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CRediT author statement

Anjali Edathil: Methodology, Investigation, Visualization, Writing-Reviewing & Editing

Pravin Kannan: Writing - Original draft, Reviewing & Editing, Formal analysis, validation

Fawzi Banat: Conceptualization, Writing-Reviewing & Editing, Supervision, Project administration

Journal Proposi

Adsorptive oxidation of sulfides catalysed by δ -MnO₂ decorated porous graphitic carbon composite

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Graphical Abstract



Environmentally benign bio adsorbent for sulfide removal

Adsorptive oxidation of sulfides catalysed by δ -MnO₂ decorated porous graphitic carbon composite

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Abstract

Removal of dissolved sulfide contaminants from aqueous model solution using bioderived porous graphitic carbon (PGC) impregnated with δ -MnO₂ was investigated. The composite adsorbent was synthesized using the chemical wet deposition method wherein MnO₂ was deposited on carbon walls through an in-situ reaction between permanganate and ethanol. Formation of transition metal oxide of manganese in the form of birnessite nanoparticles on interconnected PGC cell structure was confirmed by transmission electron microscopy, scanning electron microscopy, elemental analysis, and X-Ray diffraction characterization studies. The composite nanomaterial was tested for sulfide removal from aqueous solution at various conditions, including the pH, adsorbent dosage, initial solution concentration, and contact time. Adsorption results demonstrated an excellent adsorption capacity of ca. 90% within 20 minutes of contact time at 298 K. Equilibrium data collected from batch adsorption experiments fitted well with the Langmuir isotherm model ($K_L = 190 \text{ L/mg}$; $R^2 = 0.99$). The maximum adsorption capacity of the composite was estimated as 526.3 mg S^{2}/g at highly alkaline conditions compared to ca. 340 mg/g for a δ -MnO₂ adsorbent. Adsorptive oxidation of sulfides on composite MnO₂-PGC adsorbent was found to be controlled by the chemisorption process in accordance with the pseudo-second-order reaction model. Characterization of spent adsorbents revealed that sulfide was removed through adsorptive oxidation resulting in the formation of agglomerated particles of metal sulfate complexes and elemental sulfur. Analysis of reaction mechanism revealed that both MnO2 and PGC played a role in the adsorptive oxidation of sulfides to CaSO₄ and elemental sulfur.

Capsule: δ -MnO₂/PGC nanocomposite synthesized using a facile in-situ wet deposition technique exhibited superior sulfide uptake capacity

Keywords: δ-MnO₂, adsorption, Sulfide wastewater, Alginate, Porous graphitic carbon

1 1. Introduction

2

Effluents released from coke and steel industries, pulp and paper, petroleum refinery, 3 municipal wastewater treatment plants, and animal husbandries have been found to contain 4 dissolved hydrogen sulfide (H_2S), bisulfides (HS^-), and sulfide ions (S^{2-}) (Kociolek-Balawejder 5 and Wilk, 2011) which are often grouped together and referred as "sulfides". Reuse of sulfide 6 7 contaminated water for industrial applications is severely restricted due to the undesired reaction 8 of sulfide components with metal and metal oxides. This results in the formation of metal 9 sulfides in which induces sulfide corrosion of pipelines and processing equipment. The dissolved sulfide compounds in wastewater can also be released to the gaseous phase as H₂S, thereby 10 compounding the adverse environmental effects of sulfides even at lower concentrations (Wilk et 11 al., 2020). With the increase of sour gas fields in and around the middle eastern countries, 12 generation and subsequent release of sulfide contaminated wastewater pose a serious 13 14 environmental concern. Thus, removal of sulfide metal ions from refinery wastewater, preferably to a concentration below 0.2 ppm, is critical not only for safer discharge into aquatic bodies 15 (Vaiopoulou et al., 2005), but also to develop sustainable industrial practices in refinery plant 16 operations. 17

The presence and distribution of different ionic species of hydrogen sulfide in wastewater primarily depend on solution pH. Thompson et al. (1995) reported that at lower pH values (5-6), the predominant sulfide species remains to be aqueous hydrogen sulfide (H_2S_{aq}), and with a slight increase in pH (7-9), the solution primarily contains bisulfides (HS^-) along with sulfide (S^{2-}) ions. However, at higher solution pH (>10), the only sulfur species present in the solution are the reduced species of sulfur, S^{2-} ions.

Removal of sulfide ions from wastewater could be achieved by various techniques, 24 including filtration after liming and recycling (Artiga et al., 2005), neutralization (Tamersit and 25 Bouhidel, 2020), recuperation of sulfides and reuse (Komanowsky et al., 1984), precipitation of 26 sulfides by iron salts (Chen et al., 2018; Firer et al., 2008), oxidation by oxidizing agents with or 27 28 without catalysts (Heideman et al., 1984), and biological detoxification of sulfides (Marais et al., 29 2020; Mestrinelli et al., 2016). Among these techniques, direct oxidation of sulfides by oxidizers has been researched using different oxidizing agents like H₂O₂, KMnO₄, and ozone. Although 30 H₂O₂ is the widely used oxidizer in practice, direct removal of sulfides from water using KMnO₄ 31 is also well-known (Cadena and Peters, 1988; Dohnalek and FitzPatrick, 1983; Willey et al., 32 1964). 33

Sulfide oxidation reaction by KMnO₄ can follow different complex pathways depending 34 on the conditions encountered. For example, in the absence of oxygen, permanganate directly 35 oxidizes hydrogen sulfide. On the contrary, in aerobic systems, sulfide oxidation proceeds by 36 reaction with oxygen to form various sulfur compounds in addition to MnO₂. As the reaction 37 continues, MnO₂ acts as an oxygen-transfer catalyst and assists in further sulfide 38 oxidation. However, this process converts sulfides into elemental sulfur in addition to other by-39 products like agglomerated MnO₂ that needs to be subsequently removed by filtration, thereby 40 41 increasing the energy demand. Yao et al. demonstrated that the rate of sulfide oxidation in seawater is significantly enhanced by δ -MnO₂ through the formation of surface complexes (Yao 42 and Millero, 1993). The spent MnO₂, and the oxidized MnOOH are insoluble in alkaline medium 43 and hence favours ease of separation from wastewater (Valeika et al., 2006). 44

