



Topology Optimization of Graded Truss Lattices Based on On-the-Fly Homogenization

Telgen, Bastian; Sigmund, Ole; Kochmann, Dennis M.

Published in:
Journal of Applied Mechanics

Link to article, DOI:
[10.1115/1.4054186](https://doi.org/10.1115/1.4054186)

Publication date:
2022

Document Version
Peer reviewed version

[Link back to DTU Orbit](#)

Citation (APA):
Telgen, B., Sigmund, O., & Kochmann, D. M. (2022). Topology Optimization of Graded Truss Lattices Based on On-the-Fly Homogenization. *Journal of Applied Mechanics*, 89(6), Article 061006.
<https://doi.org/10.1115/1.4054186>

General rights

Copyright and moral rights for the publications made accessible in the public portal are retained by the authors and/or other copyright owners and it is a condition of accessing publications that users recognise and abide by the legal requirements associated with these rights.

- Users may download and print one copy of any publication from the public portal for the purpose of private study or research.
- You may not further distribute the material or use it for any profit-making activity or commercial gain
- You may freely distribute the URL identifying the publication in the public portal

If you believe that this document breaches copyright please contact us providing details, and we will remove access to the work immediately and investigate your claim.

Topology optimization of graded truss lattices based on on-the-fly homogenization

Bastian Telgen

Mechanics & Materials Lab
Department of Mechanical and Process Engineering
ETH Zürich
8092 Zürich, Switzerland
Email: telgenb@ethz.ch

Ole Sigmund

TopOpt group
Department of Mechanical Engineering
Technical University of Denmark
2800 Kongens Lyngby, Denmark
Email: sigmund@mek.dtu.dk

Dennis M. Kochmann*

Mechanics & Materials Lab
Department of Mechanical and Process Engineering
ETH Zürich
8092 Zürich, Switzerland
Email: dmk@ethz.ch

ABSTRACT

We introduce a computational framework for the topology optimization of cellular structures with spatially varying architecture, which is applied to functionally graded truss lattices under quasistatic loading. We make use of a first-order homogenization approach, which replaces the discrete truss by an effective continuum description to be treated by finite elements in a macroscale boundary value problem. By defining the local truss architecture through a set of Bravais vectors, we formulate the optimization problem with regards to the spatially varying basis vectors and demonstrate its feasibility and performance through a series of benchmark problems in 2D (though the method is sufficiently general to also apply in 3D, as discussed). Both the displacement field and the topology are continuously varying unknown fields on the macroscale, and a regularization is included for well-posedness. We argue that prior solutions obtained from aligning trusses along the directions of principal stresses are included as a special case. The outlined approach results in heterogeneous truss architectures with a smoothly varying unit cell, enabling easy fabrication with a tunable length

*Corresponding author.

scale (the latter avoiding the ill-posedness stemming from classical nonconvex methods without an intrinsic length scale).

1 INTRODUCTION

Cellular materials achieve excellent mechanical properties at a considerably lower weight than conventional solids. Having been characterized extensively with regards to the wide material property space they span [1, 2], cellular metamaterials enable their functional optimization through a careful choice of the base material(s) and, moreover, the topology and geometry of the cellular design [3]. The latter particularly applies in hierarchical networks, whose overall properties depend on the arrangement of structural members at each level [4]. The rapid development of modern additive manufacturing techniques has enabled the integration of cellular design principles across length scales down to the nanoscale [5, 6], which has opened an unprecedented design space. Cellular solids are also omnipresent in nature (e.g., in bone, wood, shell, or bamboo), whose key distinguishing feature from most man-made metamaterials is their non-periodicity stemming from self-assembly processes. The design of metamaterials, by contrast, typically explores periodic architectures in engineering design, owing to the simplicity of extracting their effective properties by homogenization.

Truss lattices are one such subclass of periodic cellular materials, exploited extensively over the past few decades [7, 8, 9]. A multitude of architected truss (meta-)materials has been introduced theoretically and experimentally with as-designed properties. Classical examples include extreme properties such as designs with high-strength- and/or stiffness-to-weight ratios [10], further unconventional properties such as auxeticity [11, 12] or near-infinite bulk-to-shear modulus ratios [12, 13, 14, 15]. Advancing from linear to nonlinear and dynamic material behavior, properties of interest have included energy absorption [16], acoustic wave tuning [17, 18], controllable nonlinear stress-strain behavior and shape recoverability under large deformations [19, 6], insensitivity to imperfections [20, 21, 22], and damage tolerance [23].

The almost infinite freedom in engineering the topology of cellular materials and the resulting enormous potential reflected by the above examples highlights the challenging inverse problem. Required are systematic approaches to obtain structures with desired properties. When it comes to optimizing the effective material behavior of periodic networks, a multitude of analytical [3], numerical [12, 24, 25] and empirical methods [26] have been deployed, successfully reaching, e.g., theoretical limits such as stiffness upper bounds [27, 28] or demonstrating extreme band gaps in their dispersion relations [29, 30]. The integration of such periodic architectures into real-world applications (from lightweight space structures to efficient

infills or patient-specific medical devices) is another challenge, since complex macroscale load conditions and constraints must be accounted for [9, 31, 32], so uniform periodic structures are not a solution, and structural-level topology optimization becomes a method of choice.

While topology optimization has evolved into a mature systematic design approach for structural optimization, the classical approach faces high computational costs in case of large-scale optimization problems involving several length scales. The recent benchmark presented in [33] proved the impressive capability of a modern high-performance implementation to optimize large structures in detail (based on more than one billion finite elements). If unregularized, the optimization problem lacks existence of solutions, meaning that increasing resolution leads to the appearance of finer and finer features (for a detailed summary on regularization approaches and manufacturability constraints, the reader is referred to [34]). In fact, for linear elastic problems with isotropic phases and multiple loads, the optimal local solution is given by laminations at multiple length-scales (3 in 2D and 6 in 3D) [35]. However, in a recent 2D microstructure optimization study [36] it was demonstrated that single-scale realizations can be obtained at low loss in performance. So-called homogenization-based approaches that use knowledge of optimal microstructures offer great potential for time savings. Such procedures require a separation of scales between the macroscale boundary value problem and the fine-scale microstructure. However, experience [37] shows that the optimal local material orientations resulting from such approaches ensure stretching-dominated microstructures that are less prone to scale separation issues.

A number of hierarchical multiscale topology optimization schemes have been introduced, which optimize a macroscale problem while accounting for the microscale topology by homogenization [38, 39, 40, 41] or computational FE^2 techniques [42]. Here, the optimization problem on the macroscale depends on a parametrization of the structural architecture on the lower scale, and the latter is optimized in a spatially varying fashion. Such schemes have often led to locally optimized (and spatially varying) unit cells (e.g., at the quadrature-point level) without ensuring proper compatibility and connectivity across the macroscale body, thus also lacking manufacturability. Different solutions have been proposed to assure the connectivity of spatially varying lattice topologies. In [43] and [44] a square-/tetrahedron-based topology description linked to a constant quadrilateral/tetrahedral mesh of the design domain in 2D and was used, respectively, with varying unit cell densities. An appealing generalization to allow for microstructural topology changes is the introduction of microstructural families, in which all members are interconnectable [45, 46]. In [47] non-designable connector cells to link adjacent cells were defined. In [48] and [49] a connectivity index used as a constraint during optimization was introduced. In [50] different microstructures were stitched to

have a better match, and in [51] transition layers that are optimized for optimal connectivity were introduced. All of these approaches produce elegant structures; however, the fixes come at the expense of a restricted design space and, more severely, the way different unit cells are connected may violate the homogenization assumptions of scale separation and periodicity.

