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Distributed Collaborative Optimization of a Multi-Region Integrated Energy System Based on Edge Computing Unit

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The coordinated optimization scheduling of the integrated energy systems is vital in multi-energy complementarity and hierarchical utilization. However, the centralized optimization is inferior to the distributed optimization of the large-scale multiregion integrated energy system (MRIES) in data processing capacity and information security. This study proposes a distributed computing architecture based on the edge computing unit (ECU), which takes the energy hub as the main body and sets the partitioning principle and method of MRIES. The ECU can finally realize the whole-system collaborative optimization of MRIES, which contains electrical, natural gas, and district heating networks through internal autonomous optimization and boundary information interaction with the cloud computing center. At the same time, an improved nested algorithm based on the consensus-alternating direction method of multipliers is proposed, which ensures the convergence of the mixed-integer linear program and effectively improves the convergence speed. Combining the advantages of the model and algorithm provides a theoretical and algorithmic support for the optimization research of the MRIES.

Keywords: edge computing unit, multiregional integrated energy system, distributed collaborative optimization, energy hub, energy conservation

1 INTRODUCTION

Carbon peak and carbon neutrality targets put forward higher requirements for accelerating energy transformation in China. Therefore, the optimization of energy structure, energy conservation, and improvement of energy efficiency has become the most basic direction of energy development (Yunzhou et al., 2021). The construction of the IES is conducive to promoting the integration of source, network, load and storage, and multi-energy complementarity, which can realize the sustainable development for optimizing energy structure and improving energy efficiency. As the crucial part of IES research, RIES (Na et al., 2020) is mostly modeled in the form of EH. With EH as the main body, the RIES can be divided into functional units such as industrial areas, commercial areas, and residential areas. Based on the advantages of the geographical range, the RIES can conveniently realize the flexible optimization and scheduling decisions, which cannot be achieved without the assistance of multi-energy collaborative management, direct monitoring, and analysis of the operational data. Therefore, the RIES is an effective control and computing unit of IES intelligent evolution at present.

The IES distributed optimization has unique advantages over the centralized optimization in data acquisition cost, processing difficulty, application scale, information privacy, and security. A reasonable partition method of the IES and a suitable distributed algorithm are the fundamental problems of the IES distributed optimization. Haozhong et al. (2019) and Jianzhu Chen et al. (2019) used the different improved ADMM to conduct the distributed optimization of the IES based on the energy network decoupled. Jianzhu Chen et al. (2019) took CHP as the central part of the model and optimized the RIES in the distributed double layer, which took the delay of the bottom thermal ring network into account. In the study by Zhang et al., (2018), ADMM was adopted to optimize the pricing strategy of the multi-EH system with the underlying heating network. In the studies by Chen et al. (2018) and Chen et al. (2021), the static and dynamic characteristics of the EHs were taken into consideration and optimized, respectively. Zhang et al. (2018) proposed a multi-agent bargaining learning method, which optimized the large-scale IES in a distributed way, while the EH worked as the agent. Based on C-ADMM, Xu et al. (2019) improved the algorithm and analyzed the MRIES consisting of electrical, gas, and thermal three-ring networks with the four EHs. In comparison, Wen et al. (2017) used an improved method based on the C-ADMM dealing with the distributed optimization of a large-scale electric-gas system. ADMM was used for the distributed optimization of the multi-agent IES in the study by Haitao et al. (2021). Wu et al. (2020) used a hierarchical optimization method to carry out the distributed optimization of the electric-thermal system.

At present, the distributed collaborative optimization of the MRIES still has shortcomings:

- (1) The role of MRIES in energy management and allocation is weakened by the decoupling method based on the different energy networks, which will be more complicated with the increase of the number and types of coupling devices.
- (2) The distributed optimization with the EH as the main body does not consider the upper and lower energy network constraints. As a result, the global optimal solution cannot be obtained directly through the data interaction between the EHs.
- (3) There is lack of a suitable distributed algorithm considering the EH off-design performance to support the expansion of the MRIES.

Therefore, this study proposes a distributed computing architecture based on an ECU and develops an IES partitioning method corresponding to it. And then, this study puts forward an improved algorithm adapted to the distributed characteristics of the model, forming a complete set of distributed computing methods based on ECU.

With the EH as the main body, the ECU is equivalent to RIES in geographical scope and structural level. The global optimal scheduling scheme is finally obtained through optimization within the unit and information interaction with the cloud. This architecture not only protects the information privacy

and security of the RIES but also dramatically reduces the pressure of data transmission, storage, and processing in the cloud through edge computing, which reduces the difficulty of processing complex data of the IES. In addition, this study proposes a set of IES partitioning methods according to the connected positions of the EHs to reasonably partition ECU regions and provide a model basis for algorithm improvement. Based on the detailed RIES model, the improved C-ADMM nested algorithm fits the ECU model well, which can solve the nonconvergence problem caused by MISOCP and guarantee the optimization results with fewer iterations. They complement each other and provide a theoretical and methodological support for the MRIES distributed cooperative optimization.

In this article, the concept of the proposed ECU, modeling method, and improved algorithm are introduced in detail, and an example of the MRIES is used to verify the scalability and effectiveness of them.

2 EDGE COMPUTING UNIT FRAMEWORK FOR IES DISTRIBUTED OPTIMIZATION SCHEDULING

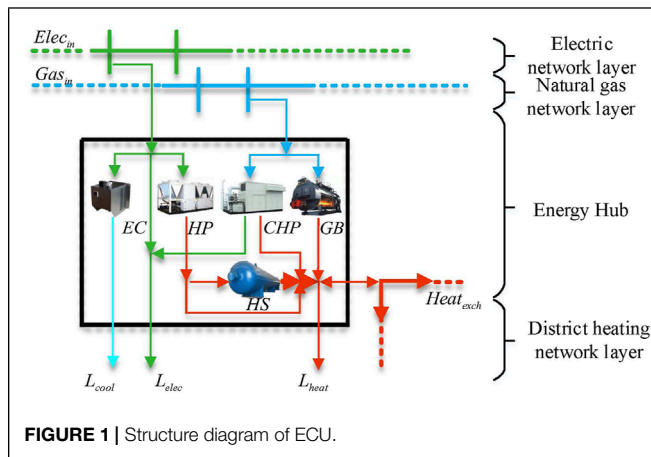
Internet of things, cloud computing, edge computing, and other technologies have played an important role in smart home management (Albatineh et al., 2020), power market (Chen S. et al., 2019), smart grid (Liu et al., 2021), (Cao et al., 2019), and other fields, but they have not fully emerged in the IES. Therefore, the ECU model proposed in this article will serve as a new energy management framework and provide a new idea for the unified management and coordinated scheduling of the IES multiple energy sources.

2.1 Framework of Edge Computing Unit

Corresponding to the cloud computing center in the IES, the ECU proposed in this article is the local energy data management unit, which can reduce cloud computing burden by finishing a part of the computing tasks at the local (Weisong et al., 2017). The structure of the ECU model presented in this article is shown in **Figure 1**.

EC, HP, CHP, and GB, as the coupling equipment convert power and natural gas into cold, heating, and power. Cooling and power are directly supplied to the local load, while the heating is transmitted to the HS or the DHN to jointly support the heating demand of the local load.

The modeling method of the upper radiant heat network is similar to that of the power grid and natural gas network. Therefore, the ring heating network is only established at the lower layer in this study for heat circulation. The ring network has high security and reliability (Wang et al., 2016), and the computing method for the ring network also meets the requirements of the radial heating network.



The ECU supports the multizone expansion, where the units are connected to each other through a power grid, natural gas network, and DHN, becoming the main body of the MRIES.