Adsorption has gained increased attention due to lower process energy demand and substantial capability in removing trace quantities of contaminants, including heavy metals (Burakov et al., 2018), and sulfide ions (Bono et al., 2016; Li et al., 2017; Soto et al., 2011) from

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wastewater. Traditionally, activated carbon synthesized from coal and various biomass materials, 48 mainly cellulosic and microbial origin (Gupta et al., 2015; Lu et al., 2020; Suhas et al., 2016) has 49 been employed as adsorbents due to its high porosity and surface area. However, large-scale 50 treatment using activated carbon remains challenging because of the low selectivity of carbon 51 towards sulfide ions. Different carbon materials like porous carbon, carbon nanotubes and 52 53 fullerene have been extensively used for advanced treatment of wastewaters (Gupta and Saleh, 2013). Recently, graphene-based material has been successfully utilized as an adsorbent in the 54 field of nano sciences (Amiri et al., 2018; Mondal et al., 2018), specifically for environmental 55 remediation (Achazhiyath Edathil et al., 2019; La et al., 2017). This led to the development of 56 57 carbon-based composite adsorbents surface functionalized with various metal oxides that cater to the removal of specific contaminants. Anchoring δ -MnO₂ on carbon structures would facilitate 58 separation of spent adsorbents, in addition to providing enhanced adsorption capacity and 59 improved mechanical and chemical stability. Many techniques have been proposed in the 60 literature for in-situ synthesis of δ -MnO₂, including precipitation using KMnO₄ and different 61 alcohols (Subramanian et al., 2008). Detailed synthesis studies conducted by Subramanian et al 62 (Subramanian et al., 2008) revealed that the morphology and the oxidized state of Mn deposited 63 on carbon walls depends on the type of alcohol used. Using the surface manoeuvring property of 64 65 alcohols, nanostructured δ -MnO₂ is formed by nucleation, aggregation and coalescence of particles. 66

During recent times, the superior physical properties of porous graphitic carbon have been exploited for numerous industrial applications, specifically as adsorption and separation media (Chai et al., 2012; Gokulakrishnan et al., 2011; Stein et al., 2009). Novel synthesis techniques have focussed on the design of porous carbon structures with surface functionalization, offering increased adsorption capacity, high selectivity, and low density. A

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substantial amount of research has focussed on developing sustainable wastewater treatment 72 73 techniques by employing bio-derived porous carbon material. Among numerous bio-derived carbon, sodium alginate derived from brown seaweed has shown great potential as a carbon 74 precursor for various energy and environmental applications (Srinivasan, 2013). Our previous 75 work investigated sulfide removal from aqueous solution using porous graphitic carbon 76 77 synthesized from alginate, and the results confirmed the enhanced adsorptive capacity of PGC for sulfides (Edathil et al., 2017). In the present study, the superior oxidative property of δ -MnO₂ 78 in conjunction with highly selective and enhanced adsorptive capacity of porous graphitic carbon 79 derived from a natural polymer, sodium alginate, is realized through MnO₂-PGC composite 80 adsorbent. In-situ synthesis of δ-MnO₂ using KMnO₄ and ethanol on porous graphitic carbon 81 through a wet chemical deposition technique has been demonstrated. The complex 82 interconnected hierarchical porous carbon structure evenly distributed with δ -MnO₂ could be 83 expected to facilitate electron transfer and oxidize sulfides to elemental sulfur and sulfates. The 84 efficacy and suitability of the adsorbent are evaluated by determining the removal efficiency and 85 maximum uptake capacity of sulfide species. As the composite adsorbent is synthesized from bio 86 derived PGC, the applicability of the adsorbent for sulfide removal from aqueous solution is 87 further encouraged. 88

89

90 2. EXPERIMENTAL SECTION

91 2.1. Materials

Alginic acid calcium salt, potassium permanganate, and ethanol were purchased from Sigma Aldrich, USA, and sodium sulfide ($Na_2S \cdot 9H_2O$) was obtained from Fisher Scientific. All chemicals were of analytical grade and hence used without further purification. Deionized water was used in the preparation and dilution of all solutions. Sulfide model solutions were prepared

by dissolving crystals of Na₂S·9H₂O in deionized water and passing nitrogen gas to avoid 96 oxidation of sulfide. Various concentrations of sulfide solutions were prepared by further 97 diluting the prepared model solution with deionized water. 98

- 99
- 100

101 2.2. Synthesis of PGC, MnO₂, and MnO₂-PGC Composites

First, porous graphitic carbon (PGC) was synthesized by annealing and subsequent 102 carbonization of alginic acid calcium salt as described in our earlier work (Edathil et al., 2017). 103 To prepare the MnO₂-PGC composites, equal quantities of KMnO₄ and PGC were added to 60 104 ml of distilled water under magnetic stirring to form a homogeneous distribution of the precursor 105 solution. After stirring for 30 minutes, 20 mL of ethanol was added dropwise and the suspension 106 107 was stirred for 12 h at room temperature to allow slow growth of MnO₂ nanoparticles on the carbon. The obtained composite particles were then filtered and washed repeatedly with enough 108 quantities of DI water until the pH reached 7. The final product abbreviated as MnO₂-PGC was 109 dried at 353 K overnight and stored for further use. Besides, pure MnO₂ particles were also 110 prepared using a similar approach, but in the absence of PGC. The synthesized samples were 111 112 used as adsorbents directly for all the adsorption experiments performed in this study. Fig. S1 in supplementary section illustrates the experimental procedure used in this study for the synthesis 113 of pure and composite adsorbents based on wet chemical deposition technique 114

