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CRediT author statement

Anjali Edathil: Methodology, Investigation, Visualization, Writing-Reviewing & Editing

Pravin Kannan: Writing – Original draft, Reviewing & Editing, Formal analysis, validation

Fawzi Banat: Conceptualization, Writing-Reviewing & Editing, Supervision, Project administration

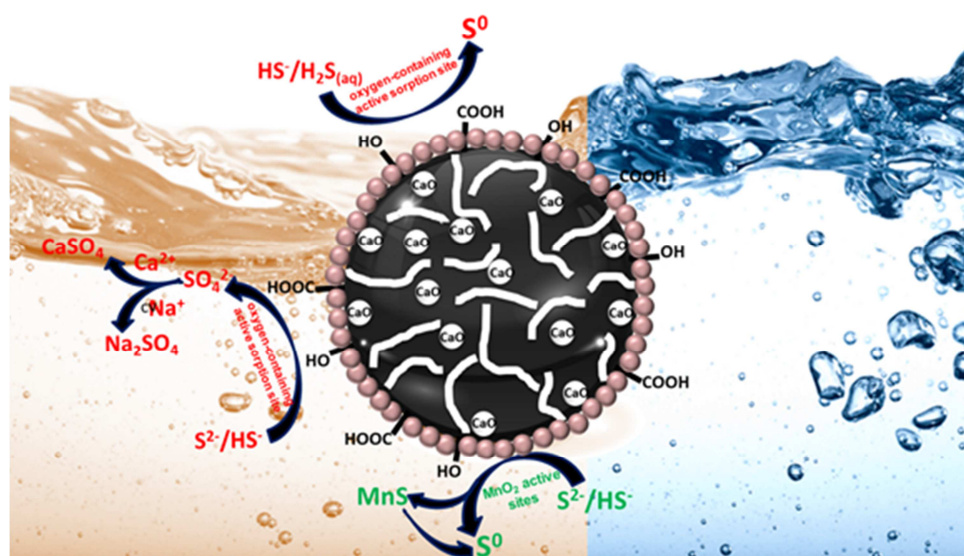
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Adsorptive oxidation of sulfides catalysed by δ -MnO₂ decorated porous graphitic carbon composite

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Graphical Abstract



Environmentally benign bio adsorbent for sulfide removal

Adsorptive oxidation of sulfides catalysed by δ -MnO₂ decorated porous graphitic carbon composite

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Abstract

Removal of dissolved sulfide contaminants from aqueous model solution using bio-derived porous graphitic carbon (PGC) impregnated with δ -MnO₂ was investigated. The composite adsorbent was synthesized using the chemical wet deposition method wherein MnO₂ was deposited on carbon walls through an in-situ reaction between permanganate and ethanol. Formation of transition metal oxide of manganese in the form of birnessite nanoparticles on interconnected PGC cell structure was confirmed by transmission electron microscopy, scanning electron microscopy, elemental analysis, and X-Ray diffraction characterization studies. The composite nanomaterial was tested for sulfide removal from aqueous solution at various conditions, including the pH, adsorbent dosage, initial solution concentration, and contact time. Adsorption results demonstrated an excellent adsorption capacity of ca. 90% within 20 minutes of contact time at 298 K. Equilibrium data collected from batch adsorption experiments fitted well with the Langmuir isotherm model ($K_L = 190$ L/mg; $R^2 = 0.99$). The maximum adsorption capacity of the composite was estimated as 526.3 mg S²⁻/g at highly alkaline conditions compared to ca. 340 mg/g for a δ -MnO₂ adsorbent. Adsorptive oxidation of sulfides on composite MnO₂-PGC adsorbent was found to be controlled by the chemisorption process in accordance with the pseudo-second-order reaction model. Characterization of spent adsorbents revealed that sulfide was removed through adsorptive oxidation resulting in the formation of agglomerated particles of metal sulfate complexes and elemental sulfur. Analysis of reaction mechanism revealed that both MnO₂ and PGC played a role in the adsorptive oxidation of sulfides to CaSO₄ and elemental sulfur.

Capsule: δ -MnO₂/PGC nanocomposite synthesized using a facile in-situ wet deposition technique exhibited superior sulfide uptake capacity

Keywords: δ -MnO₂, adsorption, Sulfide wastewater, Alginate, Porous graphitic carbon

1. Introduction

Effluents released from coke and steel industries, pulp and paper, petroleum refinery, municipal wastewater treatment plants, and animal husbandries have been found to contain dissolved hydrogen sulfide (H₂S), bisulfides (HS⁻), and sulfide ions (S²⁻) (Kociolek-Balawejder and Wilk, 2011) which are often grouped together and referred as “sulfides”. Reuse of sulfide contaminated water for industrial applications is severely restricted due to the undesired reaction of sulfide components with metal and metal oxides. This results in the formation of metal sulfides in which induces sulfide corrosion of pipelines and processing equipment. The dissolved sulfide compounds in wastewater can also be released to the gaseous phase as H₂S, thereby compounding the adverse environmental effects of sulfides even at lower concentrations (Wilk et al., 2020). With the increase of sour gas fields in and around the middle eastern countries, generation and subsequent release of sulfide contaminated wastewater pose a serious environmental concern. Thus, removal of sulfide metal ions from refinery wastewater, preferably to a concentration below 0.2 ppm, is critical not only for safer discharge into aquatic bodies (Vaipoulou et al., 2005), but also to develop sustainable industrial practices in refinery plant operations.

The presence and distribution of different ionic species of hydrogen sulfide in wastewater primarily depend on solution pH. Thompson et al. (1995) reported that at lower pH values (5-6), the predominant sulfide species remains to be aqueous hydrogen sulfide (H₂S_{aq}), and with a slight increase in pH (7-9), the solution primarily contains bisulfides (HS⁻) along with sulfide (S²⁻) ions. However, at higher solution pH (>10), the only sulfur species present in the solution are the reduced species of sulfur, S²⁻ ions.

24 Removal of sulfide ions from wastewater could be achieved by various techniques,
25 including filtration after liming and recycling (Artiga et al., 2005), neutralization (Tamersit and
26 Bouhidel, 2020), recuperation of sulfides and reuse (Komanowsky et al., 1984), precipitation of
27 sulfides by iron salts (Chen et al., 2018; Firer et al., 2008), oxidation by oxidizing agents with or
28 without catalysts (Heideman et al., 1984), and biological detoxification of sulfides (Marais et al.,
29 2020; Mestrinelli et al., 2016). Among these techniques, direct oxidation of sulfides by oxidizers
30 has been researched using different oxidizing agents like H_2O_2 , KMnO_4 , and ozone. Although
31 H_2O_2 is the widely used oxidizer in practice, direct removal of sulfides from water using KMnO_4
32 is also well-known (Cadena and Peters, 1988; Dohnalek and FitzPatrick, 1983; Willey et al.,
33 1964).

34 Sulfide oxidation reaction by KMnO_4 can follow different complex pathways depending
35 on the conditions encountered. For example, in the absence of oxygen, permanganate directly
36 oxidizes hydrogen sulfide. On the contrary, in aerobic systems, sulfide oxidation proceeds by
37 reaction with oxygen to form various sulfur compounds in addition to MnO_2 . As the reaction
38 continues, MnO_2 acts as an oxygen-transfer catalyst and assists in further sulfide
39 oxidation. However, this process converts sulfides into elemental sulfur in addition to other by-
40 products like agglomerated MnO_2 that needs to be subsequently removed by filtration, thereby
41 increasing the energy demand. Yao et al. demonstrated that the rate of sulfide oxidation in
42 seawater is significantly enhanced by $\delta\text{-MnO}_2$ through the formation of surface complexes (Yao
43 and Millero, 1993). The spent MnO_2 and the oxidized MnOOH are insoluble in alkaline medium
44 and hence favours ease of separation from wastewater (Valeika et al., 2006).