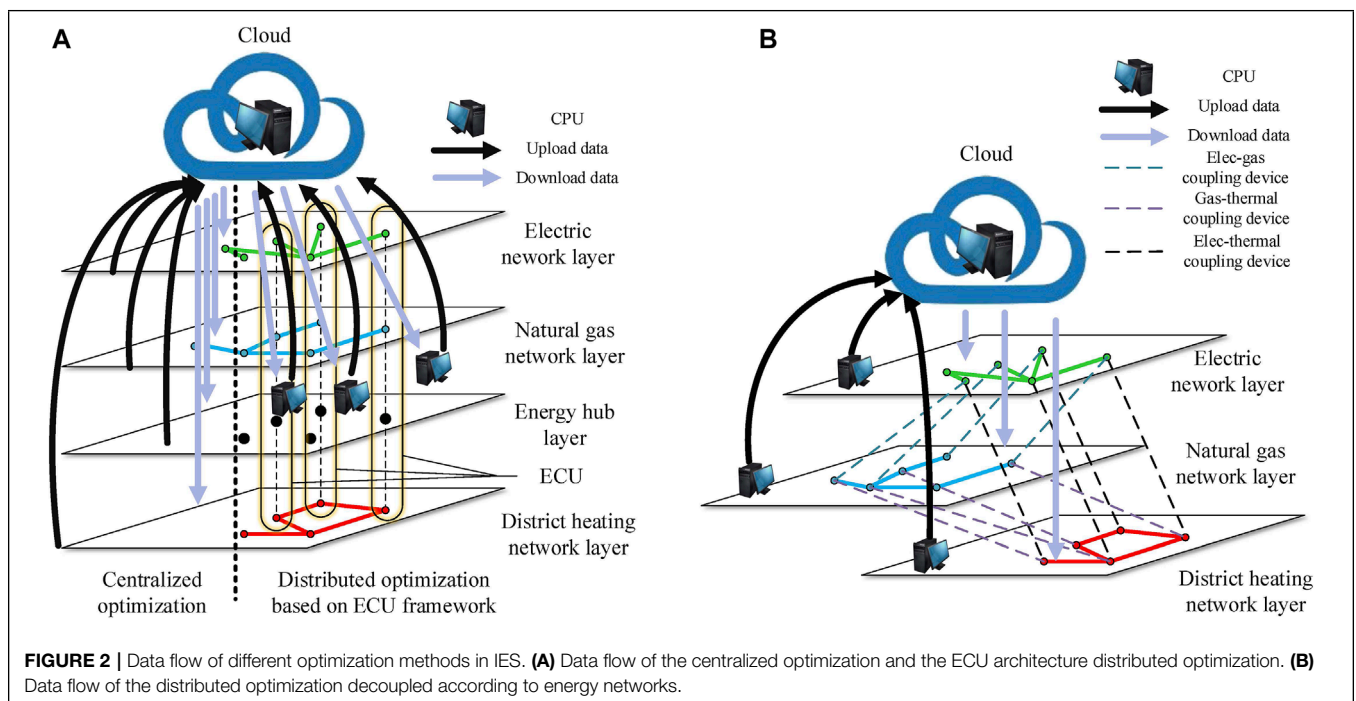
2.2 Data Exchange Process of Optimization Scheduling in Multiregion Integrated Energy System

The ECU obtains the data of the devices and nodes through the local awareness layer and submits the boundary information to the cloud after internal optimization. Then, the cloud feeds back the consensus information obtained from the centralized computing to each ECU. After that, the ECU adjusts the internal operation according to the consensus information. The MRIES achieves global optimization through several iterations.

The centralized optimization needs to submit all the device data to the cloud, which results in vast costs of communication facility construction, data transmission, storage, and processing. It deviates from the energy development idea of energy conservation and emission reduction. Meanwhile, the information security and privacy cannot be guaranteed, as shown in **Figure 2A**.

Figure 2B shows the distributed optimization based on the energy system decoupled. Each computing unit needs to process the data of the whole system, which is the mainstream distributed computing method at present. Although the amount of cloud workload is reduced by two to three times, it is still affected by the wide geographical range of the MRIES. Meanwhile, the cost of the communication facility construction is still relatively high. In addition, this method deconstructs the EH model, resulting in the separate operation of each coupling device. As the number and types of the coupling devices increase, the computational complexity of this method will increase and the cost of data transmission and storage will also increase significantly.

The decoupled method based on the ECU is shown in **Figure 2A**, where the data are transmitted within the RIES and only submits the boundary information at the coupling point between the ECUs to the cloud. This decoupled method dramatically reduces the cost of communication facility construction, data transmission, storage, and processing, while ensuring the security and privacy of the data. Furthermore, the ECU collects the data of three types of energy and processes them in a centralized manner, which can better play a synergistic role in optimization. In addition, this method lays a foundation for future research work of the unified energy management.



3 MODELING OF THE EDGE COMPUTING UNIT

3.1 IES Decoupled Principle Based on Edge Computing Unit

As previously mentioned, EH is the main body and the energy management unit of the RIES. Therefore, the EH serves as the main body of the ECU to decouple the energy system. The partition principle should be based on the whole system's lowest communication cost. The communication cost is proportional to the physical distance between the nodes. Therefore, we decouple the energy networks separately according to the adaptive method of P-median problem as shown in Eq. 1.

$$\begin{aligned}
 & \min \sum_{r \in \mathbf{R}} \sum_{f \in \mathbf{F}} l_{rf} y_{rf} \\
 & \text{s.t. } \sum_{r \in \mathbf{R}} y_{rf} = 1, \quad \forall f \in \mathbf{F} \\
 & \quad y_{rf} \in \{0, 1\}, \quad \forall r \in \mathbf{R}, \forall f \in \mathbf{F}.
 \end{aligned} \tag{1}$$

The objective function minimizes the information transmission distance within the network partitions, while the constraints ensure that the nodes are completely partitioned without repetition and omission. The IES model contains an electrical network, natural gas network, and DHN in the study. Therefore, the objective function should be applied in the three networks. After that, we can get the indices of the nodes in each unit of every network, but we need to further determine the boundaries between the units to provide the boundary data for cloud computing. As a result, section 3.2 provides a decoupled method to distinguish the boundaries between the units under different EH connection conditions.

3.2 IES Decoupled Method Based on the Edge Computing Unit

As previously mentioned, the units contain different nodes but are connected by an energy transmission line. The transmission line also falls within the scope of unit internal optimization, so the virtual node needs to be inserted into the transmission line to establish clear boundaries between the units and serve as a data collection point of the connecting transmission line.

This study proposed a decoupled method, where the EH serves as the core in each ECU. Based on the connected position of the EH to the energy network, the whole system is decoupled by the partition method as given below. In Figure 3, the source represents the source of the energy network, which is the generator in the electrical network and the compressor in the natural gas network. EH represents a real hub. The virtual node is located in the middle of the transmission line, and the node data are the energy data in the middle of the transmission line. The virtual transmission line is lossless, aiming to reduce the coupling degree between the nodes.

3.2.1 Tandem Type

This type refers to the nodes of the EHs that are series nodes in the network. It contains three subtypes, such as the head subtype, concatenation subtype, and end subtype.

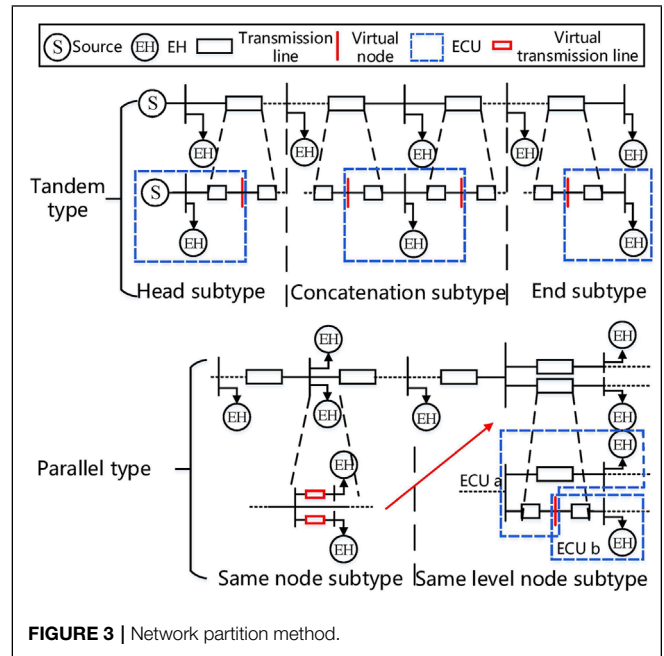


FIGURE 3 | Network partition method.

The concatenation subtype refers to the condition where the node of the EH is neither the end nor the head in the network. In this condition, the energy transmission line should be split in the middle and inserted with a virtual node on each side of the EH. The virtual node is included by the ECUs on both sides, and the insertion position of the virtual node is the boundary between the units. The data of the virtual node during the local optimization within the ECU are the boundary information submitted to the cloud.

The head/end subtype refers to the condition where the node of the EH is the head/end in the network. In this case, a virtual node should be inserted into the middle of the transmission line on only one side.

3.2.2 Parallel Type

This type contains two subtypes: same node subtype and same level node subtype, which, respectively, mean the EHs connected to the same nodes and the same level nodes in the network, as shown in Figure 3. When dealing with the same level node, a virtual node is inserted in the middle of one transmission line to transform it to the end subtype. As for the same node subtype, these node data for the EHs couple tightly, so a section of virtual transmission line should be added before each EH, which is transformed into the same level node subtype.

The energy networks are decoupled based on the abovementioned methods. The total energy consumption of a single ECU is the amount of the difference between the inflow and outflow.