- 115
- 2.3. 116

Material Characterization

The surface morphology and microstructure of the adsorbents before and after sulfide 117 adsorption were analyzed using FEG Quanta 250 scanning electron microscopy (SEM) and FEI 118 Tecnai G20 transmission electron microscopy (TEM). Prior to the SEM analysis, adsorbent 119

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particles were sputter-coated with a conductive layer of gold-palladium (Au/Pd, 3 nm thickness). The zeta potential of the adsorbent samples was measured using Zeta PALS instrument (Brookhaven Instruments Corporation, USA), and elemental analysis was recorded using energy dispersive X-ray spectrometer (Oxford-EDX, UK) fitted to the SEM. Further, the crystalline structure of the adsorbent materials was determined using analytical X'Pert PRO Powder Diffractometer (Cu-Kα radiation 1.5406 A°, 40 kV, 40 mA) in the 2θ range of 5°–80°.

126

127 2.4. Adsorption Experiments

Batch adsorption experiments were conducted by adding a certain mass of synthesized 128 adsorbent to about 10 ml of aqueous sulfide solutions with different initial concentrations 129 ranging from 1 mg/L to 200 mg/L in 50 ml stoppered conical flasks. The mass of the adsorbent 130 was varied between 3 and 11 g per 10 ml of sulfide solution to simulate the change in dosage 131 conditions. The flasks were placed in a shaking water bath (Daihan, Korea) maintained at 298 K 132 and subjected to continuous agitation at 140 rpm until equilibrium was attained. It is later shown 133 in the study that the optimum contact time to reach equilibrium for all cases was around 180 min. 134 Sulfide concentrations before and after the adsorption process were measured and analyzed, as 135 demonstrated in section 2.5. All the tests were performed in duplicates. Based on the initial (C_0) 136 and residual equilibrium concentration (Ce), percent removal, and adsorbent uptake capacity at 137 equilibrium (qe) were calculated, as shown in our previous work (Edathil et al., 2017). 138 Additionally, adsorption experiments were conducted for different contact times (from 1 to 240 139 min) at fixed process conditions of 200 mg/L initial sulfide concentration, 298 K, and pH 12. 140

141

142 2.5. Measurements of Sulfide

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143	To measure the initial and residual dissolved sulfide concentration in the aqueous
144	solution, 200 μ L of pipetted samples were analyzed using LCK 653 sulfide detection kit on UV-
145	vis Spectrophotometer (DR5000, Hach Lange) by the methylene blue method. The sulfide test is
146	based on the reaction of sodium sulfide with N, N-dimethyl-p-phenylenediamine oxalate to
147	directly form methylene blue complex. The intensity of the blue color, as measured by the UV-
148	vis spectrophotometer using Test kit 653 is assumed to be directly proportional to the amount of
149	sulfide present in the original sample (E. Sheppard and H. Hudson, 2002).

150

151 3. RESULTS AND DISCUSSION

152 **3.1.** Adsorbent Characterization

The morphology and microstructure of the synthesized adsorbents, including δ -MnO₂ and 153 MnO₂-PGC composites, were observed using Scanning Electron Microscopy images, refer Fig. 154 155 1(a) and 1(e). In addition, EDX data presented in Fig. 1(b) and 1(f) serve to determine the elemental composition of the adsorbents. The surface morphology of δ -MnO₂ exhibited both 156 dense nanosized particles in a size range of 100-200 nm and micro-sized balls. EDX spectra of δ -157 MnO₂ revealed the presence of both manganese and oxygen with trace quantities of other 158 elements from the coating process. With the addition of PGC, it could be noticed that the porous 159 160 interconnected microstructure of carbon acts as a basic building block upon which δ-MnO₂ nanoparticles are deposited. The EDX spectra of MnO₂-PGC revealed the distinct pattern peaks 161 of magnesium in addition to the peaks of carbon, oxygen, and calcium which are the major 162 constituent elements present in the PGC. The coexistence of all these elements in the obtained 163 EDX results clearly proves the formation of MnO₂-PGC composites. The SEM images of spent 164 (sulfide adsorbed) δ -MnO₂ and MnO₂-PGC composite has been illustrated in Fig. 1(c) and 1(g) 165 166 with the corresponding EDX results in Fig. 1(d) and 1(h). It could be noted that following the

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adsorption process using δ -MnO₂, the adsorbent surface underwent structural changes and 167 predominantly displayed small aggregates of elemental sulfur and sulfate nanoparticles, 168 suggesting successful adsorption/oxidation of sulfide. The presence of Na and S in the EDX 169 results, see Fig. 1(d) further confirms that sulfide has been oxidized to sodium sulfate and/or 170 elemental sulfur. The composite adsorbent also showed the presence of irregular particles with 171 172 an aggregated surface on both the carbon walls as well as on the surface of MnO₂ nanoparticles. Furthermore, EDX spectra of sulfide-adsorbed MnO₂-PGC shows a characteristic peak for sulfur 173 particles along with carbon, oxygen, and calcium. These results further confirm the successful 174 adsorptive oxidation of sulfide on the surface of the adsorbent to calcium sulfate and/or 175 176 elemental sulfur.

10



Fig. 1: Scanning Electron Microscopy (SEM) and EDX results of nanoparticle composites: (a-b) fresh MnO2 (c-d) spent MnO2 (e-f) Fresh-MnO2-PGCcomposite(g-h)sulfideadsorbedMnO2-PGCcomposites:composite



Fig. 2: Transmission Electron Microscopy (TEM) images of synthesized (a) δ -MnO₂ and (b) MnO₂-PGC composite.

