt{\frac{1}{N} \sum_{\phi, \lambda} [R(\lambda, \phi)_{\text{experimental}} - R(\lambda, \phi)_{\text{simulation}}]^2}, \quad (2)$$

where $\phi = 27^\circ - 81^\circ$ and $\lambda = 500 - 1750$ nm and $R(\lambda, \phi)_{\text{experimental}}$, $R(\lambda, \phi)_{\text{simulation}}$ are the experimental and simulation reflectance spectra respectively. $N = 28028$ is the number of points used in this case.

With increasing the number of periods, the reflection dip at long wavelengths blue shifts and a new mode appears at short wavelengths as shown in Figure 4 (b, c, e, f). This new mode red shifts and this tendency is consistent in both experiments and theory. However, before reaching a thickness equivalent to four periods the simulations consistently show the long wavelength mode red shifted compared to experiments.

From the fourth period onwards, the reflection dips in experiment and simulation start to match very well, within 4% MSDR. The reflection diagram on the 8th period also shows that the two modes start to merge, and they completely overlap for the 10th

Fig. 5 Dispersion diagram of HMM modes for ZnSe prism-SiO₂ (50 nm)-4th Period HMM-SiO₂ (500 μm) structures. (a) Experiment (b) 3D FDTD simulation on EMA HMM (c) 1D Scattering Matrix Method (SMM) on EMA and (d) 1D SMM on multilayer HMM, respectively.

period.

Table 3 Table of mean square error reflectance between 3D EMA simulation and experiment for the various periods of the HMM.

Periods	1	2	3	4	8	10
3D EMA vs Experiment	15.9	5.5	5	3.6	3.8	3.5
1D SMM on multilayer structures vs Experiment	4.5	3	4	1.5	1	1.1

In the calculation for reflectance of 1D SMM on multilayer HMM, we considered APTMS layers in Table 3. From Table 3, it can be observed that the reflection difference of the experimental and 3D EMA simulations decreases from 15.9% (1st period) to 3.5% MSDR (10th period) with increasing number of periods. This supports the prediction that the effective medium approximation starts to be accurate enough from a minimum number of periods. When comparing the accurate SMM theory with experimental results, one can see that, although generally decreasing, the difference between the spectra is maximum 4.5% MSDR. Since the 1D SMM simulations are assuming the complete geometry of the structure we can consider that the maximum 4.5% MSDR is the worst case scenario error, a combination between the experimental errors and the uncertainties in the modelling. Therefore, we can consider this number as a threshold for determining the applicability of the 3D EMA simulations. This leads us to state that the 3D EMA simulations are applicable only after the 4th period. This conclusion further supports the one obtained from Table 1.

One should note in Figure 5 that there is a clear difference between the 1D simulation results used for the theoretical study and the 3D simulation and the experimental ones. Therefore, it is more relevant to use 3D simulations to compare with the experimental data, while the 1D SMM simulations may be used for comparing the two theoretical approaches.

2.3 HMM Field Profile

To further study the experimentally observed optical modes of the structure, we investigated the field profiles from the reflection dips of various periods of the HMM.

Figure 6 shows the real part of the tangential component of the transverse magnetic field profile at the reflection dips with the angle of incidence from 33° to 85° for various periods in the structure: 2, 4 and 10 respectively calculated with transfer matrix method as discussed in Numerical Simulations under Meth-

Fig. 6 Transverse magnetic field profile of the HMM for (a) 2, (b) 4, (c) 10 periods where the red asterisk (*) marks the reflection dips corresponding to the angle, ϕ and wavelength, λ of the HMM dispersion diagram. The HMM is represented by the yellow and green color for Au and Al_2O_3 respectively and the red color represents the APTMS adhesion layer. The grey area represents the SiO_2 layer beneath and above the HMM. The roman numerals represent the period of the HMM.

ods section. From Figure 6a–c we can observe that symmetrical mode appears at higher angles and anti-symmetric mode at lower angles. The modes are due to the existence of metal-dielectric-metal (MDM) coupling configuration over dielectric-metal-dielectric (DMD) one³⁸. For the case of second period as shown in Figure 6a, the reflection dips observed at ($\phi = 35.1^\circ$, $\lambda = 500$ nm) and ($\phi = 56.3^\circ$, $\lambda = 890$ nm) are related to modes that are anti-symmetrically coupled and symmetrically coupled surface plasmon polaritons respectively.