3.3 Electrical Network Model in the Edge Computing Unit

In this study, the Distflow model is used to simulate the power flow of the distribution network in the ECU (Baran and

Wu 1989), and the SOCP is used to deal with the nonlinear model. The power balance of the node described in Eqs 2–4 is the voltage loss equation, and Eq. 5 represents the relationship between the branch current, node voltage, and power.

$$P_{j,t}^{\text{in}} = - \sum_{g \in \Pi} (j) P_{g,t}^{\text{G}} - \sum_{pv \in \Pi} (j) P_{pv,t}^{\text{PV}} - \sum_{wt \in \Pi} (j) P_{wt,t}^{\text{WT}} - (P_{ij,t} - \hat{I}_{ij,t} R_{ij}) + \sum_{o \in \Omega} (j) P_{jo,t} + \sum_{d \in \Pi} (j) P_{d,t}^{\text{LD}} + P_{j,t}^{\text{EH}} \quad (2)$$

$$Q_{j,t}^{\text{in}} = -(Q_{ij,t} - \hat{I}_{ij,t} X_{ij}) + \sum_{o \in \Omega} (j) Q_{jo,t} + \sum_{d \in \Pi} (j) Q_{d,t}^{\text{LD}} \quad (3)$$

$$\hat{V}_{j,t} = \hat{V}_{i,t} - 2(P_{ij,t} R_{ij} + Q_{ij,t} X_{ij}) + \hat{I}_{ij,t} (R_{ij}^2 + X_{ij}^2) \quad (4)$$

$$(2P_{ij,t})^2 + (2Q_{ij,t})^2 + (\hat{I}_{ij,t} - \hat{V}_{i,t})^2 \leq (\hat{I}_{ij,t} + \hat{V}_{i,t})^2 \quad (5)$$

The capacity limitation of the transmission line is shown as Eq. 6.

$$\begin{cases} \hat{I}_{ij,t}^{\min} \leq \hat{I}_{ij,t} \leq \hat{I}_{ij,t}^{\max} \\ \hat{V}_i^{\min} \leq \hat{V}_{i,t} \leq \hat{V}_i^{\max} \end{cases} \quad (6)$$

Power consumption of the ECU is shown as Eq. 7.

$$P_{n,t}^{\text{ECU}} = \sum_{i \in I_n^{\text{upper}}} P_{i,t}^{\text{in}} - \sum_{j \in I_n^{\text{under}}} P_{j,t}^{\text{in}} \quad (7)$$

3.4 Natural Gas Network Model in the Edge Computing Unit

The natural gas network model in the ECU is similar to the electrical network, including the node energy balance constraint and pipeline transport constraint. Eq. 8 represents the balance between the inflow and outflow of node b .

$$G_{b,t}^{\text{in}} = -G_{ab,t} + \sum_{\omega \in \Lambda} (b) G_{\omega,t} + \sum_{d \in Y} (b) G_{d,t}^{\text{LD}} + G_{b,t}^{\text{EH}} \quad (8)$$

The natural gas network in this article is a medium–low pressure network without considering the compressor model (Hu et al., 2020). The second-order cone programming is used to relax the Weymouth equation of the natural gas network, as shown in Eq. 9 (Liu et al., 2020). Eqs 10,11 are the upper and lower limits of the gas transmission volume and natural gas pressure of the pipeline, respectively.

$$(G_{ab,t})^2 + (K_{ab} \pi_{b,t})^2 \leq (K_{ab} \pi_{a,t})^2 \quad (9)$$

$$0 \leq G_{ab,t} \leq G_{ab}^{\max} \quad (10)$$

$$\pi_a^{\min} \leq \pi_{a,t} \leq \pi_a^{\max} \quad (11)$$

The natural gas consumption of the ECU is shown as Eq. 12.

$$G_{n,t}^{\text{ECU}} = \sum_{a \in A_n^{\text{upper}}} G_{a,t}^{\text{in}} - \sum_{b \in B_n^{\text{under}}} G_{b,t}^{\text{in}} \quad (12)$$

3.5 DHN Model in the Edge Computing Unit

This study uses the available heating H^{av} to describe the thermal flow in a pipe. Two strong-coupled variables, temperature T and mass flow q in the DHN model are decoupled to form the thermal flow network model and the basic flow-temperature equation.

The linearized heat loss equation shows as Eq. 14, and Wei et al., (2017) prove that it has good accuracy when the initial temperature is 88 ~92°C. Section 4.2 will introduce the improved distributed algorithm based on linear heat loss.

$$H^{\text{av}} = \mu q (T - T^{\text{rw}}) \quad (13)$$

$$\Delta H_{uv}^{\text{av}} = 2\pi i \frac{T^{\text{sw}} - T^{\text{c}}}{\sum R} l_{uv} \quad (14)$$

The setup of the reference direction of heating medium flow in the DHN is shown in Figure 4. The EH_n represented the n th EH. The thermal flow network model is shown as Eq. 15.

$$\begin{cases} H_{n,u,t}^{\text{EH}} + \sum_{m \in \Psi(u)} H_{um,t}^{\text{av}} = 0 \\ H_{um,t}^{\text{av}} = -(H_{mu,t}^{\text{av}} - \Delta H_{mu}^{\text{av}}), \text{ if } H_{mu,t}^{\text{av}} > 0 \\ H_{um,t}^{\text{av},\min} \leq H_{um,t}^{\text{av}} \leq H_{um,t}^{\text{av},\max}, \text{ if } H_{um,t}^{\text{av}} > 0 \end{cases} \quad (15)$$

A mixed-integer model of the thermal flow network is established based on the abovementioned equation to obtain the available heating distribution. Combined with the basic flow-temperature equation below, we can calculate the transmission temperature and thermal flow in the pipe.

$$\begin{cases} H_{u,t}^{\text{EH}} = kq_{u,t}^{\text{EH}} (T_{u,t}^{\text{EH}} - T^{\text{rw}}) \\ H_{uv,t}^{\text{av}} = kq_{uv,t}^{\text{av}} (T_{uv,t}^{\text{av}} - T^{\text{rw}}) \\ T_{u,t}^{\text{EH}} = T_{u,t}^{\text{av}}, \text{ if } H_{u,t}^{\text{EH}} > 0 \\ T_{u,t}^{\text{EH}} = T^{\text{sw}}, \text{ if } H_{u,t}^{\text{EH}} < 0 \\ T_{uv,t}^{\text{av}} = T_{u,t}^{\text{av}}, \text{ if } H_{uv,t}^{\text{av}} > 0 \\ q_{u,t}^{\text{EH}} + \sum_{m \in \Psi(u)} q_{um,t} = 0 \\ q_{uv,t} + q_{vu,t} = 0 \end{cases} \quad (16)$$

The DHN operation cost is caused by the operation cost of circulating water pumps in the network. Therefore, the EHR is introduced to describe the cost of the circulating water pumps. Eq. 17 represents the heat network operation cost of the n th ECU.

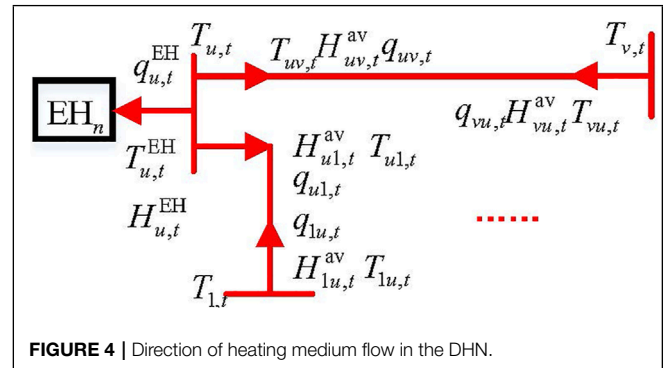


FIGURE 4 | Direction of heating medium flow in the DHN.

Each pipe is configured with a circulating water pump in this study.

$$C_n^{\text{heat}} = \sum_t \sum_{p=1}^W \left(\text{EHR}_p c_{e,t} |H_{p,t}| \right). \quad (17)$$

3.6 EH Model Considering Off-Design Performance

The EH is the energy conversion main body of the ECU. In this article, the standard matrix model is adopted for the EH model (Wang et al., 2017), and the piecewise linearization method is used to improve the accuracy of the EH model (Huang et al., 2019).

The energy flow direction of the coupling equipment is shown in **Figure 5**. **Eqs 18–20** describe the standard model of the EH. The heating output from the EH and the heating obtained from the DHN jointly support the heat load in this region.

$$V = \left[P_{\text{in}}^{\text{Grid}} \ P_{\text{in}}^{\text{EC}} \ P_{\text{in}}^{\text{HP}} \ P_{\text{in}}^{\text{CHP}} \ P_{\text{in}}^{\text{GB}} \ P_{\text{out}}^{\text{EC}} \ P_{\text{out}}^{\text{HP}} \ P_{\text{out,e}}^{\text{CHP}} \ P_{\text{out,h}}^{\text{CHP}} \ P_{\text{out}}^{\text{GB}} \ P_{\text{in}}^{\text{HS}} \ P_{\text{out}}^{\text{HS}} \right]^T. \quad (18)$$

$$V1 = \left[P^{\text{EH}} \ G^{\text{EH}} \ L_{\text{cool}} \ L_{\text{elec}} \ (L_{\text{heat}} - H^{\text{EH}}) \ 0 \ 0 \right]^T \quad (19)$$

$$Z \times V = V1. \quad (20)$$

To simplify the nonlinearity of the coupling equipment efficiency, this study uses the piecewise linearization method as shown in **Eqs 21–23** dealing with the nonlinear efficiency function of the coupling devices instead of the constant efficiency.