45 Adsorption has gained increased attention due to lower process energy demand and
46 substantial capability in removing trace quantities of contaminants, including heavy metals
47 (Burakov et al., 2018), and sulfide ions (Bono et al., 2016; Li et al., 2017; Soto et al., 2011) from

48 wastewater. Traditionally, activated carbon synthesized from coal and various biomass materials,
49 mainly cellulosic and microbial origin (Gupta et al., 2015; Lu et al., 2020; Suhas et al., 2016) has
50 been employed as adsorbents due to its high porosity and surface area. However, large-scale
51 treatment using activated carbon remains challenging because of the low selectivity of carbon
52 towards sulfide ions. Different carbon materials like porous carbon, carbon nanotubes and
53 fullerene have been extensively used for advanced treatment of wastewaters (Gupta and Saleh,
54 2013). Recently, graphene-based material has been successfully utilized as an adsorbent in the
55 field of nano sciences (Amiri et al., 2018; Mondal et al., 2018), specifically for environmental
56 remediation (Achazhiyath Edathil et al., 2019; La et al., 2017). This led to the development of
57 carbon-based composite adsorbents surface functionalized with various metal oxides that cater to
58 the removal of specific contaminants. Anchoring δ -MnO₂ on carbon structures would facilitate
59 separation of spent adsorbents, in addition to providing enhanced adsorption capacity and
60 improved mechanical and chemical stability. Many techniques have been proposed in the
61 literature for in-situ synthesis of δ -MnO₂, including precipitation using KMnO₄ and different
62 alcohols (Subramanian et al., 2008). Detailed synthesis studies conducted by Subramanian et al
63 (Subramanian et al., 2008) revealed that the morphology and the oxidized state of Mn deposited
64 on carbon walls depends on the type of alcohol used. Using the surface manoeuvring property of
65 alcohols, nanostructured δ -MnO₂ is formed by nucleation, aggregation and coalescence of
66 particles.

67 During recent times, the superior physical properties of porous graphitic carbon have
68 been exploited for numerous industrial applications, specifically as adsorption and separation
69 media (Chai et al., 2012; Gokulakrishnan et al., 2011; Stein et al., 2009). Novel synthesis
70 techniques have focussed on the design of porous carbon structures with surface
71 functionalization, offering increased adsorption capacity, high selectivity, and low density. A

72 substantial amount of research has focussed on developing sustainable wastewater treatment
73 techniques by employing bio-derived porous carbon material. Among numerous bio-derived
74 carbon, sodium alginate derived from brown seaweed has shown great potential as a carbon
75 precursor for various energy and environmental applications (Srinivasan, 2013). Our previous
76 work investigated sulfide removal from aqueous solution using porous graphitic carbon
77 synthesized from alginate, and the results confirmed the enhanced adsorptive capacity of PGC
78 for sulfides (Edathil et al., 2017). In the present study, the superior oxidative property of δ -MnO₂
79 in conjunction with highly selective and enhanced adsorptive capacity of porous graphitic carbon
80 derived from a natural polymer, sodium alginate, is realized through MnO₂-PGC composite
81 adsorbent. In-situ synthesis of δ -MnO₂ using KMnO₄ and ethanol on porous graphitic carbon
82 through a wet chemical deposition technique has been demonstrated. The complex
83 interconnected hierarchical porous carbon structure evenly distributed with δ -MnO₂ could be
84 expected to facilitate electron transfer and oxidize sulfides to elemental sulfur and sulfates. The
85 efficacy and suitability of the adsorbent are evaluated by determining the removal efficiency and
86 maximum uptake capacity of sulfide species. As the composite adsorbent is synthesized from bio
87 derived PGC, the applicability of the adsorbent for sulfide removal from aqueous solution is
88 further encouraged.

89

90 **2. EXPERIMENTAL SECTION**

91 **2.1. Materials**

92 Alginic acid calcium salt, potassium permanganate, and ethanol were purchased from
93 Sigma Aldrich, USA, and sodium sulfide (Na₂S·9H₂O) was obtained from Fisher Scientific. All
94 chemicals were of analytical grade and hence used without further purification. Deionized water
95 was used in the preparation and dilution of all solutions. Sulfide model solutions were prepared

96 by dissolving crystals of $\text{Na}_2\text{S}\cdot 9\text{H}_2\text{O}$ in deionized water and passing nitrogen gas to avoid
97 oxidation of sulfide. Various concentrations of sulfide solutions were prepared by further
98 diluting the prepared model solution with deionized water.

99

100

101 **2.2. Synthesis of PGC, MnO_2 , and MnO_2 -PGC Composites**

102 First, porous graphitic carbon (PGC) was synthesized by annealing and subsequent
103 carbonization of alginic acid calcium salt as described in our earlier work (Edathil et al., 2017).
104 To prepare the MnO_2 -PGC composites, equal quantities of KMnO_4 and PGC were added to 60
105 ml of distilled water under magnetic stirring to form a homogeneous distribution of the precursor
106 solution. After stirring for 30 minutes, 20 mL of ethanol was added dropwise and the suspension
107 was stirred for 12 h at room temperature to allow slow growth of MnO_2 nanoparticles on the
108 carbon. The obtained composite particles were then filtered and washed repeatedly with enough
109 quantities of DI water until the pH reached 7. The final product abbreviated as MnO_2 -PGC was
110 dried at 353 K overnight and stored for further use. Besides, pure MnO_2 particles were also
111 prepared using a similar approach, but in the absence of PGC. The synthesized samples were
112 used as adsorbents directly for all the adsorption experiments performed in this study. Fig. S1 in
113 supplementary section illustrates the experimental procedure used in this study for the synthesis
114 of pure and composite adsorbents based on wet chemical deposition technique

115

116 **2.3. Material Characterization**

117 The surface morphology and microstructure of the adsorbents before and after sulfide
118 adsorption were analyzed using FEG Quanta 250 scanning electron microscopy (SEM) and FEI
119 Tecnai G20 transmission electron microscopy (TEM). Prior to the SEM analysis, adsorbent

120 particles were sputter-coated with a conductive layer of gold-palladium (Au/Pd, 3 nm thickness).
121 The zeta potential of the adsorbent samples was measured using Zeta PALS instrument
122 (Brookhaven Instruments Corporation, USA), and elemental analysis was recorded using energy
123 dispersive X-ray spectrometer (Oxford-EDX, UK) fitted to the SEM. Further, the crystalline
124 structure of the adsorbent materials was determined using analytical X'Pert PRO Powder
125 Diffractometer (Cu-K α radiation 1.5406 Å, 40 kV, 40 mA) in the 2 θ range of 5°–80°.

126

127 **2.4. Adsorption Experiments**

128 Batch adsorption experiments were conducted by adding a certain mass of synthesized
129 adsorbent to about 10 ml of aqueous sulfide solutions with different initial concentrations
130 ranging from 1 mg/L to 200 mg/L in 50 ml stoppered conical flasks. The mass of the adsorbent
131 was varied between 3 and 11 g per 10 ml of sulfide solution to simulate the change in dosage
132 conditions. The flasks were placed in a shaking water bath (Daihan, Korea) maintained at 298 K
133 and subjected to continuous agitation at 140 rpm until equilibrium was attained. It is later shown
134 in the study that the optimum contact time to reach equilibrium for all cases was around 180 min.
135 Sulfide concentrations before and after the adsorption process were measured and analyzed, as
136 demonstrated in section 2.5. All the tests were performed in duplicates. Based on the initial (C_0)
137 and residual equilibrium concentration (C_e), percent removal, and adsorbent uptake capacity at
138 equilibrium (q_e) were calculated, as shown in our previous work (Edathil et al., 2017).
139 Additionally, adsorption experiments were conducted for different contact times (from 1 to 240
140 min) at fixed process conditions of 200 mg/L initial sulfide concentration, 298 K, and pH 12.

141

142 **2.5. Measurements of Sulfide**

143 To measure the initial and residual dissolved sulfide concentration in the aqueous
144 solution, 200 μL of pipetted samples were analyzed using LCK 653 sulfide detection kit on UV-
145 vis Spectrophotometer (DR5000, Hach Lange) by the methylene blue method. The sulfide test is
146 based on the reaction of sodium sulfide with N, N-dimethyl-p-phenylenediamine oxalate to
147 directly form methylene blue complex. The intensity of the blue color, as measured by the UV-
148 vis spectrophotometer using Test kit 653 is assumed to be directly proportional to the amount of
149 sulfide present in the original sample (E. Sheppard and H. Hudson, 2002).