To better understand the changes in morphological microstructure induced by in-situ 177 composite synthesis, TEM micrographs of δ -MnO₂ and MnO₂-PGC composite were recorded at 178 179 higher magnifications and are shown in Fig. 2(a) and 2(b). TEM images of δ -MnO₂ (Fig. 2(a)) revealed the nanoscale architecture of MnO₂ particles with significant agglomeration, which 180 agrees well with the SEM results. The lattice fringe spacing is 0.7 nm corresponding to the (110) 181 plane of δ -MnO₂ (Subramanian et al., 2008). On the other hand, it can be noticed from the TEM 182 image of MnO₂-PGC composite that the MnO₂ nanoparticles are interconnected and uniformly 183 distributed on the surface of the PGC. Along with the lattice fringe of 0.336 nm indexed to (002) 184 plane of graphitic carbon, the composites also showed the lattice fringe spacing corresponding to 185 the (110) plane of δ -MnO₂. Furthermore, the presence of microcrystalline domain of calcium 186 nanoparticles (indicated by the red circle) that are formed by the special 'egg-box' structure of the 187

alginate precursor containing organic calcium salts was observed in the TEM image of thecomposites (Edathil et al., 2017).

190



Fig. 3: X-ray diffractograms of various fresh and spent adsorbents.

Fig. 3 shows representative X-ray diffractograms of both fresh and spent composite 191 adsorbents in addition to fresh and spent δ-MnO₂ adsorbents and raw PGC. In porous graphitic 192 carbon, the prominent Bragg reflection observed at 26.1°, 44°, and 54° corresponds to the (002), 193 (101) and (004) planes of the graphitic carbon matrix (JCPDS file number 41-1487). 194 Additionally, the diffractogram also showed the presence of calcium oxide and calcium 195 196 hydroxide particles in the carbonaceous matrix. The diffractogram of δ or Birnessite type MnO₂ (JCPDS no. 43-1456) showed characteristic diffraction peaks at 12.8°, 24.8°, 37.6°, and 66.4° 197 attributed to (001), (001), (111) and (311) planes. In the diffractogram of fresh MnO₂-PGC 198 composite, the position of the main diffraction peak of graphitic carbon and δ -MnO₂ was well 199

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200 retained. On the other hand, XRD of sulfide adsorbed δ -MnO₂, and MnO₂-PGC composite clearly indicated the presence of additional peaks with higher intensity. The oxidation of sulfide 201 components by δ -MnO₂ and MnO₂-PGC to elemental sulfur could be confirmed by the presence 202 of predominant peaks (labeled by ^ in Fig. 3) observed at 23.3°, 36.2° and 39.5° that correspond 203 to the (222) plane of orthorhombic sulfur having S₈ structure (JCPDS 74-1465). Moreover, the 204 XRD of spent δ -MnO₂ showed the presence of additional peaks at 19.1°, 32.5° and 48.9° 205 206 (labeled by # in Fig. 3) corresponding to the (111), (200) and (300) planes of sodium sulfate (Na₂SO₄). However, the diffractogram of sulfide adsorbed MnO₂-PGC composites showed 207 dominant peaks at 29.5° and 49.3° related to the (202) and (600) planes of CaSO₄, indicating the 208 formation of calcium sulfate complex (labeled by \sim in Fig. 3). The presence of additional peaks 209 in spent adsorbents further verifies that oxidation of sulfide ions has occurred. 210

211

212 3.2. Adsorption of Sulfide Ions by Synthesized Adsorbents

213 3.2.1. Effect of Solution pH

The effect of solution pH on sulfide removal from aqueous solution was investigated 214 under identical conditions ($C_0 = 202 \text{ mg/L}$, m = 0.01 g, t = 180 min, T = 298 K) for both MnO₂ 215 and MnO₂-PGC composites. Adsorption experiments were performed at different pH values in 216 217 the range of 3 to 12, and the corresponding adsorbent removal efficiencies are illustrated in Fig. 4. The data indicates that the adsorption behaviour of both the adsorbents was not affected by the 218 solution pH, and the percent removal was marginally higher for the MnO₂-PGC composite than 219 MnO_2 nanoparticles. In aqueous solutions, sulfides mainly exist in the form of H_2S_{ag} , HS^- and 220 S^{2-} ions. Under strongly acidic conditions with pH <6, sulfides are mainly present in the form of 221 H_2S_{aq} and HS^- , while it contains negligible S^{2-i} ons. Whereas at higher pH > 6, the aqueous 222



solution predominantly contains S^{2-} along with HS⁻ions, and the concentration of HS⁻ions



Fig. 4: Effect of pH on sulfide removal using different adsorbents.

225 under strongly alkaline conditions (pH 9 to 12). The obtained pH results clearly indicates that the 226 adsorptive oxidation of sulfide by MnO_2 and MnO_2 -PGC was not hindered by adsorption sites as 227 well as the competitive adsorption. Henceforth, the adsorption process of sulfide is found to be 228 less affected by initial solution pH, inferring that the developed composite adsorbent holds the 229 potential to effectively adsorb sulfide from aqueous solution at all pH. Zeta potential 230 measurements were carried out with the aim of understanding (1) the pronounced selective 231 adsorption characteristic exhibited by δ -MnO₂ and MnO₂-PGC for sulfide species, (2) the effect

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232 of surface charge on sulfide adsorption, and (3) the stability of the system. It was interesting to observe that both adsorbents exhibited high surface negative charge at all solution pH. Since the 233 surface charge of the as-prepared adsorbents was negative in the experimental pH range as 234 indicated by the Zeta potential (Fig. 4), most likely chemisorption is caused by an electron 235 transfer reaction with the surface-active sites. The zeta potential of δ -MnO₂ ranging from -25 to -236 40 mV was caused by the presence of MnO groups on the surface of δ -MnO₂. MnO₂-PGC 237 composite also showed high negative surface charge and may be attributed to the presence of 238 carboxyl and hydroxyl groups obtained from the alginate molecules in addition to the MnO-239 groups from δ -MnO₂ particles. Even though the absolute values of the zeta potential for both 240 these adsorbents under the investigated pH range (3 to 12) were high (suggesting its good 241 stability in the colloidal state), the composites exhibited slightly higher sulfide removal 242 efficiency. This could be attributed to the better accessibility of the active sites owing to the 243 interconnected porous structure of the carbon. Thus, the active functional groups present on the 244 surface of the developed adsorbents were believed to be less affected by the initial solution pH, 245 thereby contributing to the extraordinary adsorption efficiency showcased all pH conditions. 246 Henceforth, all further adsorption experiments were carried out at the original solution pH of 247 12.06. 248