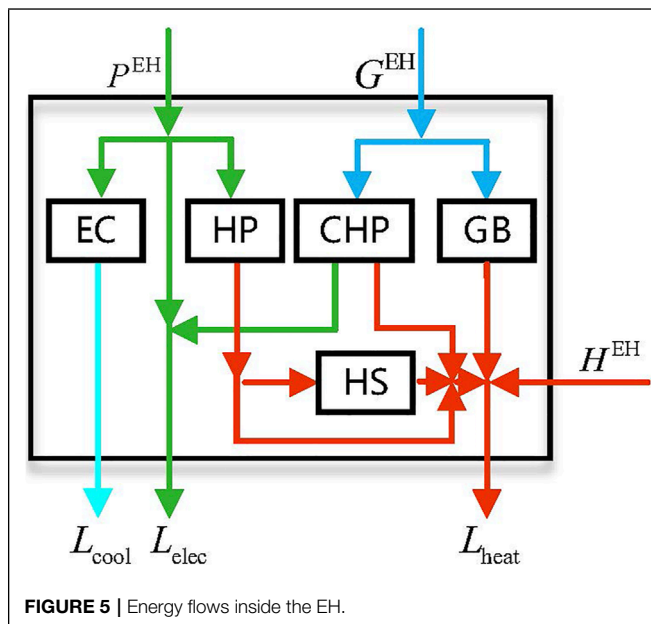


FIGURE 5 | Energy flows inside the EH.

$$X = X_0 + \sum_{y \in \Gamma} \sigma_y. \quad (21)$$

$$F_L(X) = F(X_0) + \sum_{y \in \Gamma} \eta_y \sigma_y. \quad (22)$$

$$I_{y+1}(\overline{Xy} - \underline{Xy}) \leq \sigma_y \leq I_y(\overline{Xy} - \underline{Xy}). \quad (23)$$

3.7 Objective Function of the Edge Computing Unit

The model of the ECU has been completed. The internal power grid and the natural gas network build up the SOCP, while the DHN and EH build up the MILP problem. This study takes the minimum economic cost as the optimization objective, and the objective function and the constraints of each ECU are shown in **Eq 24**.

$$\min \sum_t \left[(c_{e,t} P_{n,t}^{\text{ECU}} + c_{g,t} G_{n,t}^{\text{ECU}}) + \sum_{p=1}^W (\text{EHR}_p c_{e,t} |H_{p,t}|) \right]. \quad (24)$$

s.t. (2) – (16), (18) – (23)

4 NESTED ALGORITHM BASED ON C-ADMM

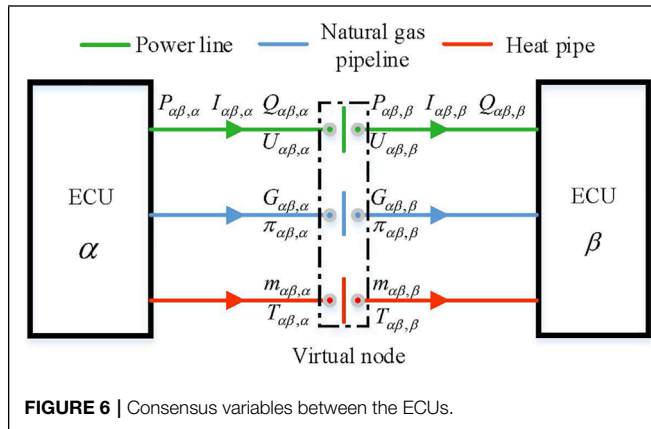
The ADMM algorithm performs well in the distributed optimization and has many improved forms. The multiregion expansion form of the standard ADMM, which guarantees convergence, is complex and does not conform to the calculation form of the ECU proposed in this article (Wang et al., 2013). The GS-ADMM cannot guarantee the convergence of multiregion expansion when $n \geq 3$, which is in the form of a serial computation (Ma et al., 2016). The C-ADMM supports the multizone expansion and is a parallel computing form, so it is used as the improved basis of the distributed algorithm in this study.

It is the key to coordinate the consensus information for the C-ADMM. The ECUs connect with each other through the power line, natural gas pipeline, and heat pipe as shown in **Figure 6**. The coupled information includes P, Q, I, U of the power line, G, π of the natural gas pipeline, and H of the heat pipe, which has an equality relationship with the consensus parameters at the virtual node as shown in **Eq. 25**.

$$x_{\alpha\beta,\alpha,t} = z_{\alpha\beta,t} = x_{\alpha\beta,\beta,t} \quad (25)$$

According to **Eq. 24**, the Lagrange expansion of the C-ADMM is shown in **Eq. 26**. **Eq. 27** is used to update the consensus variables and penalty factor.

$$L_n = \sum_{t=1}^T \left\{ (c_{e,t} P_{n,t}^{\text{ECU}} + c_{g,t} G_{n,t}^{\text{ECU}}) + \sum_{p=1}^W (\text{EHR}_p c_{e,t} |H_{p,t}|) + \sum_{\alpha \in \Theta_n} \left[\lambda_{\alpha\beta,\alpha,t} (x_{\alpha\beta,\alpha,t} - z_{\alpha\beta,t}) + \frac{\rho}{2} \|x_{\alpha\beta,\alpha,t} - z_{\alpha\beta,t}\|_2^2 \right] \right\}. \quad (26)$$



$$\begin{cases} z_{\alpha\beta,t}^{k+1} = \frac{1}{2} \left[x_{\alpha\beta,\alpha,t}^{k+1} + x_{\alpha\beta,\beta,t}^{k+1} + \frac{1}{\rho} (\lambda_{\alpha\beta,\alpha,t}^k + \lambda_{\alpha\beta,\beta,t}^k) \right] \\ \lambda_{\alpha\beta,\alpha,t}^{k+1} = \lambda_{\alpha\beta,\alpha,t}^k + \rho (x_{\alpha\beta,\alpha,t}^{k+1} - z_{\alpha\beta,t}^{k+1}) \end{cases} \quad (27)$$

In order to ensure the convergence of the optimization problems with discrete variables, previous work improved the C-ADMM algorithm, such as solving the MISOCP

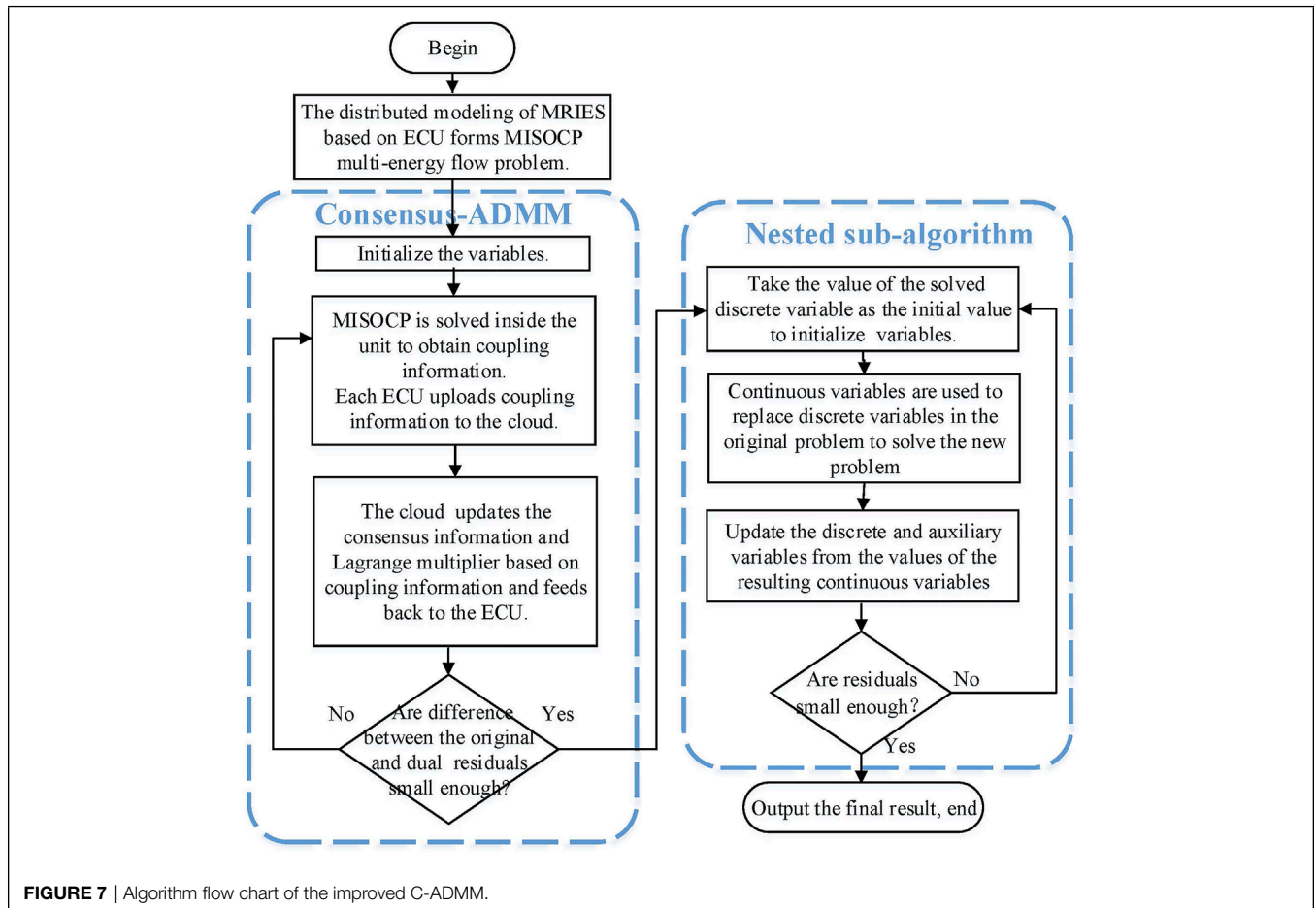
nonconvergence caused by the ring natural gas network through the nested computation of the discrete variables relaxation (Wen et al., 2017). The nonconvergence problem was solved by embedding the NC-ADMM method into the subproblem (Chen et al., 2020).