150

151 **3. RESULTS AND DISCUSSION**

152 **3.1. Adsorbent Characterization**

153 The morphology and microstructure of the synthesized adsorbents, including $\delta\text{-MnO}_2$ and
154 $\text{MnO}_2\text{-PGC}$ composites, were observed using Scanning Electron Microscopy images, refer Fig.
155 1(a) and 1(e). In addition, EDX data presented in Fig. 1(b) and 1(f) serve to determine the
156 elemental composition of the adsorbents. The surface morphology of $\delta\text{-MnO}_2$ exhibited both
157 dense nanosized particles in a size range of 100-200 nm and micro-sized balls. EDX spectra of $\delta\text{-}$
158 MnO_2 revealed the presence of both manganese and oxygen with trace quantities of other
159 elements from the coating process. With the addition of PGC, it could be noticed that the porous
160 interconnected microstructure of carbon acts as a basic building block upon which $\delta\text{-MnO}_2$
161 nanoparticles are deposited. The EDX spectra of $\text{MnO}_2\text{-PGC}$ revealed the distinct pattern peaks
162 of magnesium in addition to the peaks of carbon, oxygen, and calcium which are the major
163 constituent elements present in the PGC. The coexistence of all these elements in the obtained
164 EDX results clearly proves the formation of $\text{MnO}_2\text{-PGC}$ composites. The SEM images of spent
165 (sulfide adsorbed) $\delta\text{-MnO}_2$ and $\text{MnO}_2\text{-PGC}$ composite has been illustrated in Fig. 1(c) and 1(g)
166 with the corresponding EDX results in Fig. 1(d) and 1(h). It could be noted that following the

167 adsorption process using δ -MnO₂, the adsorbent surface underwent structural changes and
168 predominantly displayed small aggregates of elemental sulfur and sulfate nanoparticles,
169 suggesting successful adsorption/oxidation of sulfide. The presence of Na and S in the EDX
170 results, see Fig. 1(d) further confirms that sulfide has been oxidized to sodium sulfate and/or
171 elemental sulfur. The composite adsorbent also showed the presence of irregular particles with
172 an aggregated surface on both the carbon walls as well as on the surface of MnO₂ nanoparticles.
173 Furthermore, EDX spectra of sulfide-adsorbed MnO₂-PGC shows a characteristic peak for sulfur
174 particles along with carbon, oxygen, and calcium. These results further confirm the successful
175 adsorptive oxidation of sulfide on the surface of the adsorbent to calcium sulfate and/or
176 elemental sulfur.

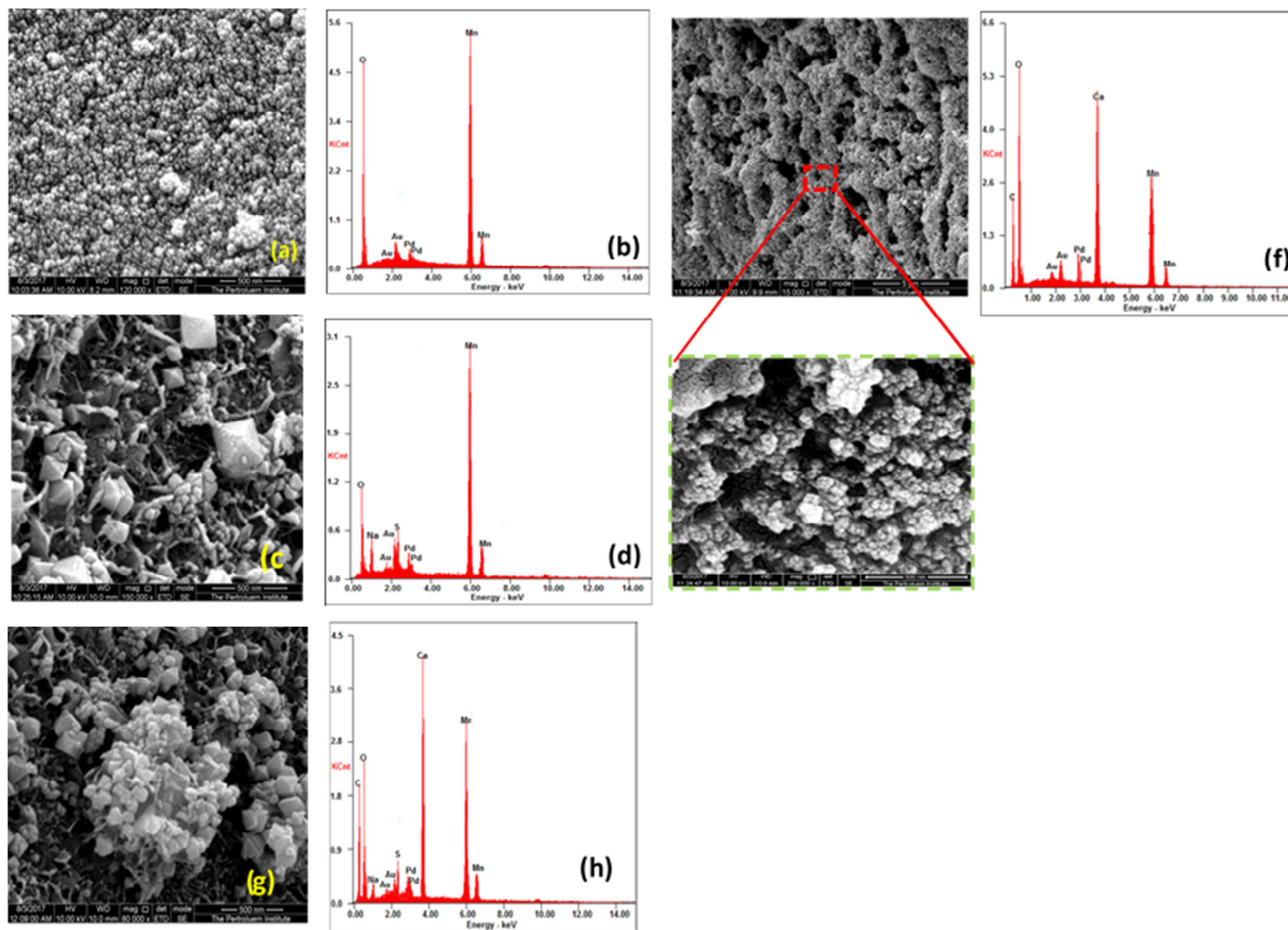


Fig. 1: Scanning Electron Microscopy (SEM) and EDX results of nanoparticle composites: (a-b) fresh MnO₂ (c-d) spent MnO₂ (e-f) Fresh -MnO₂-PGC composite (g-h) sulfide adsorbed MnO₂-PGC composite.

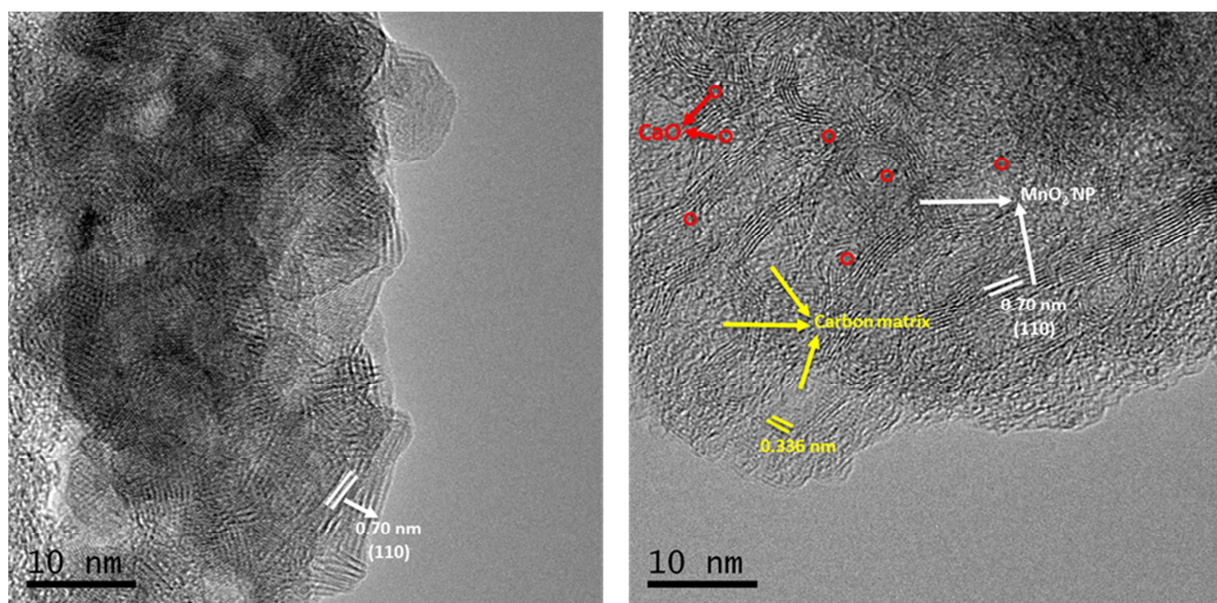


Fig. 2: Transmission Electron Microscopy (TEM) images of synthesized (a) δ - MnO_2 and (b) MnO_2 -PGC composite.