An elegant alternative is the introduction of microstructures that are continuously graded in space – analogous to the transition from classical multi-material topology optimization defining a unique material at each point (e.g., [52, 53, 54]) to a continuous grading of materials [55]. In [56] a framework for free material optimization with constrained grading was presented and demonstrated its performance for rank-2 laminates; unfortunately, this approach lacked a projection onto a finite length scale. Recently the approaches shown in [37], [57], [58] and [59], in line with earlier work in [60], were used to construct spatially variant lattices on a finite length scale, based on a rectangular microstructure representation for which a homogenization-based surrogate model was used. A Similar hybrid approach has also been applied in 3D as presented in [61]. A recent review of such multi-scale topology optimization approaches can be found in [62].

In summary, identifying optimal structural architectures with fine-scale features for complex macroscale boundary value problems can be tackled by either high-performance topology optimization schemes on the macroscale (but those come with significant expenses) or by two-scale optimization approaches (which often lack compatibility or a highly limited design space). We here present a computational framework which aims at establishing compatible, manufacturable truss networks with a tailored length scale suitable for complex macroscale problems. Based on a chosen microstructure parametrization, we employ a semi-analytical homogenized continuum model for truss lattices accounting for finite rotations [63], which is used within a macroscale finite element setup (using both translations and rotations as primary fields). Based on the assumption of a continuously varying truss architecture on the macroscale, our framework allows for the optimization of spatially variant cellular lattice structures. A projection of the obtained set of truss unit cells at the macroscale onto a chosen finite length scale [64] results in the final truss design, thereby assuring manufacturability and respecting the assumptions of periodicity and scale separation. The general framework is applicable to, in principle, any periodic cellular material and hence enables the structural realization, combination and symbiosis of a vast range of microstructural topologies within a single body. We demonstrate the approach by seeking functionally-graded truss architectures having minimal compliance. Inspired by the atomic arrangement in crystals, we parametrize the truss unit cell via a set of Bravais lattice vectors along with Voronoi tessellation. Overall, our approach may be viewed as a generalization of those

introduced previously in [37], [65], and [57]. Other recent approaches in the field include those in [66] and [67].

In the following Section 2, we summarize the optimization methodology in four steps. First, Section 2.1 introduces the microstructure parametrizaion, followed by a brief summary of the homogenization approach in Section 2.2 and of the topology optimization problem in Section 2.3. Lastly, the projection onto the finite length scale is presented in Section 2.4. To demonstrate the performance of this framework, Section 4 presents a number of benchmarks for functionally graded truss lattices with minimized compliance. Finally, Section 5 concludes this work and discusses its benefits and limitations.

2 METHODOLOGY

The present optimization methodology is based on a two-scale description of the cellular body, which separates the macroscale boundary value problem from the underlying discrete structural architecture. By assuming a separation of scales, the small-scale truss network is condensed into an effective, homogenized continuum model to be used at the larger scale. The connecting link between both is the definition of the truss topology, which is defined on the macroscale in a spatially varying fashion. Like the displacement field as the primary unknown of the macroscale boundary value problem, the truss topology is continuously varied, and the local unit cell at any point on the macroscale is the basis for the homogenized mechanical response at that point. Figure 1 schematically illustrates the two-scale setup to be explained in the following.

2.1 Spatially variant truss topology parametrization

For the geometric description of spatially variant truss lattices, we borrow principles from (spatially invariant) crystal structures in solid state physics [68]. Confining ourselves to simple Bravais lattices [69], each site in an infinite lattice in d dimensions is located at position

$$\mathbf{r}' = \mathbf{r} + \sum_{i=1}^d n_i \mathbf{a}_i \quad \text{with} \quad n_i \in \mathbb{Z}, \quad (1)$$

where \mathbf{r} denotes a reference point, $\{\mathbf{a}_1, \dots, \mathbf{a}_d\}$ are the Bravais basis of linearly independent unit vectors, and $\{n_1, \dots, n_d\}$ is a unique set of integers. Towards the description of spatially variant structures, we now allow the primitive translation vectors to vary smoothly in space on the macroscale, introducing the (at least \mathcal{C}^1 -continuous) primitive translation vector fields $\mathbf{a}_i(\mathbf{X})$ ($i = 1, \dots, d$), where $\mathbf{X} \in \Omega$ denotes a position on

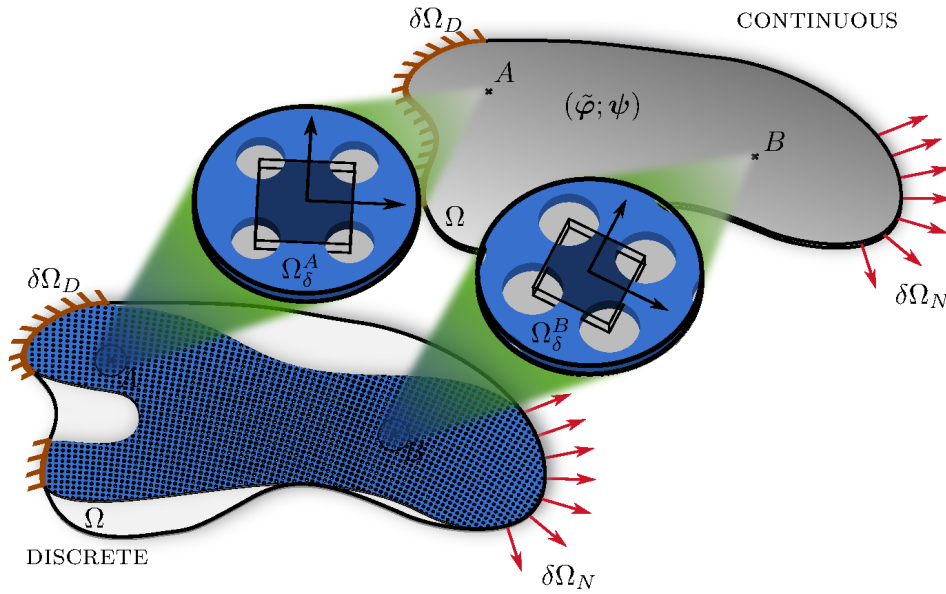


Figure 1: The *discrete* spatially variant structure is described on the macroscale as a mechanically equivalent *continuous* body, whose local effective constitutive behavior derives from the local definition of the truss topology, parameterized by the set ψ of all spatially varying topology variables and based on the assumption of a (quasi-)periodic lattice. The continuously varying topology variables ψ are optimized over the macro-domain Ω towards a minimum compliance for given boundary conditions (considering Neumann and Dirichlet boundaries $\delta\Omega_N$ and $\delta\Omega_D$, respectively). The final discrete truss representation is obtained by introducing a mapping τ' , which projects the continuous topology variable field ψ onto a discrete structure of finite length scale.

the macroscale body Ω in the undeformed configuration. In an ε -neighborhood of a point $\mathbf{X} \in \Omega$, the local lattice site locations are now approximated by

$$\mathbf{r}' \approx \mathbf{X} + \sum_{i=1}^d n_i \mathbf{a}_i(\mathbf{X}) \quad \text{with} \quad n_i \in B_\varepsilon[0] \subseteq \mathbb{Z}, \quad (2)$$

where $B_\varepsilon[x] = \{y \in \mathbb{Z} : |x - y| \leq \varepsilon\}$ defines a closed d -ball of integer radius $\varepsilon > 0$. Since the approximation (2) is only suitable if the basis vectors and hence the lattice spacing must be significantly smaller than any macroscopic fields of interest ($|\mathbf{a}_i| \ll |\Omega|$), we require a separation of scales between the fields describing the structural topology (here, $\mathbf{a}_i(\mathbf{X})$) and all macroscopic mechanical fields of interest (such as the displacement field). The topology variations are consequently so smooth on the macroscale that at each point $P \in \Omega$ the underlying structure within an ε -neighborhood can be approximated by a periodic lattice. Naturally, a spatially constant structure (i.e., a perfect lattice) is recovered on the macroscale if $\mathbf{a}_i(\mathbf{X}) = \text{const.}$