249

250 **3.2.2. Effect of Ionic Strength**

The possible presence of background salts in sulfide containing industrial wastewater tends to form complex metals that might compete with sulfide species for available adsorption sites. The influence of ionic strength on sulfide removal efficiency by the nanocomposite adsorbents was assessed through the addition of NaCl and CaCl₂ to the sulfide solution. The concentration of background electrolytes in the sulfide solution was varied from 0 to 1 M.
Adsorption studies were conducted in a batch mode at a temperature of 298 K, adsorbent dosage
of 1 mg/L, and initial sulfide concentration of 202 mg/L. Adsorption results as shown in Fig S2,
showed no significant change in removal efficiency after the addition of background electrolytes
to the sulfide solution.

260

261 **3.2.3.** Effect of Adsorbent Dose

The effect of adsorbent dose on sulfide adsorption by MnO₂ and MnO₂-PGC 262 nanocomposite has been presented in Fig. 5. Experiments were performed at the following 263 conditions: initial sulfide concentration of 202 mg/L, 180 min, 298 K, and a solution pH of 264 12.06. Adsorbent mass was varied between 2.5 and 20 mg that corresponds to a dosage of 0.25 265 266 g/L to 2 g/L. It can be noticed that the removal efficiency increases with adsorbent dosage till ca. 1 g/L, at which point the efficiency reaches a maximum. The initial increase in removal 267 efficiency is a direct result of increased contact surface area, more specifically the active sites 268 offered by the adsorbent. However, with further increasing the adsorbent dosage, the effective 269 surface area is significantly affected, resulting from overlapping or aggregation of sulfide 270 molecules near the adsorption site (Ahluwalia and Goyal, 2007). As a result, all the active sites 271 are not fully utilized, thereby leading to a decrease in the adsorption capacity, as evidenced in the 272 SEM images, refer Fig. 1e. 273



Fig. 5: Effect of adsorbent mass on sulfide removal using different adsorbents.

274 3.2.4. Effect of Initial Sulfide Ion Concentration

The amount of sulfide ions adsorbed is proportionally controlled by the initial 275 276 concentration of sulfide ions in the solution making it a crucial parameter for sensitivity analysis. All the parameters adsorbent dosage (1 g/L), agitation time (180 min), temperature (298 K), and 277 pH (12.06) except initial concentration were kept constant. The effect of initial ion concentration 278 (varying from 0 to 600 mg/L) on equilibrium adsorption capacity and removal efficiency of 279 sulfide ions on the adsorbent is shown in Fig. 6. As shown, sulfide removal efficiency for the 280 MnO₂ nanoparticle sample exhibited a gradually decreasing trend till 300 mg/L, beyond which a 281 sharp decrease could be noticed. A similar trend could be observed for the nanocomposite 282 sample, however, less pronounced. 283



Fig. 6: Effect of initial sulfide solution concentration on sulfide removal using different adsorbents.

Contrastingly, with an increase in initial sulfide ion concentration, an increase in adsorption capacity for both samples could be noticed. The steady increase could be attributed to the increased local concentration gradient of sulfide ions between the solid and aqueous phase that subsequently results in higher sulfide ion fixation at the surface area and maximum utilization of the available active sites (Barka et al., 2013). However, when the active sites are saturated with sulfide ions, the equilibrium adsorption capacity remains constant. The maximum adsorption capacity is significantly higher for the composite (505 mg/g) in comparison to the



291 MnO₂ nanoparticle (ca. 310 mg/g), thereby indicating the positive impact of introducing δ -MnO₂



particle into the interconnected morphology of the porous graphitic carbon.

Fig. 7: Effect of contact time on removal efficiency and uptake capacity.

293 **3.2.5. Effect of Contact Time**

292

In order to determine the time required for achieving adsorption equilibrium, it is significant to assess the influence of agitation time on adsorption capacity and efficiency. Fig. 7 depicts the effect of agitation time on the adsorption of sulfide ions over MnO₂-PGC adsorbent at fixed conditions of initial concentration (202 mg/L), adsorbent dosage (1 g/L), temperature (298 K), and pH (12.06). At the early stages of adsorption (t<20 min), a rapid increase in removal efficiency and adsorption capacity could be observed. Beyond 20 minutes, the effect gradually

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300 diminished until it displayed no significant increase beyond 120 minutes. The residual concentration at 180 min was found to be approximately about 0.8% of that obtained after 240 301 min. Accordingly, a quasi-equilibrium condition was assumed to have been reached at 180 min, 302 and henceforth all succeeding batch experiments were conducted for 180 min. The pronounced 303 increased rate at early stages could be attributed to the availability of abundant vacant active sites 304 on the adsorbent. As adsorption proceeds, sulfide ions gradually occupy the vacant sites at a 305 306 much slower rate until a point of saturation. The decreased sorption rate is possibly due to the 307 larger diffusion path lengths deeper into the adsorbent pores where the sulfide ions encounter higher mass transfer resistance. No significant change in sulfide concentration was observed 308 after 180 min as all sites have been occupied, and equilibrium is established. 309