177 To better understand the changes in morphological microstructure induced by in-situ
 178 composite synthesis, TEM micrographs of δ - MnO_2 and MnO_2 -PGC composite were recorded at
 179 higher magnifications and are shown in Fig. 2(a) and 2(b). TEM images of δ - MnO_2 (Fig. 2(a))
 180 revealed the nanoscale architecture of MnO_2 particles with significant agglomeration, which
 181 agrees well with the SEM results. The lattice fringe spacing is 0.7 nm corresponding to the (110)
 182 plane of δ - MnO_2 (Subramanian et al., 2008). On the other hand, it can be noticed from the TEM
 183 image of MnO_2 -PGC composite that the MnO_2 nanoparticles are interconnected and uniformly
 184 distributed on the surface of the PGC. Along with the lattice fringe of 0.336 nm indexed to (002)
 185 plane of graphitic carbon, the composites also showed the lattice fringe spacing corresponding to
 186 the (110) plane of δ - MnO_2 . Furthermore, the presence of microcrystalline domain of calcium
 187 nanoparticles (indicated by the red circle) that are formed by the special 'egg-box' structure of the

188 alginate precursor containing organic calcium salts was observed in the TEM image of the
 189 composites (Edathil et al., 2017).

190

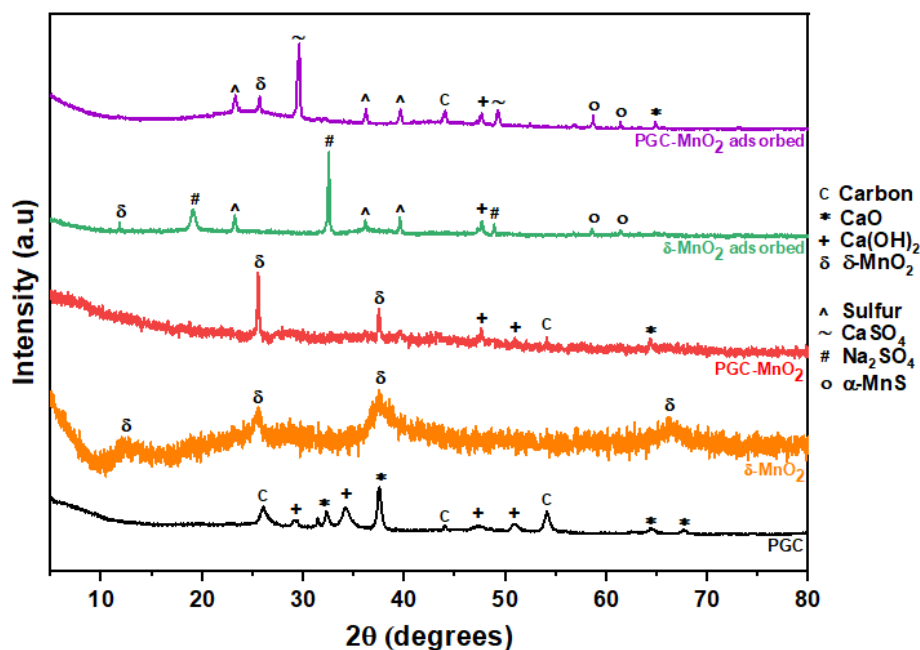


Fig. 3: X-ray diffractograms of various fresh and spent adsorbents.

191 Fig. 3 shows representative X-ray diffractograms of both fresh and spent composite
 192 adsorbents in addition to fresh and spent δ -MnO₂ adsorbents and raw PGC. In porous graphitic
 193 carbon, the prominent Bragg reflection observed at 26.1°, 44°, and 54° corresponds to the (002),
 194 (101) and (004) planes of the graphitic carbon matrix (JCPDS file number 41-1487).
 195 Additionally, the diffractogram also showed the presence of calcium oxide and calcium
 196 hydroxide particles in the carbonaceous matrix. The diffractogram of δ or Birnessite type MnO₂
 197 (JCPDS no. 43-1456) showed characteristic diffraction peaks at 12.8°, 24.8°, 37.6°, and 66.4°
 198 attributed to (001), (001), (111) and (311) planes. In the diffractogram of fresh MnO₂-PGC
 199 composite, the position of the main diffraction peak of graphitic carbon and δ -MnO₂ was well

200 retained. On the other hand, XRD of sulfide adsorbed δ -MnO₂, and MnO₂-PGC composite
201 clearly indicated the presence of additional peaks with higher intensity. The oxidation of sulfide
202 components by δ -MnO₂ and MnO₂-PGC to elemental sulfur could be confirmed by the presence
203 of predominant peaks (labeled by ^ in Fig. 3) observed at 23.3°, 36.2° and 39.5° that correspond
204 to the (222) plane of orthorhombic sulfur having S₈ structure (JCPDS 74-1465). Moreover, the
205 XRD of spent δ -MnO₂ showed the presence of additional peaks at 19.1°, 32.5° and 48.9°
206 (labeled by # in Fig. 3) corresponding to the (111), (200) and (300) planes of sodium sulfate
207 (Na₂SO₄). However, the diffractogram of sulfide adsorbed MnO₂-PGC composites showed
208 dominant peaks at 29.5° and 49.3° related to the (202) and (600) planes of CaSO₄, indicating the
209 formation of calcium sulfate complex (labeled by ~ in Fig. 3). The presence of additional peaks
210 in spent adsorbents further verifies that oxidation of sulfide ions has occurred.

211

212 **3.2. Adsorption of Sulfide Ions by Synthesized Adsorbents**

213 **3.2.1. Effect of Solution pH**

214 The effect of solution pH on sulfide removal from aqueous solution was investigated
215 under identical conditions ($C_0 = 202$ mg/L, $m = 0.01$ g, $t = 180$ min, $T = 298$ K) for both MnO₂
216 and MnO₂-PGC composites. Adsorption experiments were performed at different pH values in
217 the range of 3 to 12, and the corresponding adsorbent removal efficiencies are illustrated in Fig.
218 4. The data indicates that the adsorption behaviour of both the adsorbents was not affected by the
219 solution pH, and the percent removal was marginally higher for the MnO₂-PGC composite than
220 MnO₂ nanoparticles. In aqueous solutions, sulfides mainly exist in the form of H₂S_{aq}, HS⁻ and
221 S²⁻ ions. Under strongly acidic conditions with pH <6, sulfides are mainly present in the form of
222 H₂S_{aq} and HS⁻, while it contains negligible S²⁻ ions. Whereas at higher pH > 6, the aqueous

223 solution predominantly contains S^{2-} along with HS^- ions, and the concentration of HS^- ions
 224 further increase

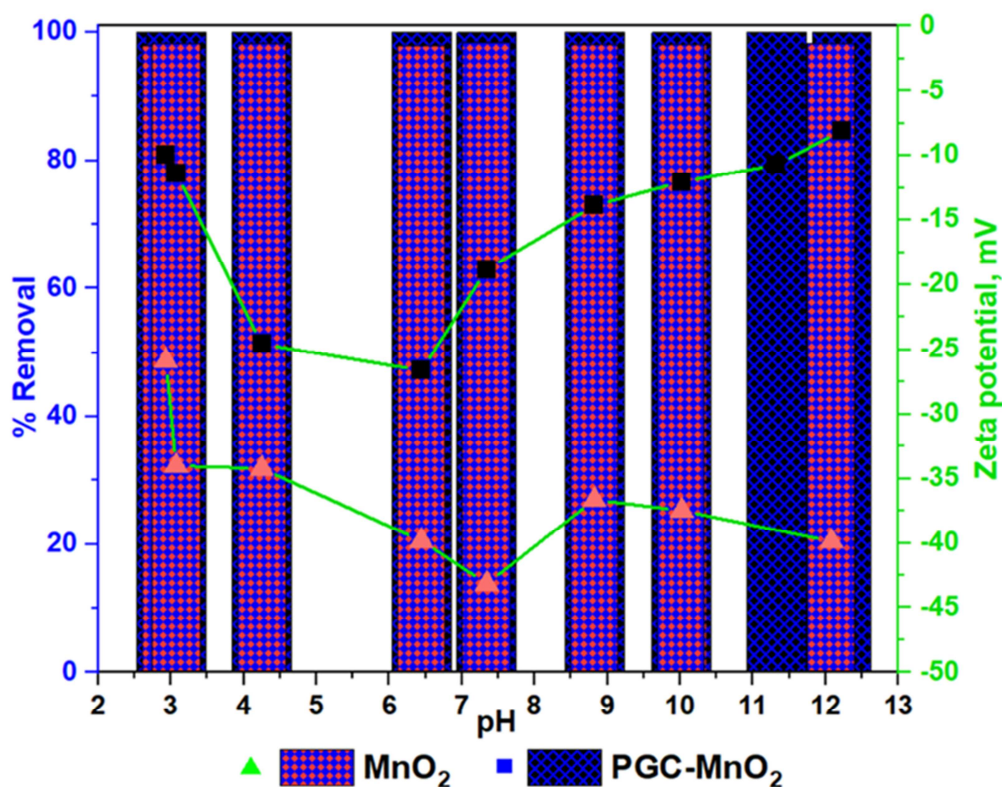


Fig. 4: Effect of pH on sulfide removal using different adsorbents.