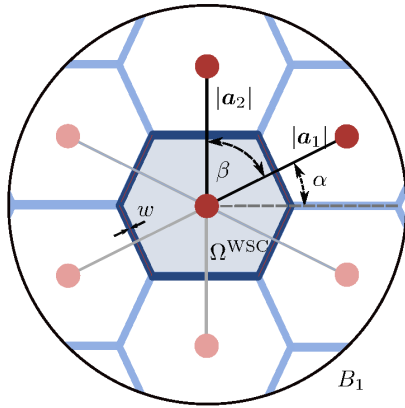


Figure 2: Construction of a unit-volume RUC in an ε -neighborhood B_1 around point $\mathbf{X} \in \Omega$. Based on the Bravais lattice parameters α , β , and $\gamma = |\mathbf{a}_2|/|\mathbf{a}_1|$ the lattice sites (red), and hence the Wigner-Seitz cell Ω_{WSC} , are uniquely defined. We choose to place nodes $\mathcal{B}_n^{\text{RUC}}$ and beams $\mathcal{B}_b^{\text{RUC}}$ (blue) on the RUC's corners and edges, respectively. All beam properties are collected in the set λ .

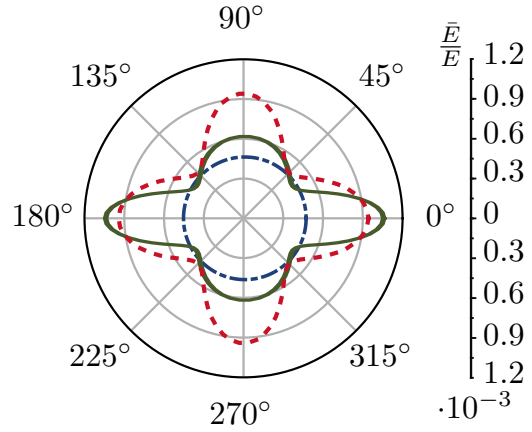


Figure 3: Effective directional Young's modulus vs. orientation for three different lattices at $\rho^{\text{RUC}} = 0.1$: the tetragonal lattice with a square RUC (dotted red, $\alpha = 0$, $\beta = \pi/2$, $\gamma = 1$), the orthorhombic lattice with a rectangular RUC (solid green, $\alpha = 0$, $\beta = \pi/2$, $\gamma = 2$), and the hexagonal lattice with a hexagonal RUC (dash-dotted blue, $\alpha = 0$, $\beta = \pi/3$, $\gamma = 1$).

for all $\mathbf{X} \in \Omega$, in which case (2) is exact for $\varepsilon \rightarrow \infty$ and coincides with (1).

The above Bravais construction only defines a point set. In order to arrive at a truss topology, one could potentially connect those sites by beams – this approach, however, is non-unique and rather restrictive in parametrizing the structural topology. Therefore, we instead use the Wigner-Seitz construction¹ [70] – based on the set of lattice sites – to define a unique primitive unit cell topology for a given set of Bravais basis vectors $\{\mathbf{a}_1, \dots, \mathbf{a}_d\}$. The Wigner-Seitz cell Ω_{WSC} is defined as the locus of points in space closer to one lattice site than to any other lattice site (see Figure 2). Its geometric construction can conveniently and efficiently be carried out by Voronoi tessellation over the neighborhood of lattice sites defined in (2) around any point $\mathbf{X} \in \Omega$. The Wigner-Seitz cell serves as representative unit cell (RUC) $\Omega_{\text{RUC}} = \Omega_{\text{WSC}}$ (see Figure 2), whose n_n^{RUC} outer vertices and n_b^{RUC} edges are identified as nodes and beams of a truss, respectively (and we denote the sets of all nodes and of all beams in the RUC by $\mathcal{B}_n^{\text{RUC}}$ and $\mathcal{B}_b^{\text{RUC}}$, respectively). This completes the unique definition of the truss unit cell topology based on a given set of (local) Bravais basis vectors.

For convenience, we represent the Bravais lattice vectors in fractional coordinates, i.e., in 2D $\mathbf{a}_1 =$

¹We point out that this choice is only one possible option among various others (e.g., one could extend the unit cell definition to include several particles, as originally done for multi-lattices in [68]). The general approach laid out here is independent of the specific choice of topology parametrization.

$(|a_1| \cos \alpha, |a_1| \sin \alpha)$ and $a_2 = (|a_2| \cos(\alpha + \beta), |a_2| \sin(\alpha + \beta))$, where angles α and β define, respectively, the orientation and the relative orientation of the two Bravais vectors (see Figure 2). The scale separation allows us to define the homogenization problem on any scale. To ensure RUC uniqueness, we enforce the representative unit cell to have a normalized volume of $|\Omega_{\text{RUC}}| = |\det(a_1, \dots, a_d)| = 1$. The volume constraint reduces the number of independent Bravais lattice variables to $d^2 - 1$. In 2D, we choose α , β , and $\gamma = |a_2|/|a_1|$.

Since the mechanical response of a truss depends not only on topology but also on its material parameters and strut geometry, we here assume that all beams are of rectangular cross-section with constant out-of-plane thickness t and spatially varying width $w(\mathbf{X})$. (It is straightforward to relax this constrained by introducing additional geometric design variables.) The beam width w is a direct consequence of the effective density $\bar{\rho}(\mathbf{X})$ through $w = \bar{\rho}(\mathbf{X})|\Omega_{\text{RUC}}|/L$. All beams are assumed to be composed of the same isotropic linear elastic material with Young's modulus E and mass density ρ . The beam properties are summarized in the set $\lambda(\mathbf{X}) = \{E, \rho, t, w(\mathbf{X})\}$, which in the spatially variant context varies with position $\mathbf{X} \in \Omega$ on the macroscale, analogous to the basis vectors. From now on, we refer to the set of all design variables, uniquely defining the associated RUC Ω_{RUC} as well as $\mathcal{B}_n^{\text{RUC}}$ and $\mathcal{B}_b^{\text{RUC}}$, as

$$\psi(\mathbf{X}) = \{a_1(\mathbf{X}), \dots, a_d(\mathbf{X}); \lambda(\mathbf{X})\}. \quad (3)$$

Any further quantities required for the subsequent optimization problem, such as the local mass density $\rho(\mathbf{X})$ or the effective mechanical response (of an equivalent periodic structure), can be extracted from a given set $\psi(\mathbf{X})$ via homogenization, as described in the following.

2.2 Effective continuum description based on first-order homogenization

The topology optimization problem requires information about the local mechanical constitutive behavior on the macroscale, which must depend on the truss architecture on the microscale. Our natural solution is a first-order homogenization approach, exploiting the assumed separation of scales and extracting the effective response from the RUC. We here employ the semi-analytical approach in [63], whose framework provides an efficient description of periodic truss lattices of general linear elastic beam architectures, accounting for finite rotations and hence geometric nonlinearity. In the following, we summarize the homogenization technique to the extent necessary for subsequent discussions and discuss its validity for the

investigated type of spatially variant trusses. For further details of the model and its numerical implementation we refer to [63].