In order to ensure the convergence of the MISOCP constituent, a nested subalgorithm was added to the C-ADNN algorithm in this article, as shown in Eq. 28. The additional increment term describes that all the ECUs support transmission loss of the DHN which can constrain the direction of each iteration and improve the convergence speed, while the loss linearization of the heat network is the premise of this improvement. The algorithm flow chart is shown in Figure 7.

$$L_n = (25) + \lambda_{\text{loss}}^H \left(\sum_{n=1}^N H_{n,t}^{\text{EH}} - \sum_{p=1}^W \Delta H_p^{\text{av}} \right) + \frac{\rho}{2} \left\| \sum_{n=1}^N H_{n,t}^{\text{EH}} - \sum_{p=1}^W \Delta H_p^{\text{av}} \right\|_2^2 \quad (28)$$

The nested subalgorithm is introduced as given below.

Step 1. Initializing the discrete variables B , k , and θ . Setting the error tolerance δ .



Step 2. Combining Eqs 2–16 and Eqs 18–23 to solve Eq. 29 and then obtaining the value of C_B , before which the unknown variable C_B takes place of the discrete variable B .

$$C_{B,s}^{k+1} = \arg \min_{C_{B \leftarrow B}} \left[(27) + \sum_{s=1}^S \frac{\theta}{2} \|B_s^k - C_{B,s}^k + z_{B,s}^k\|_2^2 \right]. \quad (29)$$

Step 3. Updating the discrete variables B and auxiliary variables z_B as shown in Eq. (30).

$$\begin{cases} B_s^{k+1} = \arg \min_B \sum_{s=1}^S \|B_s^k - C_{B,s}^k + z_{B,s}^k\|_2^2 \\ z_{B,s}^{k+1} = z_{B,s}^k + (B_s^k - C_{B,s}^k) \end{cases} \quad (30)$$

Step 4. Comparing the error obtained by Eq. 29 with δ . If the error is little enough, the iterative process will be broken, and if on the contrary, steps two to four will be repeated.

The addition of the nested subalgorithm makes the solution approach the feasible region infinitely. When the difference between the original and the dual errors of the original problem is small enough, the convergence process can be sped up significantly.

5 CASE STUDY

5.1 System Description

According to the partition method, the insertion of virtual nodes into the energy networks and partitioning them is based on the principle stated in section 3.1. The ECUs can completely contain all the nodes without repeat, as shown in Figure 8A. The partition details are shown in Figure 8B.

This article uses the improved C-ADMM algorithm to complete the distributed optimization of the MRIES in two scenarios.

Scenario A: Optimizing the MRIES containing electrical, gas, and heating networks based on the ECUs.

Scenario B: Optimizing the MRIES containing the electrical and natural gas networks based on the ECUs.

In both the scenarios, the MRIES have the same loads. Nevertheless, in Scenario B, the coupling equipment produces the heating to meet the heating demands.

Conversion efficiency functions of the coupling devices are shown in Table 1. The types of coupling devices in the MRIES are shown in Table 2. The energy prices and loads of each EH are shown in Figure 9.

The codes were written in MATLAB 9.4.0.813654 (R2018a), and all the experiments were conducted on a desktop with 3.00 GHz Intel Core i5 and 16.0 GB RAM.

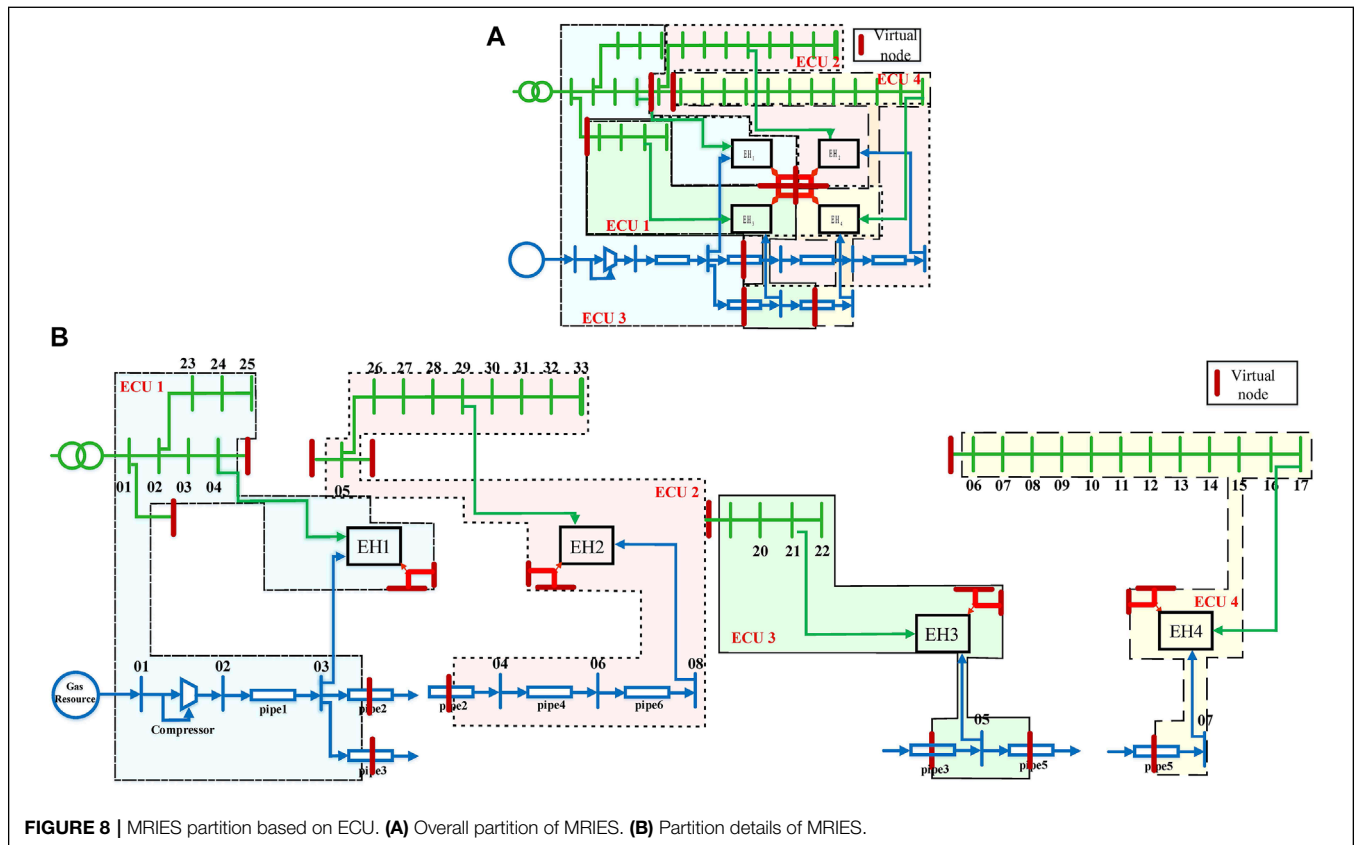


FIGURE 8 | MRIES partition based on ECU. (A) Overall partition of MRIES. (B) Partition details of MRIES.

TABLE 1 | Parameters of the energy coupling equipment.

Coupling Device	Capacity (kW)	Efficiency Function
EC	400	Out = $-0.00003041 \cdot \ln 3 + 0.01901 \cdot \ln 2 + 0.2593 \cdot \ln$
HP	400	Out = $3 \cdot \ln$
CHP	e:300	Out = $0.0001150 \cdot \ln 2 + 0.2305 \cdot \ln$
	h:420	Out = $0.0001611 \cdot \ln 2 + 0.3228 \cdot \ln$
GB	900	Out = $0.8 \cdot \ln$
HS	800	h = $-0.00005 \cdot \ln + 0.93$
	(3.2 MWh)	g = $-0.00005 \cdot \text{Out} + 0.93$

TABLE 2 | Region type and the configuration of EHS.

Region Types		Equipment				
		EC	HP	CHP	GB	HS
EH1	Residential area	✓	✓	✓		
EH2	Office area	✓	✓	✓	✓	
EH3	Business area	✓	✓	✓		✓
EH4	Industrial area	✓	✓	✓		✓

5.2 Analysis of Optimization Results

The improved algorithm proposed is used to optimize this MRIES in this article. The energy inputs to the equipment of the four ECUs in the different scenarios are shown in Figure 10.