On the 4th period, the modes at ($\phi = 37.6^\circ$, $\lambda = 500$ nm) and ($\phi = 47.8^\circ$, $\lambda = 708$ nm) starts to blue and red shift respectively as shown in Figure 6b. We could not observe any higher index modes of the HMMs which are related to the coupling of SPPs at the interfaces of the multilayer HMM in DMD configuration as analyzed by Higuchi et.al.³⁹. This is because the maximum effective mode index achievable in this configuration is about 2.5, the ZnSe refractive index.

For the 10th period as shown in Figure 6c, the two modes observed at ($\phi = 45.6^\circ$, $\lambda = 603$ nm) and ($\phi = 43.4^\circ$, $\lambda = 570$ nm) merge into one.

3 Methods

3.1 HMM Fabrication

The HMM samples were fabricated on 500 μm thick glass wafers. The wafers were precleaned in Piranha solution (70% H_2SO_4 + 30% H_2O_2) for 20 minutes to remove any organic dust residues. The unit cell consist of four-layers: 1nm APTMS - 10nm Au - 1nm APTMS - 10 nm Al_2O_3 . Fabrication starts with the immersion of the cleaned wafers into 2.5 % APTMS in isopropyl alcohol (IPA)

solution for 3 hours⁴⁰ to deposit the APTMS adhesion layer. Then 10 nm Au layer was sputtered at 2 mtorr pressure with a deposition rate of 10 $\text{\AA}/\text{second}$. Another layer of APTMS is deposited on top of the 10 nm Au layer in the similar way before the deposition of Al_2O_3 . The deposition of 10 nm Al_2O_3 was done using atomic layer deposition at temperature of 200 $^\circ\text{C}$ for 93 cycles where each cycle consists of 0.1 second pulse time of the precursors trimethyl-aluminum (TMA) and H_2O . We continued fabrication of various samples with different periods following the same process steps.

3.2 Optical Characterization

The reflection measurements were performed using high index ZnSe semi-cylinder prism of refractive index ranging from 2.4 to 2.7 in the visible and near infrared wavelength regime. TM-polarized light was used to excite the modes. The light source was a Super-K high continuum broadband laser from NKT Photonics allowing us to measure from a wavelength of 500 nm to 1750 nm. The samples were placed on the ZnSe prism with the help of a tightening screw with an unavoidable air gap between the sample and the prism. The incidence angles were varied from 27° to 81° with a 2° interval by rotating the mechanical stage. Each incidence angle was measured five times when ascending and five times when descending the angle to avoid the mechanical stage uncertainties. The reference spectrum is the measure of the reflectance without the sample at 45° incidence. Note that the noise close to 1100 nm visible in the experimental dispersion diagram is due to normalization errors arising from the spectral characteristics of the light source and not related to sample's response.

3.3 Numerical Simulations

The series of calculation in Table 1 were performed by the scattering matrix formalism to calculate the reflectance from the multilayer structures⁴¹. We considered TM-polarized incident light with the magnetic field parallel to the plane of interface and for the same range of wavelengths of $\lambda = 500 - 1750$ nm and the angle of incidence as in the experiment, $\phi = 27^\circ - 81^\circ$ for the case of calculation in Table 1 and $\phi = 33^\circ - 85^\circ$ for the simulation in Figure 6.

The model structure consists ZnSe prism– SiO_2 (50 nm thick)–HMM– SiO_2 substrate. Here HMM is either multilayer of Au and Al_2O_3 or the one characterized by EMA.