Acknowledging that the deformation of Timoshenko-Ehrenfest beams is described by both rotations and translations, we employ a macroscale kinematic continuum description of micropolar type, introducing two primary fields on the macroscale: a deformation mapping $\mathbf{x} = \boldsymbol{\varphi}(\mathbf{X})$ and a rotation field $\boldsymbol{\theta} = \boldsymbol{\theta}(\mathbf{X})$, where $\mathbf{x} \in \boldsymbol{\varphi}(\Omega)$ and $\mathbf{X} \in \Omega$ are the deformed and undeformed positions of a material point. Assuming the deformation fields vary smoothly (at least \mathcal{C}^1 -continuous), the local deformation within an infinitesimal neighborhood of a point $\mathbf{X} \in \Omega$ is approximated to first order² by

$$\begin{aligned} x_i(\mathbf{X} + d\mathbf{X}) &= \varphi_i(\mathbf{X}) + F_{iJ}(\mathbf{X}) dX_J + \text{h.o.t.}, \\ \theta_i(\mathbf{X} + d\mathbf{X}) &= \theta_i(\mathbf{X}) + \kappa_{iJ}(\mathbf{X}) dX_J + \text{h.o.t.}, \end{aligned} \quad (4)$$

with deformation gradient $\mathbf{F}(\mathbf{X}) = \nabla \boldsymbol{\varphi}(\mathbf{X})$ and curvature tensor $\boldsymbol{\kappa}(\mathbf{X}) = \nabla \boldsymbol{\theta}(\mathbf{X})$. Under the assumption of a separation of scales, we apply (4) in the neighborhood of $\mathbf{X} \in \Omega$ to the nodes in the truss RUC centered at \mathbf{X} and defined by $\psi(\mathbf{X})$. Consequently, every node $\alpha \in \mathcal{B}_n^{\text{RUC}}$ initially located at $\mathbf{X}_\alpha^m \in \Omega_{\text{RUC}}$ is deformed according to

$$\begin{aligned} \mathbf{x}_\alpha^m &= \boldsymbol{\varphi}(\mathbf{X}) + \mathbf{F}(\mathbf{X}) \mathbf{X}_\alpha^m + \delta \mathbf{x}_\alpha + \text{h.o.t.}, \\ \boldsymbol{\theta}_\alpha^m &= \boldsymbol{\theta}(\mathbf{X}) + \boldsymbol{\kappa}(\mathbf{X}) \mathbf{X}_\alpha^m + \delta \boldsymbol{\theta}_\alpha + \text{h.o.t.} \end{aligned} \quad (5)$$

Here and in the following, the superscript m denotes microscale quantities. Importantly, unlike the affine deformation in (4), the approximations (5) introduce shifts $\tilde{\boldsymbol{\delta}}_\alpha = (\delta \mathbf{x}_\alpha, \delta \boldsymbol{\theta}_\alpha)$, which allow nodes to deform relative to the RUC average in a periodic fashion. By defining one set of shifts for each unique periodic node in the unit cell, this effectively imposes periodic boundary conditions for both nodal translations and rotations and hence ensures that the average primary fields ($\boldsymbol{\varphi}$ and $\boldsymbol{\theta}$) and their gradients (\mathbf{F} and $\boldsymbol{\kappa}$) are imposed as averages across the RUC. The relaxation from an affine to a general periodic deformation of the RUC proves to be especially important for bending-dominated truss architectures, in which soft modes are accommodated primarily by bending in a manner far from affine deformation [63].

²For reduced computational complexity, we choose to truncate the Taylor series to linear order. A detailed discussion and a comparison with second-order approximations can be found in [63].

Based on the co-rotational beam description in [71], the strain energy of each beam in the RUC is a function of the nodal displacements and rotations, such that an effective strain energy density can be defined as the RUC average

$$W(\psi; \mathbf{F}; \boldsymbol{\theta}; \boldsymbol{\kappa}; \tilde{\boldsymbol{\delta}}) = \frac{1}{V_{\text{RUC}}} \sum_{\nu \in \mathcal{B}_b^{\text{RUC}}(\psi)} W_\nu(\tilde{\mathbf{x}}_{\nu_1}^m, \tilde{\mathbf{x}}_{\nu_2}^m), \quad (6)$$

where $V_{\text{RUC}} = |\Omega_{\text{RUC}}|$ is the volume (or area in 2D) of the RUC, and W_ν is the strain energy of beam ν having the two nodes ν_1 and ν_2 with degrees of freedom $\tilde{\mathbf{x}}_\alpha = (\mathbf{x}_\alpha^m, \boldsymbol{\theta}_\alpha^m)$ from (5) for $\alpha = \nu_1, \nu_2$. We note that the resulting energy density W is effectively independent of φ , since $\varphi(\mathbf{X})$ in (5) merely constitutes rigid-body translations, which do not affect the strain energy (whereas $\boldsymbol{\theta}(\mathbf{X})$ implies nodal rotations and beam bending, hence not implying rigid-body rotations).

For linear elasticity, the shifts are expected to minimize the unit cell energy (which is local in the shifts), so that we may condense them out on the microscale. The resulting condensed energy density may be stated as

$$W^*(\psi; \mathbf{F}; \boldsymbol{\theta}; \boldsymbol{\kappa}) = \min_{\tilde{\boldsymbol{\delta}}} \{W(\psi; \mathbf{F}; \boldsymbol{\theta}; \boldsymbol{\kappa}; \tilde{\boldsymbol{\delta}}) : \text{constr.}\}, \quad (7)$$

with constraints ensuring that the shifts $\tilde{\boldsymbol{\theta}}$ do not violate the imposition of the average kinematic variables from the macroscale (see [63]). (7) defines a generally nonlinear optimization problem to be solved numerically in an iterative fashion³. With the above effective energy density W^* (dependent on the local unit cell architecture ψ), we may employ principles of continuum mechanics to derive, e.g., the first Piola-Kirchhoff stress tensor as $\mathbf{P} = \partial W^* / \partial \mathbf{F}$ as well as analogous couple stress tensors associated with the remaining macroscale fields, as well as consistent stiffness matrices such as $\mathbb{C} = \partial^2 W^* / \partial \mathbf{F} \partial \mathbf{F}$.

Finally, for a given field $\psi(\mathbf{x})$ defining the local truss architecture, we can solve the macroscale boundary

³Although this minimization must be carried out numerically in general, all first and second derivatives with respect to the kinematic variables can be computed in closed-form, thus allowing for the efficient use of consistent tangents [63].

value problem on Ω , viz.

$$(\boldsymbol{\varphi}, \boldsymbol{\theta})_\psi = \arg \inf \left\{ \int_{\Omega} W^*(\boldsymbol{\psi}; \mathbf{F}, \boldsymbol{\theta}, \boldsymbol{\kappa}) \, dV - \int_{\partial\Omega_T} \hat{\mathbf{T}} \cdot \boldsymbol{\varphi} \, dS - \int_{\partial\Omega_m} \hat{\mathbf{m}} \cdot \boldsymbol{\theta} \, dS : \boldsymbol{\varphi} = \hat{\boldsymbol{\varphi}} \text{ on } \partial\Omega_u, \boldsymbol{\theta} = \hat{\boldsymbol{\theta}} \text{ on } \partial\Omega_\theta \right\} \quad (8)$$

with tractions $\hat{\mathbf{T}}$ acting on the boundary $\partial\Omega_T \subset \partial\Omega$, and moments $\hat{\mathbf{m}}$ imposed on $\partial\Omega_m \subset \partial\Omega$. For conciseness, we introduce the generalized deformation mapping $\tilde{\boldsymbol{\varphi}}(\mathbf{X}) = (\boldsymbol{\varphi}(\mathbf{X}), \boldsymbol{\theta}(\mathbf{X}))$ along with $\tilde{\mathbf{F}} = \nabla \tilde{\boldsymbol{\varphi}}$ and $\hat{\mathbf{t}} = (\hat{\mathbf{T}}, \hat{\mathbf{m}})$, such that (8) simplifies to

$$\tilde{\boldsymbol{\varphi}} = \arg \inf \left\{ \int_{\Omega} W^*(\boldsymbol{\psi}; \tilde{\boldsymbol{\varphi}}, \tilde{\mathbf{F}}) \, dV - \int_{\partial\Omega_N} \hat{\mathbf{t}} \cdot \tilde{\boldsymbol{\varphi}} \, dS : \tilde{\boldsymbol{\varphi}} = \hat{\boldsymbol{\varphi}} \text{ on } \partial\Omega_D \right\} \quad (9)$$