225 under strongly alkaline conditions (pH 9 to 12). The obtained pH results clearly indicates that the
 226 adsorptive oxidation of sulfide by MnO_2 and MnO_2 -PGC was not hindered by adsorption sites as
 227 well as the competitive adsorption. Henceforth, the adsorption process of sulfide is found to be
 228 less affected by initial solution pH, inferring that the developed composite adsorbent holds the
 229 potential to effectively adsorb sulfide from aqueous solution at all pH. Zeta potential
 230 measurements were carried out with the aim of understanding (1) the pronounced selective
 231 adsorption characteristic exhibited by δ - MnO_2 and MnO_2 -PGC for sulfide species, (2) the effect

232 of surface charge on sulfide adsorption, and (3) the stability of the system. It was interesting to
233 observe that both adsorbents exhibited high surface negative charge at all solution pH. Since the
234 surface charge of the as-prepared adsorbents was negative in the experimental pH range as
235 indicated by the Zeta potential (Fig. 4), most likely chemisorption is caused by an electron
236 transfer reaction with the surface-active sites. The zeta potential of δ -MnO₂ ranging from -25 to -
237 40 mV was caused by the presence of MnO groups on the surface of δ -MnO₂. MnO₂-PGC
238 composite also showed high negative surface charge and may be attributed to the presence of
239 carboxyl and hydroxyl groups obtained from the alginate molecules in addition to the MnO-
240 groups from δ -MnO₂ particles. Even though the absolute values of the zeta potential for both
241 these adsorbents under the investigated pH range (3 to 12) were high (suggesting its good
242 stability in the colloidal state), the composites exhibited slightly higher sulfide removal
243 efficiency. This could be attributed to the better accessibility of the active sites owing to the
244 interconnected porous structure of the carbon. Thus, the active functional groups present on the
245 surface of the developed adsorbents were believed to be less affected by the initial solution pH,
246 thereby contributing to the extraordinary adsorption efficiency showcased all pH conditions.
247 Henceforth, all further adsorption experiments were carried out at the original solution pH of
248 12.06.

249

250 3.2.2. Effect of Ionic Strength

251 The possible presence of background salts in sulfide containing industrial wastewater
252 tends to form complex metals that might compete with sulfide species for available adsorption
253 sites. The influence of ionic strength on sulfide removal efficiency by the nanocomposite
254 adsorbents was assessed through the addition of NaCl and CaCl₂ to the sulfide solution. The

255 concentration of background electrolytes in the sulfide solution was varied from 0 to 1 M.
256 Adsorption studies were conducted in a batch mode at a temperature of 298 K, adsorbent dosage
257 of 1 mg/L, and initial sulfide concentration of 202 mg/L. Adsorption results as shown in Fig S2,
258 showed no significant change in removal efficiency after the addition of background electrolytes
259 to the sulfide solution.

260

261 3.2.3. Effect of Adsorbent Dose

262 The effect of adsorbent dose on sulfide adsorption by MnO_2 and MnO_2 -PGC
263 nanocomposite has been presented in Fig. 5. Experiments were performed at the following
264 conditions: initial sulfide concentration of 202 mg/L, 180 min, 298 K, and a solution pH of
265 12.06. Adsorbent mass was varied between 2.5 and 20 mg that corresponds to a dosage of 0.25
266 g/L to 2 g/L. It can be noticed that the removal efficiency increases with adsorbent dosage till ca.
267 1 g/L, at which point the efficiency reaches a maximum. The initial increase in removal
268 efficiency is a direct result of increased contact surface area, more specifically the active sites
269 offered by the adsorbent. However, with further increasing the adsorbent dosage, the effective
270 surface area is significantly affected, resulting from overlapping or aggregation of sulfide
271 molecules near the adsorption site (Ahluwalia and Goyal, 2007). As a result, all the active sites
272 are not fully utilized, thereby leading to a decrease in the adsorption capacity, as evidenced in the
273 SEM images, refer Fig. 1e.

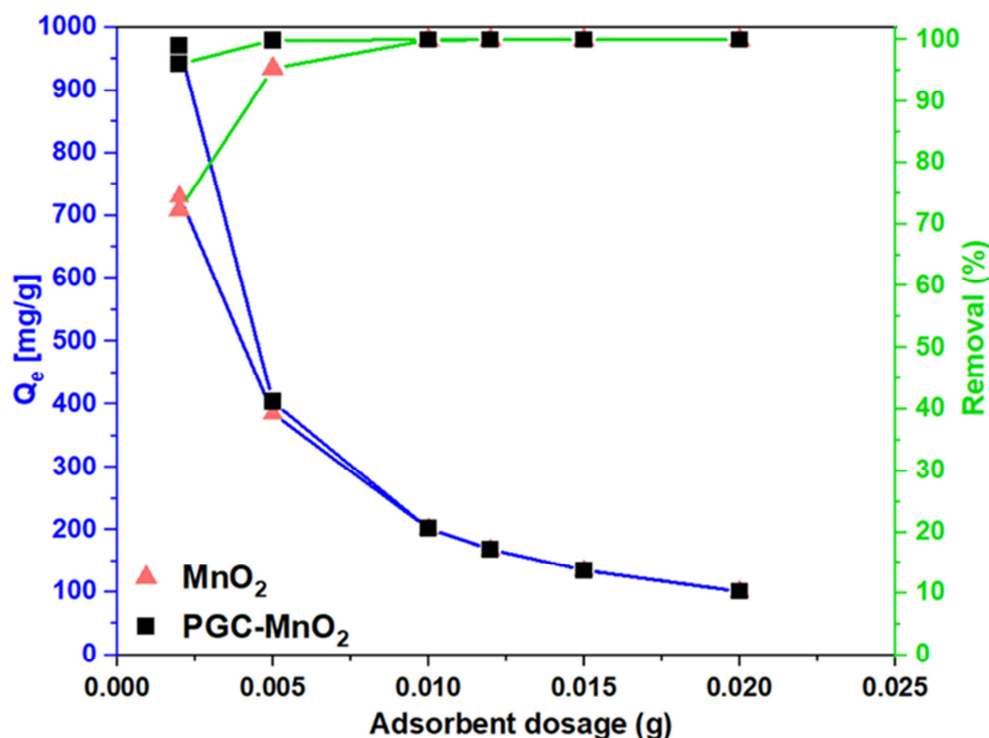


Fig. 5: Effect of adsorbent mass on sulfide removal using different adsorbents.

274 3.2.4. Effect of Initial Sulfide Ion Concentration

275 The amount of sulfide ions adsorbed is proportionally controlled by the initial
 276 concentration of sulfide ions in the solution making it a crucial parameter for sensitivity analysis.
 277 All the parameters adsorbent dosage (1 g/L), agitation time (180 min), temperature (298 K), and
 278 pH (12.06) except initial concentration were kept constant. The effect of initial ion concentration
 279 (varying from 0 to 600 mg/L) on equilibrium adsorption capacity and removal efficiency of
 280 sulfide ions on the adsorbent is shown in Fig. 6. As shown, sulfide removal efficiency for the
 281 MnO₂ nanoparticle sample exhibited a gradually decreasing trend till 300 mg/L, beyond which a
 282 sharp decrease could be noticed. A similar trend could be observed for the nanocomposite
 283 sample, however, less pronounced.