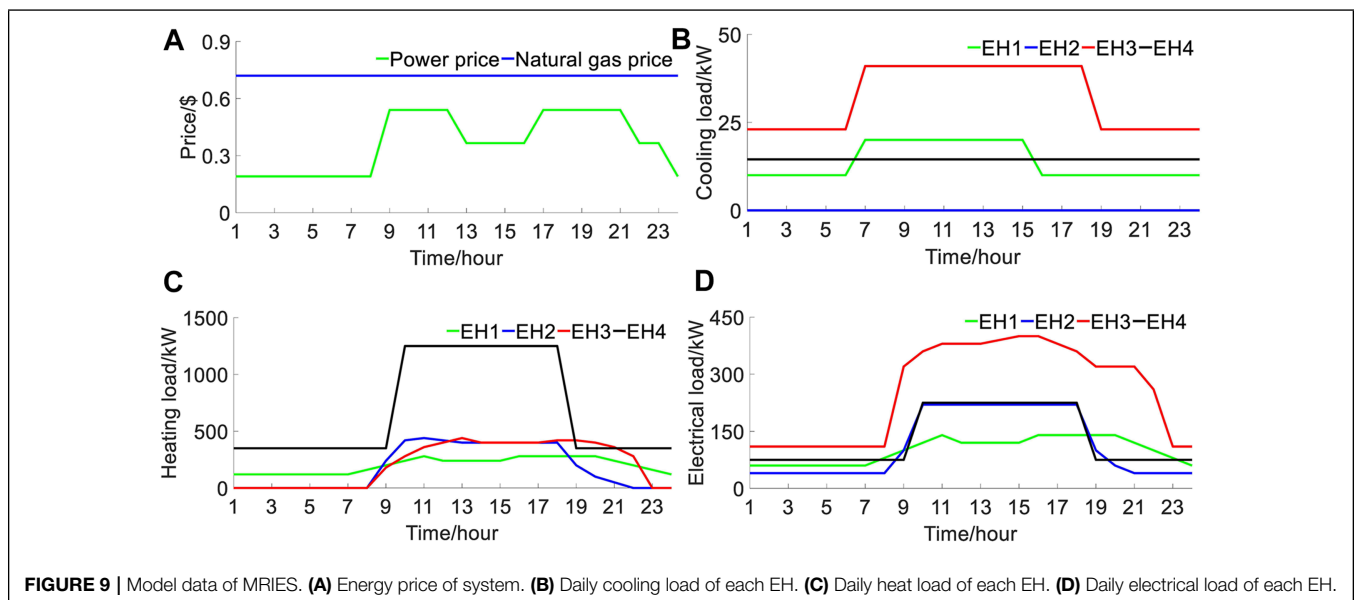
As shown in Figure 10A, to support the heating load concentrated in midday, the HP is constantly working during low loading time of energy consumption when the power is cheaper. The heating is stored in the HS at night, which releases when the electricity price is high. In addition to this, the GB supports the

remaining heating demand. Since there is no GB in EH3, it can only generate heat through the CHP. Furthermore, EH3 has the largest electric load at midday. As a result, the CHP runs at full capacity at all the time. In addition, the CHPs in EH2 and EH4 also run at full capacity at midday when the electric and heating load is large. On the other hand, the electric and heating load is relatively small in EH1. Therefore, the CHP is mainly used for power and heating supply in the peak load period, and the HP will start up for heat supplement during the flat power demand period.

As shown in Figure 10B, EH4 uses HP and GB with a high cost to supply heat due to the lack of DHN for heat exchange in scenario B. EH3 no longer needs to provide the heating to the DHN, which produced significant heating in scenario A. As a result, the utilization rate of HP and HS becomes lower. The overall energy cost response of the MRIES weakened in scenario B.

The heating generated by the EH, which is beyond the local heating load, is transmitted to the DHN. As shown in Figure 11, the energy represented by the blue block is equal to the energy of other color blocks higher than the heat load line (except the purple block that indicates heating storage). It should be noted that for the intuitive description, the load curves in Figure 11 are superimposed of electricity, gas, and heating load curves.

Because the coupling of the ECU in the electric network and natural gas network is only reflected in energy transmission, the energy interaction of each ECU in the DHN is mainly analyzed. The energy outputs of each EH device and the energy interaction with the DHN are integrated into Figures 11A–D. Evidently, the DHN realizes the heating interaction between the ECUs and dramatically increases the flexibility of energy utilization of the system. In scenario A, the EH1 internal equipment composition is relatively simple, which mainly



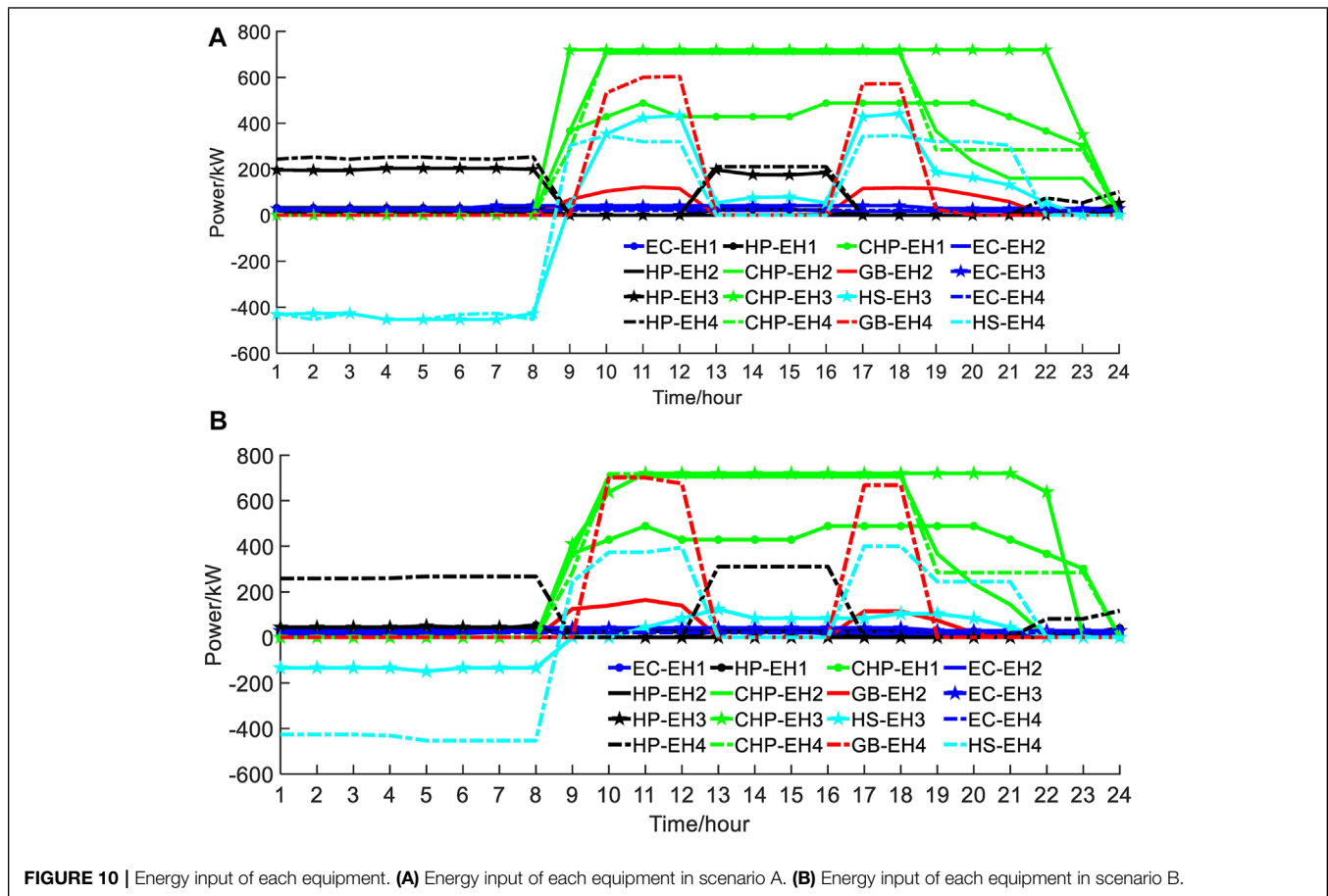


FIGURE 10 | Energy input of each equipment. **(A)** Energy input of each equipment in scenario A. **(B)** Energy input of each equipment in scenario B.

absorbs the heat from the DHN. Although EH4 has many types of internal heat generation equipment, it still mainly absorbs the heat from the DHN due to its large heating load.