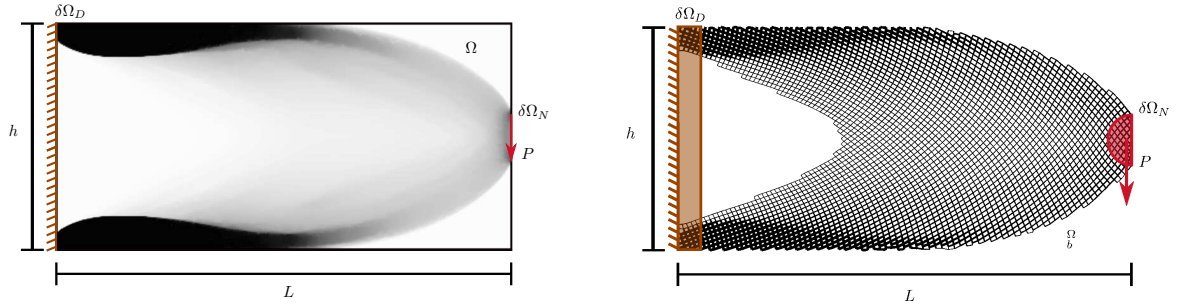
with the combined Dirichlet boundary $\partial\Omega_D$.

2.3 Topology optimization

In topology optimization we classically seek to find the optimal material distribution that minimizes an objective function under given constraints. Here, the global design field is $\boldsymbol{\psi}(\mathbf{X})$, which we define to be varying continuously across Ω (or its finite element discretization Ω_h). In our examples, we focus on classical benchmarks that minimize the compliance for single-load-case problems while enforcing a total volume (or mass) constraint. However, the framework presented here is sufficiently general to be extended to more complex objective functions and, specifically, it is already laid out for nonlinear problems (since the homogenization scheme accounts for finite beam rotations).

The optimization problem is formalized by

$$\begin{aligned} \min_{\boldsymbol{\psi}} : \quad & \mathcal{L}(\boldsymbol{\psi}; \tilde{\boldsymbol{\varphi}}) = \int_{\Omega} \ell(\boldsymbol{\psi}; \tilde{\boldsymbol{\varphi}}) \, dV = \int_{\Omega} \left[W^*(\boldsymbol{\psi}; \tilde{\boldsymbol{\varphi}}, \tilde{\mathbf{F}}) + c_p ||\nabla \boldsymbol{\psi}_i||_p \right] \, dV \\ \text{s.t.} : \quad & \int_{\Omega} W^*(\boldsymbol{\psi}; \tilde{\boldsymbol{\varphi}}, \tilde{\mathbf{F}}) \, dV = \int_{\partial\Omega_S} \hat{\mathbf{t}} \cdot \tilde{\boldsymbol{\varphi}} \, dS, \\ & : \int_{\Omega} \rho(\boldsymbol{\psi}) \, dV - V_{\max} \leq 0, \\ & : \text{RUC topology constraints,} \end{aligned} \quad (10)$$



(a) Continuum cantilever beam problem as defined in [74]. All nodes on the left edge are clamped. The load $P = 10^{-6}$ is applied as distributed load over the central 20% of the right edge. Solid black indicates 50% volume fraction.

(b) Discrete cantilever beam. All nodes with distance to the left edge smaller than $0.1h$ are clamped. The load P is distributed to all nodes with distance smaller $0.1h$ to the centerright point. This image serves for visualization purposes only.

Figure 4: The cantilever beam is well studied and serves as benchmark. In this study, the beam domain Ω has a length $L = 2$ and a height $h = 1$. Furthermore, we choose the load $P = 10^{-6}$.

where $\|(\cdot)\|_p$ denotes the L^p norm (in the following, we use $p = 2$), and the L^p -constraint [72] governs the smoothness of the global design variable field $\psi(\mathbf{X})$ through a regularization constant $c_p \geq 0$. V_{\max} defines the maximum material volume in the domain Ω (in subsequent examples we choose $\rho^\Omega = V_{\max}/|\Omega| = 0.2$), and the “RUC topology constraints” stand for any constraints imposed on the local truss topology and architecture (such as constraints on the unit cell topology, beam geometry, etc.). For the design updates of ψ we use the method of moving asymptotes [73]. Due to its nonlinear nature, the above optimization problem is solved iteratively, minimizing the objective with respect to the design variables ψ in a step-wise fashion. At each iteration step, the multiscale finite element problem defined in (2.2) is solved for $\tilde{\varphi}$ in equilibrium. Computing the increments of the design field ψ requires computing its gradient, which is classically termed the sensitivity and given by

$$\frac{\partial \ell}{\partial \psi_i} = \frac{\partial W^*}{\partial \psi_i} + c_p \frac{\nabla \psi_i |\nabla \psi_i|^{p-2}}{\|\nabla \psi_j\|_p^{p-1}}, \quad (11)$$

where the semi-analytical homogenization scheme introduced in Section 2.2 allows us to efficiently calculate the change of the condensed energy density ∂W^* , locally in each quadrature point, with respect to a design variable change $\partial \psi_i$ through a local forward-difference scheme (introducing a small perturbation on each design variable of 10^{-9}).

For a performance comparison to literature benchmarks, we restrict our study to the cantilever beam in

Figure 4a with an applied load of magnitude P and define the beam compliance, normalized by the effective density ρ^Ω , as

$$\mathcal{C}_C(\tilde{\mathbf{x}}) = \frac{\rho^\Omega}{P^2} \int_{\Omega} W^*(\psi; \tilde{\varphi}, \tilde{\mathbf{F}}) dV. \quad (12)$$

In subsequent examples, we study three different RUC families in $d = 2$ dimensions (2D), whose truss architectures are constrained by the RUC topology constraints in Table 1. The square lattice family resembles the study in [37] and serves as a benchmark. The rectangular lattice family, and ultimately the monoclinic Bravais lattice, exemplify two generalizations facilitated by this approach. Note that the effective density $\bar{\rho}$ is analogous to classical density-based topology optimization, while the Bravais lattice variables (α, β, γ) allow for tailoring of the local anisotropy of the effective elastic surfaces. By letting the effective density vary up to 50%, we are stretching the assumption of slender beams. Please find a detailed discussion and reasoning of the upper density bound in A. As initial guess we use a homogeneous design variable field with values in the center of the design variable ranges.

Table 1: RUC topology constraints for tetragonal and orthorhombic crystal lattice families, and a “monoclinic” Bravais lattice parametrization that includes all primitive Bravais lattice families in 2D (tetragonal, hexagonal, orthorhombic, monoclinic). While the tetragonal lattice family is widely used in the literature, other lattice families are oftentimes neglected, which restricts the design space.

tetragonal	orthorhombic	monoclinic
$-\pi \leq \alpha \leq \pi$	$-\pi \leq \alpha \leq \pi$	$-\pi \leq \alpha \leq \pi$
$\beta = \pi/2$	$\beta = \pi/2$	$0 \leq \beta \leq \pi$
$\gamma = 1$	$0.5 \leq \gamma \leq 2$	$0.5 \leq \gamma \leq 2$
$10^{-5} \leq \bar{\rho} \leq 0.5$	$10^{-5} \leq \bar{\rho} \leq 0.5$	$10^{-5} \leq \bar{\rho} \leq 0.5$

2.4 From the continuous solution to a discrete structure

Solving the optimization problem (10) results in a continuous distribution of the truss design parameter field ψ across Ω on the macroscale, whose underlying microstructure is, in principle, infinitely fine based on the separation of scales. In order to construct a discrete truss at a finite length scale (based on the continuous optimal field ψ obtained from (10)), we here extend the approach presented in [64].