310

311 **3.3.** Adsorption Kinetic Studies

To evaluate the adsorption rate and elucidate the reaction mechanism of sulfide ions on 312 MnO₂-PGC composites, experimental data were analyzed using the frequently employed kinetic 313 models, including pseudo-first-order (PFO), pseudo-second-order reaction (PSO), and 314 intraparticle diffusion (IPD) models. In a well-agitated batch system, the resistance offered by 315 the film is negligible in comparison to the adsorbent internal microstructure (surface and pore). 316 The diffusion mass transfer can be captured by an apparent diffusion coefficient that ensembles 317 the different steps involved in the intraparticle diffusion process. The behavior of intraparticle 318 diffusion could be explained by the Weber & Morris intra-particle diffusion model (IPD) as: (Dil 319 et al., 2016; Nekouei et al., 2015; Weber and Morris, 1963) 320

321
$$q_t = k_i t^{0.5} + C$$
 (1)

21

where k_i is the intra-particle diffusion rate constant (mg/g. min^{0.5}) and C is the empirical constant 322 (mg/g). The value of C depends on the film boundary layer thickness wherein a larger value of C 323 represents a significant effect of the boundary layer on adsorbate diffusion (Kannan and 324 Sundaram, 2001). Typically, the rate-controlling step is deduced by analyzing the linear 325 relationship between q_t and t^{0.5}, as shown in supplementary file Fig. S3. It can be noticed that 326 the experimental data exhibits three different linear parts (I, II, III), each possibly indicating 327 different stages of intra-particle diffusion. The first part refers to the least-resistive external 328 surface adsorption or macro-pore diffusion, the second part to the relatively less-accessible 329 mesopores, and the third part to micropore diffusion (Cheng et al., 2013). It is evident that the 330 linear part of the diffusion curve (step I) does not pass through the origin, and therefore the 331 diffusion process might not be solely controlled by any specific stage but is probably influenced 332 by multiple steps. The corresponding rate constants and intercept for the three parts are denoted 333 as k_{i1}, C₁, k_{i2}, and k_{i3}, and are summarized in Table 1. It can be noted that the rate constants 334 gradually decrease from 16.72 mg/g.min^{0.5} (step 1) to 3.94 (step II) to 0.09 (step III), strongly 335 indicating increasing diffusion resistance with the progress of the adsorption process. Stage I is 336 predominant when there are numerous vacant sites in the adsorbent particle during the initial 337 stages. However, during stage 2, most of the active sites on the surface are saturated, and hence 338 intra-particle diffusion is limited by the interior mesopores. Finally, at the last step, the sulfide 339 ions diffuse towards micropores and establish equilibrium between the solid and dissolved 340 Moreover, the increasing value of intercept C indicates the deviation from the 341 phases. dominating rate-controlling mechanism as a result of the increasing boundary layer thickness. 342

343 Kinetic data analysis using pseudo-first and second-order reaction models is frequently344 employed to determine how fast adsorption equilibrium would be achieved. For the PFO reaction

model, adsorption rate constant (k_f) was determined by plotting $ln(q_e - q_t)$ against t for sulfide 345 ion adsorption on MnO₂-PGC composite at an initial concentration of 202 mg/L and 298 K. 346 Values of equilibrium loading (qe) and second-order rate constant (ks) for the PSO model was 347 obtained from a linear plot of t/q_t versus t, refer to supplementary file Fig. S4. Model 348 parameters, including rate constants and equilibrium loading, were obtained through linear 349 regression, and the accuracy of the fit was evaluated from the regression coefficient (\mathbb{R}^2). 350 Further, in order to assess the error propagated through linearization, the constants were also 351 evaluated using non-linear forms of the model equations and compared with the results from 352 linear forms. A summary of model equations, along with the regressed parameters from different 353 models, have been compiled in Table 1. It could be noticed that both PFO and PSO reaction 354 models predict experimental data reasonably well, as evidenced by the high values of the 355 regression coefficient. Despite the good fit of the PFO linear model, the values of both constants, 356 namely rate constant and equilibrium capacity, are vastly different from the PFO non-linear and 357 PSO model estimates. It should be remembered that the PFO model is applicable only during 358 initial adsorption stages and high adsorbate solution concentration (Wang and Guo, 2020), and 359 360 thus employing it for larger time frames would induce significant error. The low value of equilibrium adsorbent loading estimated by the PFO linear model could be a direct consequence 361 of extending the model for a wider time step. The qe values estimated by the PSO linear and 362 non-linear models are in good agreement with the experimentally calculated equilibrium loading 363 364 values ($q_{e,exp}$).

365

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Model		Equation	Rate constants	q _e (mg/g)		R ²
				qe, exp	Q e, cal	
PFO	Linear	$\ln(1-(q_t/q_e)) = -k_f t$	$k_{f=}0.04\pm0.0018$	201.9	56.4 ± 0.9	0.954
	Non-linear	$q_t = q_e(1 - e^{-k_f t})$	$k_{f=} 0.86 \pm 0.02$		184.9±2.1	0.903
PSO	Linear	$t/q_t = t/q_e + (1/k_s q_e^2)$	$k_s = 0.0028 \pm 0.0005$	201.9	204.1±0.6	0.999
	Non-linear	$q_t = (k_s q_e^2) t/(1+k_s q_e t)$	$k_s = 0.0065 \pm 0.0009$		194.7±1.1	0.967
			$k_{i1} = 16.72 \pm 1.2$			0.99
IPD	$q_t = k_i t^{(1/2)} + C$	$C_1 = 111.74 \pm 2.1$	201.9			
			$k_{i2} = 3.94{\pm}1.5$			0.77
		20-	$k_{i3} = 0.09{\pm}0.05$			0.79