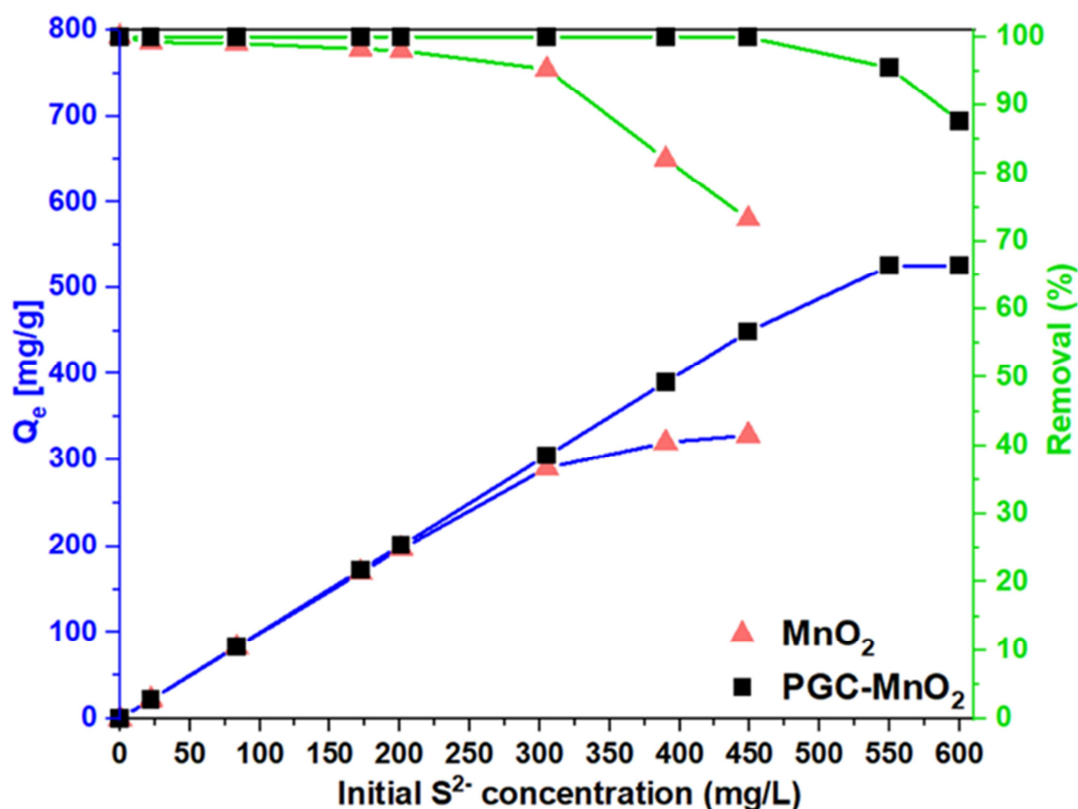


Fig. 6: Effect of initial sulfide solution concentration on sulfide removal using different adsorbents.

284 Contrastingly, with an increase in initial sulfide ion concentration, an increase in
 285 adsorption capacity for both samples could be noticed. The steady increase could be attributed to
 286 the increased local concentration gradient of sulfide ions between the solid and aqueous phase
 287 that subsequently results in higher sulfide ion fixation at the surface area and maximum
 288 utilization of the available active sites (Barka et al., 2013). However, when the active sites are
 289 saturated with sulfide ions, the equilibrium adsorption capacity remains constant. The maximum
 290 adsorption capacity is significantly higher for the composite (505 mg/g) in comparison to the

291 MnO₂ nanoparticle (ca. 310 mg/g), thereby indicating the positive impact of introducing δ-MnO₂
 292 particle into the interconnected morphology of the porous graphitic carbon.

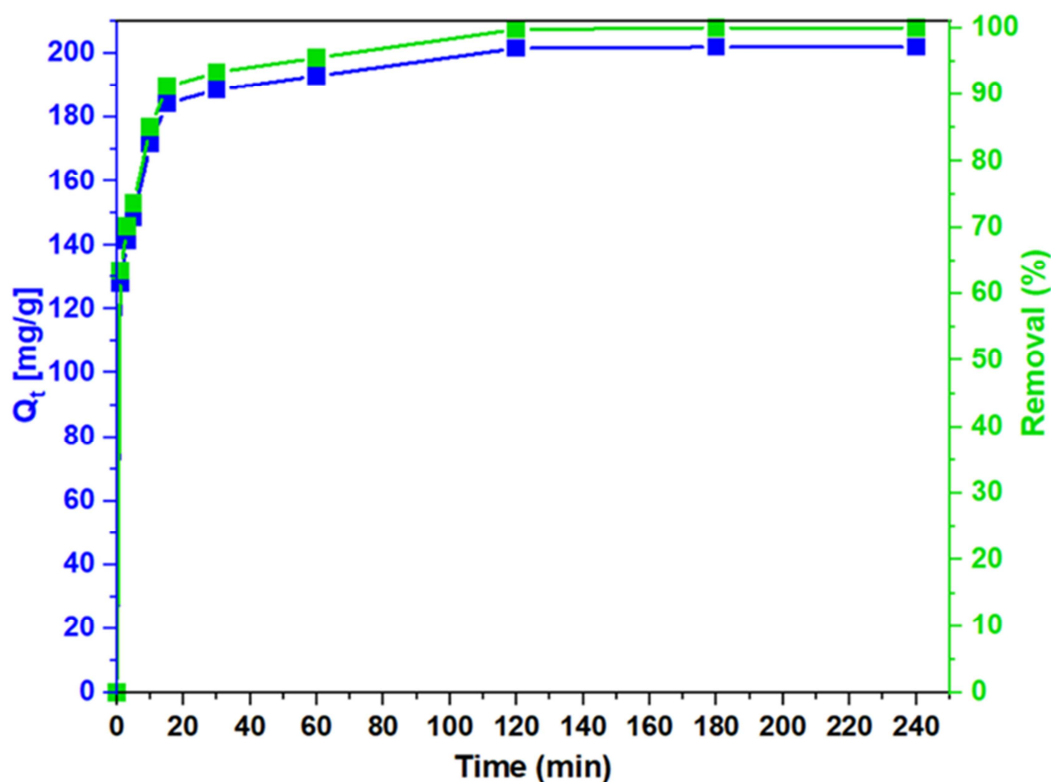


Fig. 7: Effect of contact time on removal efficiency and uptake capacity.

293 3.2.5. Effect of Contact Time

294 In order to determine the time required for achieving adsorption equilibrium, it is
 295 significant to assess the influence of agitation time on adsorption capacity and efficiency. Fig. 7
 296 depicts the effect of agitation time on the adsorption of sulfide ions over MnO₂-PGC adsorbent at
 297 fixed conditions of initial concentration (202 mg/L), adsorbent dosage (1 g/L), temperature (298
 298 K), and pH (12.06). At the early stages of adsorption ($t < 20$ min), a rapid increase in removal
 299 efficiency and adsorption capacity could be observed. Beyond 20 minutes, the effect gradually

300 diminished until it displayed no significant increase beyond 120 minutes. The residual
301 concentration at 180 min was found to be approximately about 0.8% of that obtained after 240
302 min. Accordingly, a quasi-equilibrium condition was assumed to have been reached at 180 min,
303 and henceforth all succeeding batch experiments were conducted for 180 min. The pronounced
304 increased rate at early stages could be attributed to the availability of abundant vacant active sites
305 on the adsorbent. As adsorption proceeds, sulfide ions gradually occupy the vacant sites at a
306 much slower rate until a point of saturation. The decreased sorption rate is possibly due to the
307 larger diffusion path lengths deeper into the adsorbent pores where the sulfide ions encounter
308 higher mass transfer resistance. No significant change in sulfide concentration was observed
309 after 180 min as all sites have been occupied, and equilibrium is established.