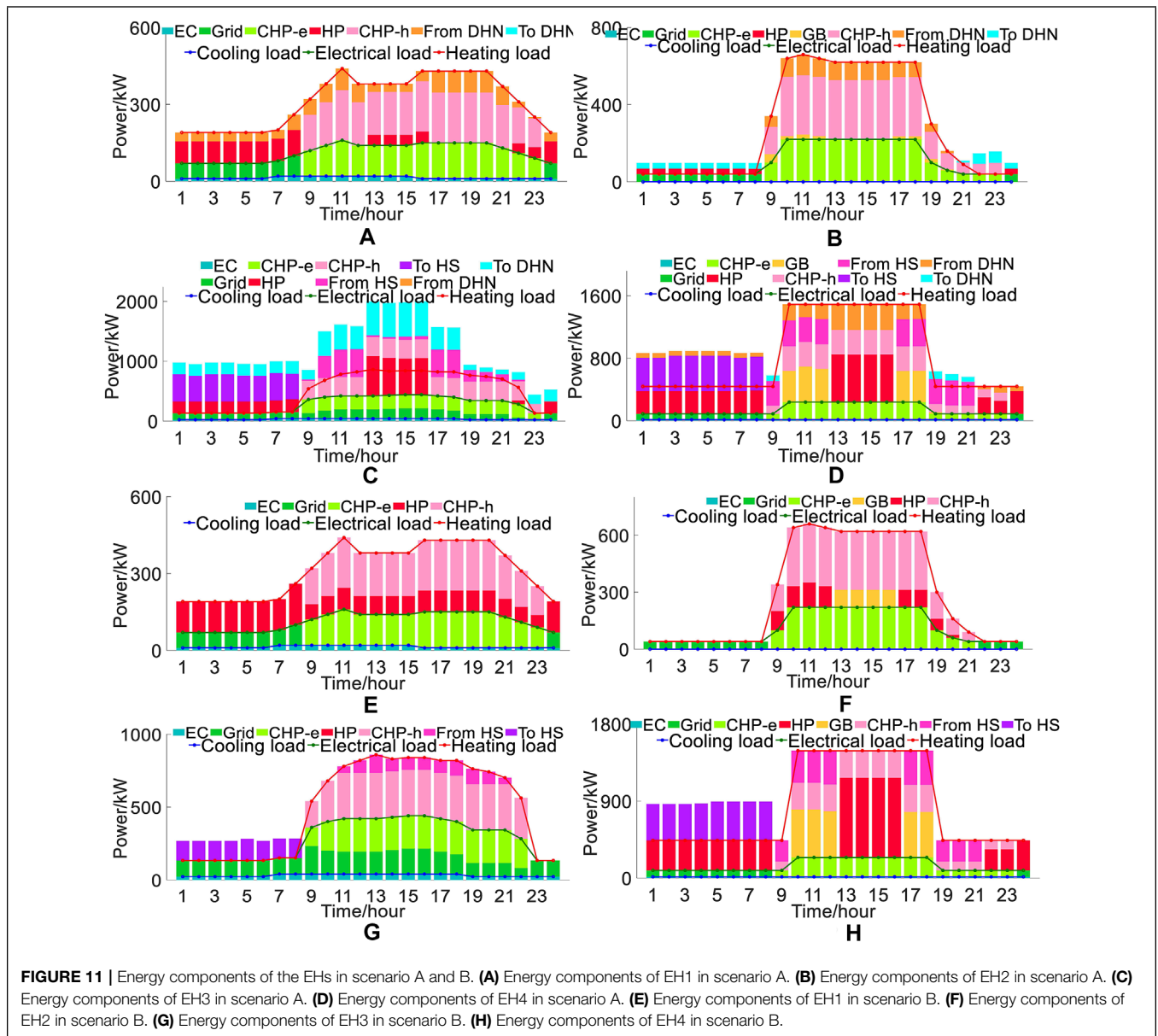
From **Figure 11E–H**, we can see that the heating support of EH3 is significantly reduced in scenario B. EH1, EH2, and EH4 have to convert energy through the coupling equipment in their units to meet the local loads, confirming the previous analysis conclusion. The total energy cost of scenario A is 12,281.24 dollars while that of scenario B is 15,234.56 dollars. For now, we can get the importance of the multi-energy cooperative scheduling.

5.3 Comparison of Algorithm Performance

The accuracy and convergence performance of the algorithm proposed are improved in this article. As analyzed previously, the improved algorithm can realize the MRIES global optimization through the unit internal optimization and information interaction between the units. The distributed optimization is not based on the whole system data; it can only approach the result of the centralized algorithm infinitely but cannot be better than that, and the insufficient iteration of the MISOCP will aggravate this error. The centralized algorithm which optimizes based on

the whole system data can provide a precision reference for the improved distributed algorithm. The improved C-ADMM algorithm in this article adds the nested subalgorithm, which can not only overcome the nonconvergence problem caused by the MISOCP but can also approach the feasible region more closely than the C-ADMM algorithm, making the results more accurate. The results of the centralized algorithm, C-ADMM algorithm, and improved C-ADMM algorithm are shown as **Table 3**. The total energy cost error of the improved C-ADMM algorithm is about 0.1%. In contrast, the error of the C-ADMM algorithm is about 1.3%. In addition, the electricity and gas cost error are also relatively less. This shows that the improved algorithm proposed in this article achieves better optimization results than the original C-ADMM.

By comparing the convergence performance of the improved algorithm proposed in this article with that of the C-ADMM, the improved algorithm meets the accuracy requirement after 40 iterations. In comparison, the original algorithm needs 90 iterations under the same parameters as shown in **Figure 12**. In this article, the unit internal optimization and the information interaction between the units with the cloud are integrated and simulated on a computer. According to the simulation statistics, the C-ADMM algorithm takes 79.71 s, while the improved



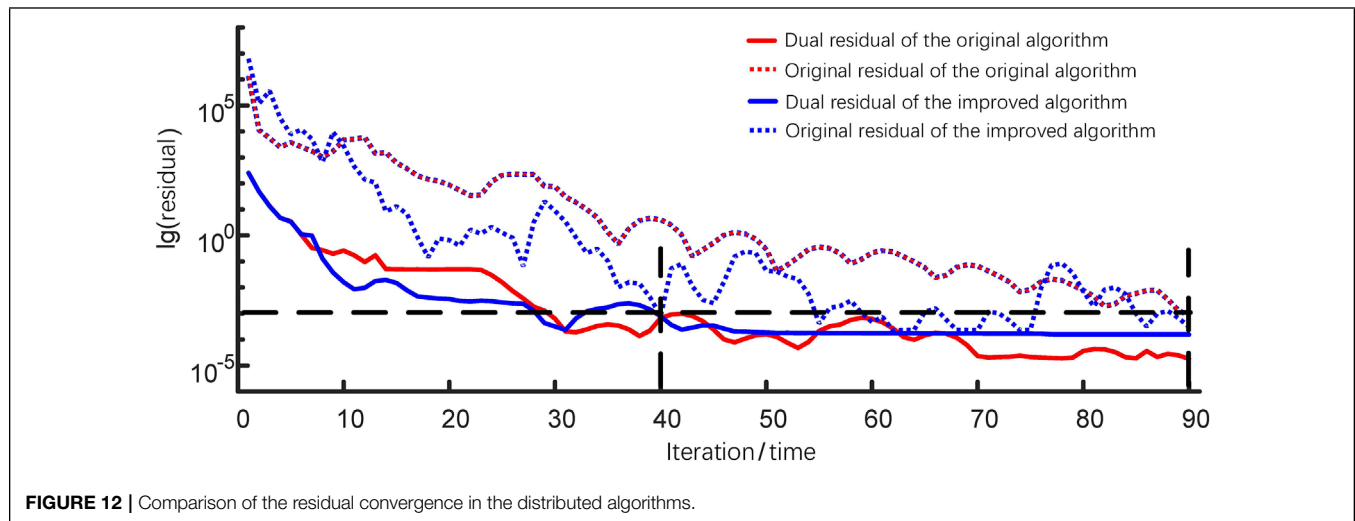
C-ADMM algorithm takes 40.76 s. Therefore, the convergence performance of the improved algorithm is better than that of the original algorithm.

The rationality of the distributed optimization with the ECU as a subsystem was verified by the improved algorithm.

At the same time, the improved algorithm is proven to be superior to the original algorithm. The ECU provides a standard unit form for the improved consensus-ADMM algorithm, and their strengths are closely combined to achieve good optimization results.

TABLE 3 | Comparison of the algorithm error.

Algorithm	Total cost		Power cost		Natural gas cost	
	data/\$	error	data/\$	error	data/\$	error
Centralized optimization	12,281.24	0	5,950.02	0	6,343.91	0
C-ADMM	12,436.12	1.3%	5,694.48	4.3%	6,741.64	6.3%
Improved C-ADMM	12,293.95	0.1%	5,715.71	3.9%	6,578.99	3.7%



6 CONCLUSION AND PROSPECTS

From the perspective of the data interaction architecture, this study compares the differences, advantages, and disadvantages of the centralized optimization and distributed optimization, where the IES is decoupled according to the energy networks and the distributed optimization based on the proposed ECU framework. In addition, a unified network partition method is proposed, and the ECU model is introduced in detail.

This study improved the C-ADMM method to adapt to the ECU model. A study case verifies the improved convergence performance of the improved algorithm, and the algorithm was proven to assist the ECU model in completing the distributed optimization of the MRIES well.