According to EMA¹⁸, the effective ordinary and extraordinary permittivities, ϵ_o and ϵ_e are expressed by

$$\epsilon_o = f_m \cdot \epsilon_m + f_d \cdot \epsilon_d \quad (3)$$

$$\epsilon_e = \left(\frac{f_m}{\epsilon_m} + \frac{f_d}{\epsilon_d} \right)^{-1}, \quad (4)$$

where ϵ_m and ϵ_d are the permittivities of metal and dielectric, and f_m and f_d are the volume fraction of metal and dielectric layers, respectively. In general, EMA is assumed to hold under the condition that the thicknesses of each layer are deeply sub-wavelength. We note that in our structure with thickness of 10

nm for both Au and Al₂O₃ layers as compared to the wavelength interval of $\lambda = 500 - 1750$ nm, we maintain the ratio between the period thickness ($\Lambda = 20$ nm) and wavelengths of $\Lambda/\lambda = 1/25 - 1/87.5$. The permittivity of the Al₂O₃ film, ϵ_d , was measured by ellipsometer. The permittivity of Au film, ϵ_m , is characterized by the Drude–Lorentz model:⁴²

$$\epsilon_m = 1 + \sum_{m=0}^{m=5} G_m \Omega_m^2 / (\omega_m^2 - \omega^2 + j\omega\Gamma_m) \quad (5)$$

where $m = 0$ is the Drude term, thus $\omega_0 = 0$.

The permittivities of ZnSe prism and fused silica (SiO₂) substrate are taken from Connolly et al.⁴³ and Malitson et al.⁴⁴ respectively.

Reflectance spectra of the effective medium approximated HMMs, provided in Figure 4, are conducted with use of commercially available Lumerical software. To compare more precisely with the experimental results, we included APTMS adhesion layer in the unit cell and used 3D FDTD simulations. The refractive index of APTMS is assumed to be 1.46.^{45–47}

Here the HMM is an indefinite uniaxial layer homogenized by EMA for a unit cell of 4 layers with three different materials, APTMS - Au - APTMS - Al₂O₃, based on the below formula where f parameters stand for volume fractions of Al₂O₃ as f_{d1} , APTMS as f_{d2} and Au as f_m in the unit cell.

$$\epsilon_o = f_m \cdot \epsilon_m + f_{d1} \cdot \epsilon_{d1} + f_{d2} \cdot \epsilon_{d2} \quad (6)$$

$$\epsilon_e = \left(\frac{f_m}{\epsilon_m} + \frac{f_{d1}}{\epsilon_{d1}} + \frac{f_{d2}}{\epsilon_{d2}} \right)^{-1} \quad (7)$$

A nested parameter sweep is used to calculate the reflection of TM-polarized plane wave for angles between 27° - 81° and wavelengths between 500 - 1750 nm for different thickness of homogenized HMM corresponding to 1, 2, 3, 4, 8, and 10 periods.

The transverse magnetic field profile in Figure 6 is calculated using transfer-matrix method⁴⁸. We use the reflectance coefficient to obtain the tangential field components at ZnSe prism-SiO₂ interface. This obtained field was further used to calculate the fields in structure, considering 1nm resolution.

4 Conclusions

High quality periodic multilayer structures with number of periods from 1 to 10 were fabricated and optically characterized using prism coupling experiment. The study was to compare reflectance by the various structures with the one predicted by the effective medium approximation. The structures were fabricated by combining two deposition techniques: sputtering and atomic layer deposition which allows controlling the thickness and minimizing the roughness of each layer of the HMMs. The final RMS roughness obtained was 0.80 nm. The optical characterization also shows a very good agreement with the effective medium approximation calculation using 3D FDTD method as close as below 4% MSDR in comparison to the experiment from the 4th period of the structure. Our findings show that we need at least 4 periods of the multilayer structure to comply with the criteria for the

applicability of EMA.

Conflicts of interest

There are no conflicts to declare.

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