We introduce a mapping $\epsilon(\mathbf{X}) : \Omega \rightarrow [0, 1]$, such that a value of 0 refers to one phase (e.g., void) and a value of 1 to another phase (e.g., solid). Most generally, we represent $\epsilon(\mathbf{X})$ of a periodic unit cell in terms of a Fourier series (e.g., we find the complex amplitudes for a discretely defined unit cell through a fast Fourier transform). When assuming translational symmetry such as in a lattice, we use the symmetry information and represent the infinite structure in terms of the Fourier series over reciprocal lattice vectors, most generally written as

$$\epsilon(\mathbf{X}) = \sum_{\mathbf{k}} b_{\mathbf{k}} e^{i2\pi\mu\mathbf{k}\cdot\mathbf{X}} \quad \text{with} \quad \mathbf{k} = \sum_{i=1}^d m_i \mathbf{k}_i \quad (13)$$

being an integer combination of the primitive reciprocal lattice vectors \mathbf{k}_i , and $b_{\mathbf{k}}$ denoting the complex amplitude related to the spatial harmonic with reciprocal lattice vector \mathbf{k} . μ represents a dimensionless length scale introduced to govern the unit cell size. Translational symmetry is ensured by the primitive reciprocal lattice vectors which, in \mathbb{R}^3 , are given by

$$\mathbf{k}_1 = \frac{\mathbf{a}_2 \times \mathbf{a}_3}{\mathbf{a}_1 \cdot (\mathbf{a}_2 \times \mathbf{a}_3)}, \quad \mathbf{k}_2 = \frac{\mathbf{a}_3 \times \mathbf{a}_1}{\mathbf{a}_2 \cdot (\mathbf{a}_3 \times \mathbf{a}_1)}, \quad \mathbf{k}_3 = \frac{\mathbf{a}_1 \times \mathbf{a}_2}{\mathbf{a}_3 \cdot (\mathbf{a}_1 \times \mathbf{a}_2)}, \quad (14)$$

based on the primitive Bravais lattice vectors \mathbf{a}_i . In 2D, the reciprocal lattice vectors \mathbf{k}_1 and \mathbf{k}_2 follow from (14) with $\mathbf{a}_3 = (0, 0, 1)$.

When constructing a spatially variant truss, the spatial variation of $\mathbf{k}(\mathbf{X})$ renders (13) problematic, since the latter requires a constant history of the frequency vectors \mathbf{k} in space. When violated, highly distorted projections arise. As a remedy, in [64] a projection function $\phi_{\mathbf{k}}(\mathbf{X})$ was introduced to obtain the mapping

$$\epsilon'(\mathbf{X}) = \sum_{\mathbf{k}} b_{\mathbf{k}} e^{i2\pi\mu\phi_{\mathbf{k}}(\mathbf{X})} \quad (15)$$

with lattice symmetry enforced locally through

$$\nabla \phi_{\mathbf{k}}(\mathbf{X}) = \mathbf{k}(\mathbf{X}). \quad (16)$$

That is, we ensure that $\nabla\phi_{\mathbf{k}}$ is locally tangential to the (local) \mathbf{k} -vector defined through (14) at every point on the macroscale.

Finding the field $\phi : \Omega \rightarrow \mathbb{R}^d$, in principle, requires the solution of an over-determined system. When the lattice is perfectly periodic, the system has the solution $\phi_{\mathbf{k}}(\mathbf{X}) = \mathbf{k} \cdot \mathbf{X} + c$ with arbitrary $c \in \mathbb{R}$. By contrast, for all spatially variant trusses, we find $\phi_{\mathbf{k}}$ as a least-square minimizer:

$$\phi_{\mathbf{k}}(\mathbf{X}) = \arg \min \int_{\Omega} \|\nabla\phi_{\mathbf{k}}(\mathbf{X}) - \mathbf{k}\|^2 d\Omega. \quad (17)$$

Given a separation of scales between the spatial variation of the lattice vectors and the introduced RVE length scale μ , this ensures quasi-periodicity in the neighborhood of each RVE (on the microscale). The global residual defined by (17) (which is generally non-zero) can thus be interpreted as a measure of the violation of scale separation.

For the lattice description introduced in Section 2.1, we define a mapping function $\tau(\mathbf{X})$ which attains a value of 1 at each lattice site while being 0 elsewhere:

$$\tau(\mathbf{X}) = \prod_{i=1}^d \sum_{n=-\infty}^{\infty} \delta\left(\mu \frac{\mathbf{k}_i \cdot \mathbf{X}}{\|\mathbf{k}_i\|} - n\|\mathbf{k}_i\|\right) = \prod_{i=1}^d \text{III}(\mu \mathbf{k}_i \cdot \mathbf{X}), \quad (18)$$

where $\delta(x)$ and $\text{III}(x)$ denote the Kronecker delta and Kronecker delta impulse train, respectively, in d dimensions. Decomposing (18) into spatial harmonics, the lattice mapping function can be represented as the Fourier series

$$\tau(\mathbf{X}) = \prod_{i=1}^d \frac{1}{1+2M} \sum_{m=-M}^M e^{i2\pi m \mu \mathbf{k}_i \cdot \mathbf{X}} = \prod_{i=1}^d \frac{1}{1+M} \left[1 + \sum_{m=1}^M \cos(2\pi m \mu \mathbf{k}_i \cdot \mathbf{X}) \right]. \quad (19)$$

Note that, in general, an infinite number ($M \rightarrow \infty$) of spatial harmonics is required to represent the Dirac combs exactly. For implementation purposes, we truncate the above Fourier series and, using the fact that

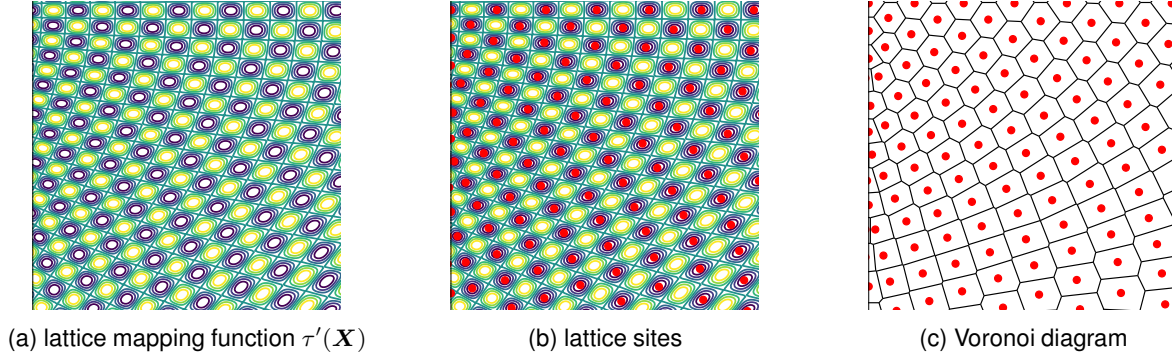


Figure 5: The discrete lattice is constructed from the lattice mapping function by first identifying the lattice sites, e.g., at lattice mapping function minima, and second constructing the Voronoi diagram over all lattice sites.