Table 1: Summary of kinetic model equations and parameters of MnO₂-PGC composite

352 **3.4.** Adsorption Isotherms

The experimental data of adsorption isotherms were analysed using three different 353 models, namely Langmuir, Freundlich, and Temkin. The standard mathematical equations 354 describing the models could be found widely in literature, and hence is not presented in this 355 work. Isotherm parameters were estimated by linear regression analysis and are listed in Table 356 S1 along with the corresponding model equations. As shown, the value of the regression 357 358 coefficient for the Langmuir model equation is 0.99 for both MnO₂ and composite samples. It is an implication that sulfide ion adsorption on both samples follows a monolayer adsorption 359 process with no interaction between the adsorbed molecules. MnO₂-PGC Comparing the value of 360 Langmuir adsorption constant (k_L) between MnO₂ and composite sample, it can be inferred that 361 the affinity of sulfide ion adsorption on MnO₂ is higher than that of MnO₂-PGC composite. 362 363 However, due to increased surface area, the PGC composite possesses significantly higher adsorption capacity than MnO₂ nanoparticle. The applicability of Freundlich isotherm for sulfide 364 adsorption on MnO₂ and PGC composite was also tested and validated with isotherm 365 366 experimental data. The solution concentration influence coefficient (1/n) value of 0.05 for MnO₂ sample strongly indicates favourable adsorption. However, the linear regression coefficient for 367 368 the MnO₂-PGC composite sample was 0.69, which is significantly smaller than that of the 369 Langmuir model. Similarly, the regression coefficient for the Temkin adsorption model is far from unity indicating a non-linear relationship between ln q_e and ln C_e. Therefore, sulfide ion 370 adsorption on MnO₂-PGC composite follows monolayer adsorption, and thus, Langmuir 371 adsorption isotherm is more suitable for modeling the equilibrium process. Based on the results, 372 the maximum sulfide adsorption capacity on MnO₂-PGC composite was estimated to be 526.3 373

- 374 mg/g. Compared with other sulfide adsorbents presented in literature, it can be seen from Table 2
- that MnO₂-PGC exhibited superior adsorption capacity.

Adsorbent	Initial Concentration (ppm)	Adsorption capacity (mg/g)	Reference
Granular ferric hydroxide (GFH)	19.8 ± 0.6	29.1 ± 0.6	(Sun et al., 2014)
Alg/Iron Oxide-NP	<mark>64.3</mark>	<mark>136.9</mark>	(Pal et al., 2018)
Activated Carbon (AC) - 500°C	<mark>0-1000</mark>	<mark>58.8</mark>	(Hariz and Monser, 2014)
PGC	<mark>45</mark>	<mark>149.25</mark>	(Edathil et al., 2017)
GSH Composites	<mark>202-450</mark>	370.4	(Achazhiyath Edathil et al., 2019)
CeO2-NiAl-LDHs coated	<mark>0.1 M</mark>	<mark>181.15</mark>	(Achazhiyath Edathil et al.,
activated carbon			2019)
MnO ₂ nanoparticle	0-450	303.03	This work
MnO ₂ -PGC	<mark>0-600</mark>	<mark>526.32</mark>	This work

Table 2: Comparison of sulfide adsorption capacities for different adsorbents

376 **3.5. Reaction Mechanism**

The MnO₂-PGC composite was employed for sulfide removal in order to exploit the advantages of the oxidative nature of MnO₂ and the surface functionality of PGC offered by oxygen functional groups. To further understand the mechanism involved in adsorption/oxidation, it is of great importance to understand the elementary reaction step involved in the dissolution of crystalline hydrate of Na₂S in water. In aqueous alkaline solution, dissolution of Na₂S solution yields sulfides $[S_{aq}^{2-}]$, bisulfides $[HS_{aq}^{-}]$ and aqueous H₂S $[H_2S_{aq}]$

(Linkous et al., 2004). Thus, the interaction of the dissolved sulfur species with oxygen 383 functional groups present on the PGC and the MnO₂ nanoparticles results in the distribution of 384 sulfides oxidation products over the composite adsorbent surface The $C(O^*)_{(ads)}$ species which is 385 the oxygen-containing active sorption site and/or radical of the form C (O*) on the carbon 386 surface, are believed to be responsible for the successful adsorptive oxidation of sulfide to 387 different species such as elemental sulfur and calcium sulfate. When aqueous hydrogen sulfide 388 389 ions contact the graphitic carbon surface, it undergoes oxidative decomposition to produce sulfur atoms. Sulfur atoms react in a substitution reaction with the C(O) surface complex and in an 390 addition reaction with radical C* to form C-S complexes and continue until the formation of 391 elemental sulfur chains (S_8) . The possible redox reaction involved in the formation of elemental 392 sulfur by PGC is illustrated as below: 393

394

$$\mathrm{HS}^{-}+\mathrm{C}(0^{*})_{(\mathrm{ads})}\rightarrow\mathrm{S}_{(\mathrm{ads})}+\mathrm{OH}^{-}$$

$$H_2S_{(ads)} + C(0^*)_{(ads)} \rightarrow \frac{1}{8} S_8^0 + H_2O + C$$

395

In aqueous medium, bisulfides (HS⁻) reacts with the oxygen functional groups to form sulfur oxides, $SO_{2(ads)}$ and $SO_{3(ads)}$ and is as evidenced in the literature (Brazhnyk et al., 2007; Lemos et al., 2012). These sulfur oxides further react with water resulting in the formation of sulfate ions (SO_4^{2-}) that continues to react with calcium metal ions present in the PGC matrix to form calcium sulfates. XRD further confirms the presence of CaSO₄.