310

311 3.3. Adsorption Kinetic Studies

312 To evaluate the adsorption rate and elucidate the reaction mechanism of sulfide ions on
313 MnO₂-PGC composites, experimental data were analyzed using the frequently employed kinetic
314 models, including pseudo-first-order (PFO), pseudo-second-order reaction (PSO), and
315 intraparticle diffusion (IPD) models. In a well-agitated batch system, the resistance offered by
316 the film is negligible in comparison to the adsorbent internal microstructure (surface and pore).
317 The diffusion mass transfer can be captured by an apparent diffusion coefficient that ensembles
318 the different steps involved in the intraparticle diffusion process. The behavior of intraparticle
319 diffusion could be explained by the Weber & Morris intra-particle diffusion model (IPD) as: (Dil
320 et al., 2016; Nekouei et al., 2015; Weber and Morris, 1963)

$$321 \quad q_t = k_i t^{0.5} + C \quad (1)$$

322 where k_i is the intra-particle diffusion rate constant ($\text{mg/g} \cdot \text{min}^{0.5}$) and C is the empirical constant
323 (mg/g). The value of C depends on the film boundary layer thickness wherein a larger value of C
324 represents a significant effect of the boundary layer on adsorbate diffusion (Kannan and
325 Sundaram, 2001). Typically, the rate-controlling step is deduced by analyzing the linear
326 relationship between q_t and $t^{0.5}$, as shown in supplementary file Fig. S3. It can be noticed that
327 the experimental data exhibits three different linear parts (I, II, III), each possibly indicating
328 different stages of intra-particle diffusion. The first part refers to the least-resistive external
329 surface adsorption or macro-pore diffusion, the second part to the relatively less-accessible
330 mesopores, and the third part to micropore diffusion (Cheng et al., 2013). It is evident that the
331 linear part of the diffusion curve (step I) does not pass through the origin, and therefore the
332 diffusion process might not be solely controlled by any specific stage but is probably influenced
333 by multiple steps. The corresponding rate constants and intercept for the three parts are denoted
334 as k_{i1} , C_1 , k_{i2} , and k_{i3} , and are summarized in Table 1. It can be noted that the rate constants
335 gradually decrease from $16.72 \text{ mg/g} \cdot \text{min}^{0.5}$ (step 1) to 3.94 (step II) to 0.09 (step III), strongly
336 indicating increasing diffusion resistance with the progress of the adsorption process. Stage I is
337 predominant when there are numerous vacant sites in the adsorbent particle during the initial
338 stages. However, during stage 2, most of the active sites on the surface are saturated, and hence
339 intra-particle diffusion is limited by the interior mesopores. Finally, at the last step, the sulfide
340 ions diffuse towards micropores and establish equilibrium between the solid and dissolved
341 phases. Moreover, the increasing value of intercept C indicates the deviation from the
342 dominating rate-controlling mechanism as a result of the increasing boundary layer thickness.

343 Kinetic data analysis using pseudo-first and second-order reaction models is frequently
344 employed to determine how fast adsorption equilibrium would be achieved. For the PFO reaction

345 model, adsorption rate constant (k_f) was determined by plotting $\ln(q_e - q_t)$ against t for sulfide
346 ion adsorption on MnO_2 -PGC composite at an initial concentration of 202 mg/L and 298 K.
347 Values of equilibrium loading (q_e) and second-order rate constant (k_s) for the PSO model was
348 obtained from a linear plot of t/q_t versus t , refer to supplementary file Fig. S4. Model
349 parameters, including rate constants and equilibrium loading, were obtained through linear
350 regression, and the accuracy of the fit was evaluated from the regression coefficient (R^2).
351 Further, in order to assess the error propagated through linearization, the constants were also
352 evaluated using non-linear forms of the model equations and compared with the results from
353 linear forms. A summary of model equations, along with the regressed parameters from different
354 models, have been compiled in Table 1. It could be noticed that both PFO and PSO reaction
355 models predict experimental data reasonably well, as evidenced by the high values of the
356 regression coefficient. Despite the good fit of the PFO linear model, the values of both constants,
357 namely rate constant and equilibrium capacity, are vastly different from the PFO non-linear and
358 PSO model estimates. It should be remembered that the PFO model is applicable only during
359 initial adsorption stages and high adsorbate solution concentration (Wang and Guo, 2020), and
360 thus employing it for larger time frames would induce significant error. The low value of
361 equilibrium adsorbent loading estimated by the PFO linear model could be a direct consequence
362 of extending the model for a wider time step. The q_e values estimated by the PSO linear and
363 non-linear models are in good agreement with the experimentally calculated equilibrium loading
364 values ($q_{e,\text{exp}}$).

365

366

Table 1: Summary of kinetic model equations and parameters of MnO₂-PGC composite

Model		Equation	Rate constants	q _e (mg/g)		R ²
				q _{e, exp}	q _{e, cal}	
PFO	Linear	$\ln(1-(q_t/q_e)) = -k_f t$	$k_f = 0.04 \pm 0.0018$	201.9	56.4 ± 0.9	0.954
	Non-linear	$q_t = q_e(1 - e^{-k_f t})$	$k_f = 0.86 \pm 0.02$		184.9 ± 2.1	0.903
PSO	Linear	$t/q_t = t/q_e + (1/k_s q_e^2)$	$k_s = 0.0028 \pm 0.0005$	201.9	204.1 ± 0.6	0.999
	Non-linear	$q_t = (k_s q_e^2) t / (1 + k_s q_e t)$	$k_s = 0.0065 \pm 0.0009$		194.7 ± 1.1	0.967
IPD	--	$q_t = k_i t^{(1/2)} + C$	$k_{i1} = 16.72 \pm 1.2$	201.9	---	0.99
			$C_1 = 111.74 \pm 2.1$			0.77
			$k_{i2} = 3.94 \pm 1.5$			0.79
			$k_{i3} = 0.09 \pm 0.05$			

352 3.4. Adsorption Isotherms

353 The experimental data of adsorption isotherms were analysed using three different
354 models, namely Langmuir, Freundlich, and Temkin. The standard mathematical equations
355 describing the models could be found widely in literature, and hence is not presented in this
356 work. Isotherm parameters were estimated by linear regression analysis and are listed in Table
357 S1 along with the corresponding model equations. As shown, the value of the regression
358 coefficient for the Langmuir model equation is 0.99 for both MnO₂ and composite samples. It is
359 an implication that sulfide ion adsorption on both samples follows a monolayer adsorption
360 process with no interaction between the adsorbed molecules. MnO₂-PGC Comparing the value of
361 Langmuir adsorption constant (k_L) between MnO₂ and composite sample, it can be inferred that
362 the affinity of sulfide ion adsorption on MnO₂ is higher than that of MnO₂-PGC composite.
363 However, due to increased surface area, the PGC composite possesses significantly higher
364 adsorption capacity than MnO₂ nanoparticle. The applicability of Freundlich isotherm for sulfide
365 adsorption on MnO₂ and PGC composite was also tested and validated with isotherm
366 experimental data. The solution concentration influence coefficient ($1/n$) value of 0.05 for MnO₂
367 sample strongly indicates favourable adsorption. However, the linear regression coefficient for
368 the MnO₂-PGC composite sample was 0.69, which is significantly smaller than that of the
369 Langmuir model. Similarly, the regression coefficient for the Temkin adsorption model is far
370 from unity indicating a non-linear relationship between $\ln q_e$ and $\ln C_e$. Therefore, sulfide ion
371 adsorption on MnO₂-PGC composite follows monolayer adsorption, and thus, Langmuir
372 adsorption isotherm is more suitable for modeling the equilibrium process. Based on the results,
373 the maximum sulfide adsorption capacity on MnO₂-PGC composite was estimated to be 526.3

374 mg/g. Compared with other sulfide adsorbents presented in literature, it can be seen from Table 2
 375 that MnO₂-PGC exhibited superior adsorption capacity.