the translational symmetry is contained in all spatial harmonics, choose $M = 1$ such that

$$\tau'(\mathbf{X}) = \frac{1}{2^d} \prod_{i=1}^d [1 + \cos(2\pi\mu\phi_{\mathbf{k}_i}(\mathbf{X}))] \quad (20)$$

represents the truncated lattice mapping function with locally enforced lattice symmetry according to (16). We thus converted the strictly periodic and discontinuous lattice mapping (18) into a spatially varying and \mathcal{C}^∞ -continuous truncated mapping function (20), whose local maxima represent lattice site locations and have value 1 for convenience of implementation. We thus identify the lattice sites within Ω as the local maxima of (20) (see Figure 5b). Finally, the truss is constructed by extracting all nodes \mathcal{B}_n^Ω and beams \mathcal{B}_b^Ω of width $w(\mathbf{X}) > w_{\min}$ – analogous to the construction of the RUC described in Section 2.1 – from the Voronoi diagram over all lattice sites in the global domain Ω (see Figure 5c). The threshold w_{\min} reflects the lower bound on $\bar{\rho}$ set in Table 1.

2.5 Discrete description

With the effective continuum description introduced in Section 2.2 we efficiently approximate the lattice behavior, as demonstrated previously for periodic lattices in [63]. To validate its applicability to the spatially-variant lattices introduced here, we compare to full discrete simulations.

Based on the global sets of nodes and beams, \mathcal{B}_n^Ω and \mathcal{B}_b^Ω , respectively (see Section 2.1), we define the total potential energy of the beam network subjected to generalized external nodal tractions $\hat{\mathbf{t}}$ acting on

all nodes in $\mathcal{B}_n^{\partial\Omega_N}$ as

$$I(\tilde{\mathbf{x}}) = \sum_{\nu \in \mathcal{B}_b^\Omega} W_\nu(\tilde{\mathbf{x}}_{\nu_1}, \tilde{\mathbf{x}}_{\nu_2}) - \sum_{\alpha \in \mathcal{B}_n^{\partial\Omega_N}} (\hat{\mathbf{t}}_\alpha \cdot \tilde{\mathbf{x}}_\alpha), \quad (21)$$

where $\tilde{\mathbf{x}} = \{\tilde{\mathbf{x}}_1, \dots, \tilde{\mathbf{x}}_{n_n}\}$ is the set of all nodal degrees of freedom. Unlike for the continuum cantilever beam in Figure 4a, the load P is distributed over a semi-circular area $\partial\Omega_N$, as shown in Figure 4b, to assure an even load distribution between discrete nodes. For analogous reasons, the fixed boundary condition at the left boundary of the domain is spread over a thin slice $\mathcal{B}_n^{\partial\Omega_D}$. Classically, the generalized force vector of node α , containing both forces and moments, and the associated stiffness matrix follow as, respectively,

$$\tilde{\mathbf{t}}_\alpha(\tilde{\mathbf{x}}) = \frac{\partial I}{\partial \tilde{\mathbf{x}}_\alpha}(\tilde{\mathbf{x}}), \quad \tilde{\mathbf{K}}_{\alpha\beta}(\tilde{\mathbf{x}}) = \frac{\partial I}{\partial \tilde{\mathbf{x}}_\alpha \partial \tilde{\mathbf{x}}_\beta}(\tilde{\mathbf{x}}). \quad (22)$$

We obtain the quasistatic response from energy minimization, i.e.,

$$\tilde{\mathbf{x}} = \arg \min \{I : \tilde{\mathbf{x}}_\alpha = \mathbf{0} \text{ for } \alpha \in \mathcal{B}_n^{\partial\Omega_D}\}, \quad (23)$$

where the generalized displacements $\tilde{\mathbf{x}}_\alpha$ of all nodes in $\mathcal{B}_n^{\partial\Omega_D}$ near the left boundary are enforced to be zero. For comparability with literature and the compliance of the effective continuum description (12), we define the normalized compliance for the discrete beam network as

$$\mathcal{C}_D(\tilde{\mathbf{x}}) = \frac{\rho^\Omega}{P^2} \sum_{\nu \in \mathcal{B}_b^\Omega} W_\nu(\tilde{\mathbf{x}}_{\nu_1}, \tilde{\mathbf{x}}_{\nu_2}), \quad \text{where} \quad \rho^\Omega = \frac{1}{|\Omega|} \sum_{\nu \in \mathcal{B}_b^\Omega} w_\nu L_\nu t \rho \quad (24)$$

with L_ν denoting the length of beam ν .

3 NUMERICAL IMPLEMENTATION

The mechanical boundary value problem on the macroscale, described by the variational optimization problem (9) or (23), is solved via a finite-element approximation which discretizes Ω into Ω_h , using bi-linear

quadrilateral elements to result in bi-linear interpolations of both the displacement field φ_h and the rotation field θ_h across Ω_h . To accommodate the micropolar nature of the discretization, we use an in-house finite-element code, which solves the stationarity conditions (i.e., the equations of linear momentum balance) via Newton-Raphson iteration for quasistatic equilibrium. Further details about the numerical treatment of the homogenized continuum model can be found in [63].

The design parameter field $\psi(\mathbf{X})$, defined in (3), is interpolated using the exact same finite element approximation based on bi-linear quadrilateral elements, thus providing a continuous field of spatially varying truss unit cell architectures. As pointed out in Section 2.3, finding the solution for $\psi(\mathbf{X})$ involves the method of moving asymptotes. The overall optimization problem is solved in an iterative fashion, minimizing the objective function with respect to field $\psi(\mathbf{x})$, while solving the macroscale boundary value problem.

To construct the discrete truss in a postprocessing step from the given interpolated ψ -field, we first solve for the projection function (17), using again the same finite element approximation, and then identify the lattice sites as local maxima of (20). Only at this step we introduce the finite length scale μ . Finally, we build the global Voronoi diagram and extract node locations and beam connections.

4 NUMERICAL EXAMPLES

The introduced methodology is a tool for the optimization of generic structures based on a free choice of the underlying Bravais RUC topology and constituents. In the following, we showcase the potential of this approach by studying the optimization of tetragonal, orthorhombic and monoclinic truss lattices, and we investigate the influence of the RUC constraints. Moreover, we discuss the underlying assumption of a separation of scales and demonstrate how it can be (approximately) fulfilled in the lattice projection as a trade-off between continuum design variable field regularization and choice of length scale.

4.1 Tetragonal lattice family

The tetragonal truss lattice family (see Table 1) has been extensively studied in the literature and is the basis of various lattice optimization schemes (e.g. [43, 48, 37]). Hence, the tetragonal lattice family serves as an excellent introductory example and benchmark for our method. We first present optimized continuum design variable results and discuss the influence of mesh element size and the relaxation constant. Afterwards, we project the continuous fields onto a finite scale and compare the performance of the discrete truss lattice with that of the optimized continuum.