401

$$HS^-+3 C(0^*)_{(ads)} \rightarrow SO_{2(ads)} + OH^-$$

402
$$SO_{2(ads)} + C(0^*)_{(ads)} \rightarrow SO_{3(ads)} + C^*$$

403
$$SO_{3(ads)} + H_2O \rightarrow 2H^+ + SO_4^{2-}$$

$$SO_4^{2-} + Ca^{2+} \rightarrow CaSO_4 0.5H_2 0$$

The production of elemental sulfur $[S_8^0]$ by MnO₂ proceeds through a series of surface complex formation initiated by the adsorption of HS⁻ onto the manganese oxide surface followed by oxidation as illustrated below:

$$S^{2-}+2MnO_{2(ads)}+2H_{2}O \rightarrow +2MnOOH + S^{0}+2OH^{-}$$

With MnOOH as catalyst,

$$S^{2^{-}} + 2H_{2}O + O_{2} \rightarrow 2S^{0} + 40H^{-}$$

$$MnO_{2(ads)} + HS^{-} \rightarrow Mn^{2+}{}_{(ads)} + 2H_{2}O + \frac{1}{8}S_{8}{}^{0}$$

$$Mn^{2+}{}_{(ads)} + 2H_{2}O \leftrightarrow Mn(OH)_{2(ads)} + H^{+}$$

$$2Mn(OH)_{2(ads)} + 2O_{2} \leftrightarrow 2MnO(OH)_{2(ads)}$$

$$412 \qquad 2MnO(OH)_{2(ads)} \leftrightarrow MnO_{2(ads)}^{*} + H_{2}O$$

The adsorbed HS⁻ ions also participate in redox reactions to form an intermediate metal surface complex MnS that could undergo two different competitive reaction pathways to form elemental sulfur and sulfates through the formation of zero-valent sulfur intermediate (Herszage and dos Santos Afonso, 2003).

419

$$MnO_{2(ads)} + H_{2}O \rightarrow MnOH^{2+}_{(ads)}$$

$$MnOH^{2+}_{(ads)} + HS^{-} \rightarrow MnS_{(ads)} + H_{2}O$$

$$MnS_{(ads)} + H_{2}O \rightarrow MnOH_{2(ads)} + S^{0}$$

420
$$MnOH_{2(ads)} \rightarrow MnOH^{2+}_{(ads)} * + Mn^{2+}_{(aq)}$$

$$S + HS^- \rightarrow HS_2^-$$

 $HS_2^- + 7S \rightarrow S_8 + HS^-$

 $MnOH_{2(ads)} + MnS_{(ads)} + MnOH^{2+}_{(ads)} \rightarrow SO_4^{2-} + 3MnOH_{2(ads)}$

421

$$\mathrm{SO_4}^{2-} + \mathrm{Na^{2+}}_{(\mathrm{aq})} \rightarrow \mathrm{NaSO_4}_{(\mathrm{aq})}$$

422

Oxidation of S_{aq}^{2-} , HS_{aq}^{-} and H_2S_{aq} species by MnO₂-PGC composites was experimentally 423 verified by the presence of sulfate in the form of calcium sulfate and elemental sulfur from XRD 424 analysis. Results from EDX also confirm the participation of MnO2 in the oxidizing reaction 425 resulting in the formation of various sulfur species. In addition, with the deposition of MnO₂ on 426 PGC, the maximum adsorption capacity was significantly enhanced when compared to bare 427 428 PGC, which was reported to be 149.2 mg/g (Edathil et al., 2017). The high values of solid adsorbent loading and negligible liquid phase equilibrium concentrations at low sulfide initial 429 concentration conditions are an indication of the formation of metal complexes, including 430 calcium sulfate wherein the rate of adsorption is very high relative to the rate of desorption. The 431 results obtained from XRD and EDX well support the combined effect of PGC and MnO₂ on 432 oxidation of sulfide molecules. However, techniques for desorbing the sulfide contaminants from 433 434 the adsorbent needs to be investigated before recovery and reuse of spent adsorbent could be 435 envisaged.

436

437 CONCLUSION

The feasibility of employing the MnO₂-PGC composite adsorbent for the removal of 438 hazardous sulfide components from aqueous systems was investigated through batch adsorption 439 studies at different process conditions. MnO₂-PGC nanocomposite adsorbents were synthesized 440 via the in-situ chemical wet deposition method using PGC derived from calcium alginate as 441 442 carbon precursor. The synthesized fresh composite and spent adsorbent were examined using 443 TEM, SEM, EDX and XRD and revealed that the surface modification of PGC by MnO₂ nanoparticles helped in drastically enhancing the oxidative capability of bare carbon. It was 444 found that the removal efficiency of the adsorbent was not affected by the solution pH; however, 445 it was dependent on the initial sulfide ion concentration. Kinetic studies inferred that adsorption 446 of sulfide ions by MnO₂-PGC composite was well-described by pseudo-second-order kinetic 447 model, confirming that chemisorption controlled the overall rate of sulfide sorption. 448 Experimental isotherm data confirmed the suitability of the Langmuir model for describing the 449 equilibrium conditions, and the maximum adsorption capacity was estimated to be 526.3 mg/g, 450 significantly higher than that of PGC. Results confirmed that the high adsorption capacity could 451 be attributed to the reactivity of bounded MnO₂, and oxygen atoms present on the active sites of 452 PGC with interconnected morphology that oxidized sulfide contaminants to sulfates and 453 elemental sulfur. In summary, the excellent adsorptive characteristics demonstrate that the 454 MnO₂-PGC composites can serve as an adsorbent material to remove hazardous sulfide 455 contaminants from aqueous solution. 456

457

458 **Conflict of Interest**

459 There are no conflicts of interest to declare.

460

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Adsorptive oxidation of sulfides catalysed by $\delta\text{-}MnO_2$ decorated porous graphitic carbon composite

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<u>Highlights</u>

- δ -MnO₂/porous graphitic carbon nanocomposite synthesized by in-situ wet deposition
- Surface functionalized PGC and precipitated δ -MnO₂ catalyzed oxidation of sulfides
- Sulfides species converted to metal sulfates and sulfur, and removed by adsorption
- Equilibrium best-described by Langmuir model with an uptake capacity of 526.3 mg/g
- Kinetic intra-particle diffusion model suggested multiple rate-controlling steps

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Declaration of interests

 \boxtimes The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

□The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

None		
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