Table 2: Comparison of sulfide adsorption capacities for different adsorbents

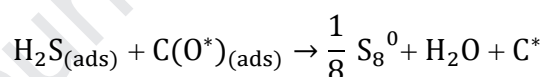
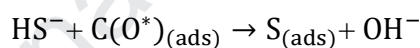
Adsorbent	Initial Concentration (ppm)	Adsorption capacity (mg/g)	Reference
Granular ferric hydroxide (GFH)	19.8 ± 0.6	29.1 ± 0.6	(Sun et al., 2014)
Alg/Iron Oxide-NP	64.3	136.9	(Pal et al., 2018)
Activated Carbon (AC) - 500°C	0-1000	58.8	(Hariz and Monser, 2014)
PGC	45	149.25	(Edathil et al., 2017)
GSH Composites	202-450	370.4	(Achazhiyath Edathil et al., 2019)
CeO ₂ -NiAl-LDHs coated activated carbon	0.1 M	181.15	(Achazhiyath Edathil et al., 2019)
MnO ₂ nanoparticle	0-450	303.03	This work
MnO ₂ -PGC	0-600	526.32	This work

376 3.5. Reaction Mechanism

377 The MnO₂-PGC composite was employed for sulfide removal in order to exploit the
 378 advantages of the oxidative nature of MnO₂ and the surface functionality of PGC offered by
 379 oxygen functional groups. To further understand the mechanism involved in
 380 adsorption/oxidation, it is of great importance to understand the elementary reaction step
 381 involved in the dissolution of crystalline hydrate of Na₂S in water. In aqueous alkaline solution,
 382 dissolution of Na₂S solution yields sulfides [S_{aq}²⁻], bisulfides [HS_{aq}⁻] and aqueous H₂S [H₂S_{aq}]

383 (Linkous et al., 2004). Thus, the interaction of the dissolved sulfur species with oxygen
 384 functional groups present on the PGC and the MnO₂ nanoparticles results in the distribution of
 385 sulfides oxidation products over the composite adsorbent surface. The C(O*)_(ads) species which is
 386 the oxygen-containing active sorption site and/or radical of the form C(O*) on the carbon
 387 surface, are believed to be responsible for the successful adsorptive oxidation of sulfide to
 388 different species such as elemental sulfur and calcium sulfate. When aqueous hydrogen sulfide
 389 ions contact the graphitic carbon surface, it undergoes oxidative decomposition to produce sulfur
 390 atoms. Sulfur atoms react in a substitution reaction with the C(O) surface complex and in an
 391 addition reaction with radical C* to form C-S complexes and continue until the formation of
 392 elemental sulfur chains (S₈). The possible redox reaction involved in the formation of elemental
 393 sulfur by PGC is illustrated as below:

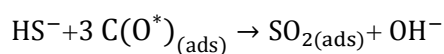
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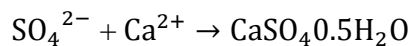


395

396 In aqueous medium, bisulfides (HS⁻) reacts with the oxygen functional groups to form sulfur
 397 oxides, SO_{2(ads)} and SO_{3(ads)} and is as evidenced in the literature (Brazhnyk et al., 2007; Lemos
 398 et al., 2012). These sulfur oxides further react with water resulting in the formation of sulfate
 399 ions (SO₄²⁻) that continues to react with calcium metal ions present in the PGC matrix to form
 400 calcium sulfates. XRD further confirms the presence of CaSO₄.

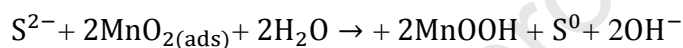
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404 The production of elemental sulfur [S_8^0] by MnO_2 proceeds through a series of surface complex
 405 formation initiated by the adsorption of HS^- onto the manganese oxide surface followed by
 406 oxidation as illustrated below:

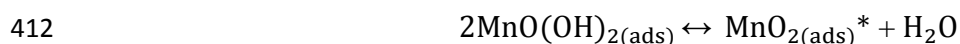
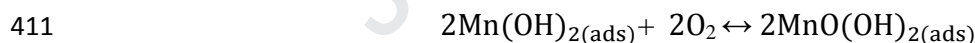
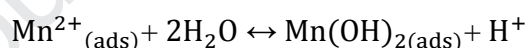
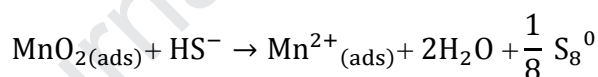
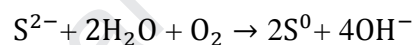
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409 With MnOOH as catalyst,

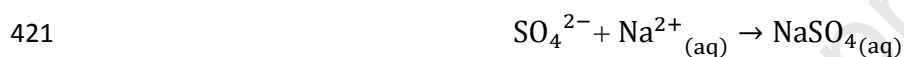
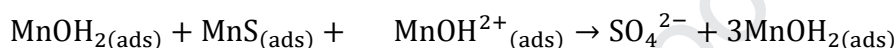
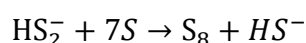
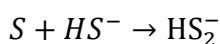
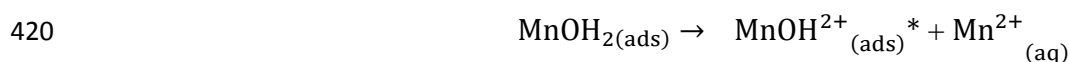
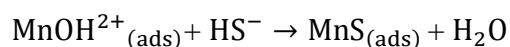
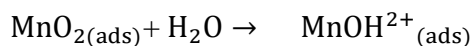
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413

414 The adsorbed HS^- ions also participate in redox reactions to form an intermediate metal
 415 surface complex MnS that could undergo two different competitive reaction pathways to form
 416 elemental sulfur and sulfates through the formation of zero-valent sulfur intermediate (Herszage
 417 and dos Santos Afonso, 2003).

418



422

423 Oxidation of $\text{S}_{\text{aq}}^{2-}$, HS_{aq}^- and $\text{H}_2\text{S}_{\text{aq}}$ species by MnO_2 -PGC composites was experimentally
 424 verified by the presence of sulfate in the form of calcium sulfate and elemental sulfur from XRD
 425 analysis. Results from EDX also confirm the participation of MnO_2 in the oxidizing reaction
 426 resulting in the formation of various sulfur species. In addition, with the deposition of MnO_2 on
 427 PGC, the maximum adsorption capacity was significantly enhanced when compared to bare
 428 PGC, which was reported to be 149.2 mg/g (Edathil et al., 2017). The high values of solid
 429 adsorbent loading and negligible liquid phase equilibrium concentrations at low sulfide initial
 430 concentration conditions are an indication of the formation of metal complexes, including
 431 calcium sulfate wherein the rate of adsorption is very high relative to the rate of desorption. The
 432 results obtained from XRD and EDX well support the combined effect of PGC and MnO_2 on
 433 oxidation of sulfide molecules. However, techniques for desorbing the sulfide contaminants from
 434 the adsorbent needs to be investigated before recovery and reuse of spent adsorbent could be
 435 envisaged.

436

437 CONCLUSION

438 The feasibility of employing the MnO₂-PGC composite adsorbent for the removal of
439 hazardous sulfide components from aqueous systems was investigated through batch adsorption
440 studies at different process conditions. MnO₂-PGC nanocomposite adsorbents were synthesized
441 via the in-situ chemical wet deposition method using PGC derived from calcium alginate as
442 carbon precursor. The synthesized fresh composite and spent adsorbent were examined using
443 TEM, SEM, EDX and XRD and revealed that the surface modification of PGC by MnO₂
444 nanoparticles helped in drastically enhancing the oxidative capability of bare carbon. It was
445 found that the removal efficiency of the adsorbent was not affected by the solution pH; however,
446 it was dependent on the initial sulfide ion concentration. Kinetic studies inferred that adsorption
447 of sulfide ions by MnO₂-PGC composite was well-described by pseudo-second-order kinetic
448 model, confirming that chemisorption controlled the overall rate of sulfide sorption.
449 Experimental isotherm data confirmed the suitability of the Langmuir model for describing the
450 equilibrium conditions, and the maximum adsorption capacity was estimated to be 526.3 mg/g,
451 significantly higher than that of PGC. Results confirmed that the high adsorption capacity could
452 be attributed to the reactivity of bounded MnO₂, and oxygen atoms present on the active sites of
453 PGC with interconnected morphology that oxidized sulfide contaminants to sulfates and
454 elemental sulfur. In summary, the excellent adsorptive characteristics demonstrate that the
455 MnO₂-PGC composites can serve as an adsorbent material to remove hazardous sulfide
456 contaminants from aqueous solution.

457

458 Conflict of Interest

459 There are no conflicts of interest to declare.

460

461 **Acknowledgment**

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Adsorptive oxidation of sulfides catalysed by δ -MnO₂ decorated porous graphitic carbon composite

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Highlights

- δ -MnO₂/porous graphitic carbon nanocomposite synthesized by in-situ wet deposition
- Surface functionalized PGC and precipitated δ -MnO₂ catalyzed oxidation of sulfides
- Sulfides species converted to metal sulfates and sulfur, and removed by adsorption
- Equilibrium best-described by Langmuir model with an uptake capacity of 526.3 mg/g
- Kinetic intra-particle diffusion model suggested multiple rate-controlling steps

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Declaration of interests

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

None

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