In conclusion, the ECU model proposed in this article can fully play the advantages of energy utilization and data management of the RIES and serve as a distributed unit connected to the upper energy network and the lower load layer. Moreover, it breaks through the limitation that the IES distributed optimization with EH as the main body failed to consider the constraints of networks. In addition, the ECU framework can be used as the unit of the MRIES for further research, such as model predictive control and study for the uncertainty involved by wind power and photovoltaic. In addition, the future work will consider carbon emission in

the optimization objective for the carbon peak and carbon neutrality targets.

DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

AUTHOR CONTRIBUTIONS

MW: conceptualization, methodology, software, validation, formal analysis, investigation, writing—original draft, visualization, and resources. HZ: methodology, software, validation, writing—review and editing, supervision, project administration, and funding acquisition. HT: methodology, writing—review and editing, and project administration. QW: methodology, validation, writing—review and editing, and project administration.

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NOMENCLATURE

Abbreviations

- ADMM** Alternating direction multiplier method
C-ADMM Consensus-alternating direction multiplier method
CHP Combined heat and power
DHN District Heating Network
ECU Edge computing unit
EC Electrical chiller
EHR Electricity consumption to transferred heating quantity ratio
EH Energy hub
GB Gas boiler
GS-ADMM Gauss–Seidel alternating direction multiplier method
HP Heat pump
HS Heat storage
IES Integrated energy system
MILP Mixed-integer linear programming
MISOCP Mixed-integer second-order cone programming
MRIES Multiregion integrated energy system
NC-ADMM Nonconvex alternating direction multiplier method
RIES Regional integrated energy system
SOCP Second-order cone programming

Indices

- a, b, ω** Index of natural gas network nodes
 d Index of loads in energy networks
 g, pv, wt Indices of electrical generating units, photovoltaic power plants, and wind turbines
 i, j, o Index of electrical network nodes
 k Index of iteration numbers
 p Index of heating network pipelines
 r, f Indices of unpartitioned nodes and EH nodes in energy networks
 s Index of binary variables
 t Index of time intervals
 u, v, m Index of heating network nodes

Parameters

- μ** Proportionality constant
 ρ Penalty factor in the C-ADMM algorithm
 ΣR Total thermal resistance between the heat medium and surrounding medium per kilometer of pipe
 θ Penalty factor in the subalgorithm
 $c_{e,t}, c_{g,t}$ Electricity price and natural gas price at t
 K_{ab} Weymouth characteristic parameter of the pipeline ab
 l_{uv} Length of the pipe uv

- N** Number of EHs
 πi Circular constant
 S Number of binary variables
 W Number of pipes in the DHN

Sets

- $\gamma \in \Gamma$** Set of segments in piecewise linearization
 $\Lambda(b), Y(b)$ Set of loads and downstream nodes connected to node j in the natural gas network
 $\Phi(u)$ Set of downstream nodes connected to node u in the DHN
 $\Pi(j), \Omega(j)$ Set of devices and downstream nodes connected to node j in the power system
 Θ_n Set of energy transmission lines between the n th ECU with others
 $A_n^{\text{upper}}, B_n^{\text{under}}$ Set of upstream and downstream virtual nodes of the ECU n in the natural gas network
 $I_n^{\text{upper}}, J_n^{\text{under}}$ Set of upstream and downstream virtual nodes of the ECU n in the power system

Variables

- ΔH_p^{av}** Available heating loss of the p th pipe
 $\Delta H_{uv}^{av}, \Delta H_{mu}^{av}$ Available heating loss of pipe uv and pipe mu
 $\hat{I}_{ij,t}$ Square value of branch ij current at t
 $\hat{I}_{ij}^{\text{max}}, \hat{I}_{ij}^{\text{min}}$ Lower/upper bounds of square value of branch ij current
 $\hat{V}_{(\cdot),t}$ Square value of the node voltage at t
 $\hat{V}_i^{\text{max}}, \hat{V}_i^{\text{min}}$ Lower/upper bounds of square value of node i voltage
 $\mathbb{I}_\gamma, \mathbb{I}_{\gamma+1}$ Binary variables to guarantee the continuity of X and $F_L(X)$
 \bar{X}_γ, X_γ Lower/upper bounds of the γ -th segment of X
 $\pi_{(\cdot),t}$ Gas pressure of node at t
 $\pi_a^{\text{min}}, \pi_a^{\text{max}}$ Lower/upper bounds of gas pressure of node a
 $\sigma_\gamma, \eta_\gamma$ Value of the γ -th segment of X and coefficient of the γ -th segment of $F_L(X)$
 EHR_p The EHR of the water pump p
 $C_B, Z_{B,B}$ Continuous variable, auxiliary variable, and binary variable, $C_B \in [0, 1]$
 C_n^{heat} Cost of the DHN connected to EH n
 $F(X), F_L(X)$ Nonlinear function and its linearized function
 $G_{(\cdot),t}$ Natural gas in pipeline at t
 $G_{(\cdot),t}^{\text{in}}$ Natural gas injected into the node at t
 G_{ab}^{max} Upper bounds of natural gas in the pipeline ab
 $G_{b,t}^{\text{EH}}$ Natural gas injected to the EH connected to node b at t
 $G_{d,t}^{\text{LD}}$ Natural gas injected to load d at t
 $G_{n,t}^{\text{ECU}}$ Natural gas consumption of the ECU n at t
 H^{EH} Heating input of EH from the DHN
 H^{av} Available heating

$H_{p,t}$	Heating transferred in pipe p	q	Mass flow
$H_{u,t}^{EH}$	Heating injected into the EH connected to the node u at t	$q_{u,t}^{EH}$	Mass flow injected into the EH of node u at t
$H_{um,t}^{av,min}, H_{um,t}^{av,max}$	Lower/upper bounds of available heating from node u to node m	$q_{uv,t}, q_{vu,t}$	Mass flow from node u to node v and node v to node u at t
$H_{um,t}^{av}, H_{mu,t}^{av}$	Available heating from node u to node m and node m to node u at t	R_{ij}, X_{ij}	Resistance and reactance of branch ij
$H_{uv,t}^{av}, H_{vu,t}^{av}$	Available heating from node u to node v and node v to node u at t	T, T^e	Real temperature and ambient temperature
$L_{cool}, L_{elec}, L_{heat}$	Cooling, electricity, and heating loads of the EH	T^{rw}, T^{sw}	Return water temperature and supply water temperature
P^{EH}, G^{EH}	Power and natural gas input of the EH	$T_{(\cdot),t}$	Node temperature at t
$P_{(\cdot),t}, Q_{(\cdot),t}$	Active power and reactive power on branch at t	$T_{u,t}^{EH}$	Temperature of heat medium injected into the EH connected to node u at t
$P_{(\cdot),t}^{in}, Q_{(\cdot),t}^{in}$	Active power and reactive power injected to node at t	$T_{uv,t}, T_{vu,t}$	Temperature of heat medium from node u to node v and node v to node u at t
$P_{in}^{CHP}, P_{out,e}^{CHP}, P_{out,h}^{CHP}$	Input and output energy of the CHP	V	Matrix of coupling equipment's input and output energy
$P_{in}^{EC}, P_{out}^{EC}$	Input and output energy of the EC	VI	Matrix of the EH's input resources and loads
$P_{in}^{GB}, P_{out}^{GB}$	Input and output energy of the GB	X, X_0	Continuous variable and its initial value
P_{in}^{Grid}	Input energy from the grid	$x_{\alpha\beta,\alpha,t}, x_{\alpha\beta,\beta,t}$	Coupling variables on both sides of the virtual node at t
$P_{in}^{HP}, P_{out}^{HP}$	Input and output energy of the HP	y_{rf}	Binary variable of node r partition to region f
$P_{in}^{HS}, P_{out}^{HS}$	Input and output energy of the HS	Z	Standard matrix of the EH
$P_{d,t}^{LD}, Q_{d,t}^{LD}$	Active power and reactive power injected to load d at t	$z_{\alpha\beta,t}$	Consensus variable of the virtual node at t
$P_{g,t}^G$	Active power generated from the generator g at t	$\lambda_{\alpha\beta,\alpha,t}, \lambda_{\alpha\beta,\beta,t}$	Lagrange multipliers of the ECU's on both sides of the virtual node at t
$P_{j,t}^{EH}$	Active power injected to the EH connected to node j at t	λ_{loss}^H	Lagrange multiplier in terms of the transmission loss in the DHN at t
$P_{n,t}^{ECU}$	Power consumption of the ECU n at t	B_s^k, B_s^{k+1}	The s th binary variables in the k th and the $(k+1)$ -th iteration
$P_{pv,t}^{PV}$	Active power generated from photovoltaic power plants pv at t	$C_{B,s}^k, C_{B,s}^{k+1}$	The s th continuous variables in the k th and the $(k+1)$ -th iteration
$P_{wt,t}^{WT}$	Active power generated from wind turbine wt at t	$z_{B,s}^k, z_{B,s}^{k+1}$	The s th auxiliary variables in the k th and the $(k+1)$ -th iteration