Continuum

We solve the optimization problem stated in (10), subjected to the tetragonal RUC constraints (see Table 1), on a continuum mesh of 400x200 Q4 elements. The mesh resolution was chosen as a trade-off between convergence (see Figure 7), fine resolution for projection step, and acceptable computation time (< 20 minutes on a regular laptop until convergence). The infimizing design variable fields $\psi(\mathbf{X})$ for low ($c_p = 10^{-13}$), medium ($c_p = 10^{-12}$) and strong ($c_p = 10^{-11}$) regularization are presented in Figure 19. The

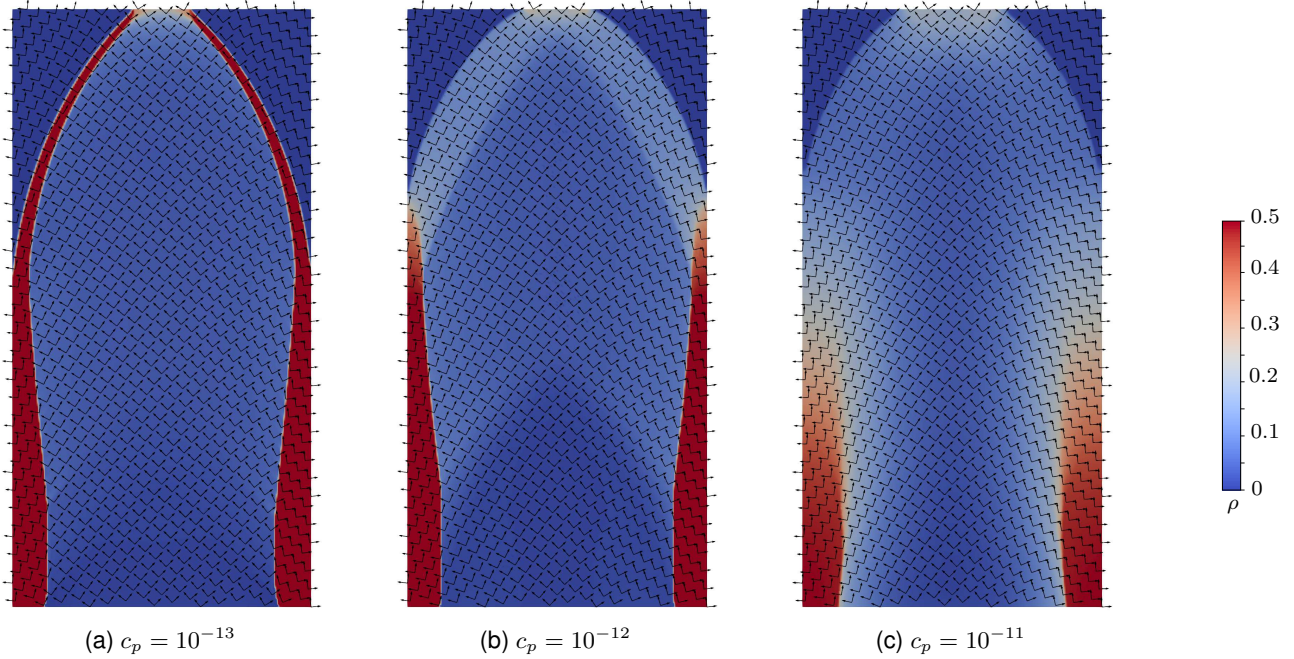


Figure 6: Optimized cantilever beam based on a tetragonal truss lattice for different regularizations. Local Bravais bases are indicated by arrows, and the density is shown by the color code. The arrows are scaled and shown at selected locations for readability. Resolution: 400x200 elements. All plots are rotated by 90° . Full design variable fields can be found in Figure 19.

Table 2: Minimized continuum compliance \mathcal{C}_C for tetragonal, orthorhombic, and monoclinic crystal lattice families with different regularization constants c_p and initial guesses. The (H)omogeneous initial guess assumes initial angles $\alpha = \pi/4$, $\beta = \pi/2$, $\gamma = 1$, and $\rho = \rho^\Omega = 0.2$. The (O)rthotropic initial guess uses the optimized fields from the orthotropic lattice family as initial guess.

c_p	tetragonal	orthorhombic	monoclinic	
	(H)	(H)	(H)	(O)
10^{-13}	66.6	62.2	76.3	62.2
10^{-12}	67.4	63.3	78.4	63.3
10^{-11}	84.8	79.9	88.2	79.9

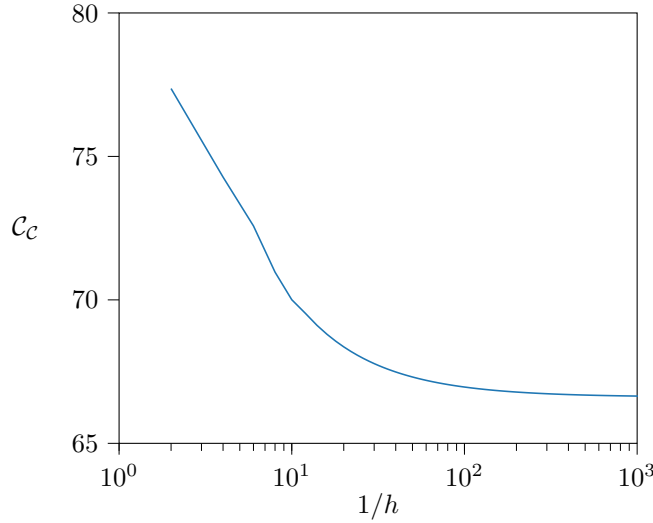


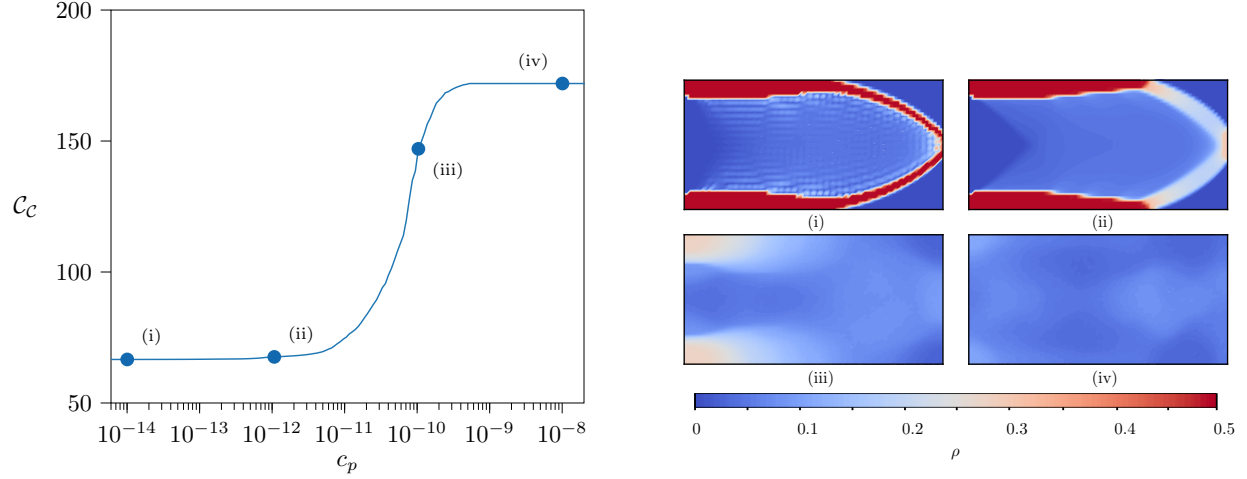
Figure 7: Compliance versus mesh resolution for tetragonal lattice cantilever problem. A mesh of 80x40 elements is within 2% of the converged compliance 66.6. $c_p = 10^{-13}$.

resulting Bravais bases vectors and density field can be found in [Figure 6](#). The corresponding compliance values are shown in [Table 2](#).

The regularization, as a constraint on the design variable field, has a detrimental effect on the effective compliance. The regularization's influence on the compliance and density field is illustrated in [Figure 8a](#) and [Figure 8b](#), respectively. While for low regularization, its influence on compliance and density is negligible (see case (i)), the compliance is affected with increasing c_p (case (ii)). When further increasing, the compliance degrades strongly (case (iii)) and finally reaches a second plateau (case (iv)). This upper plateau refers to spatially constant values of α and ρ . Given the negative effect on structural performance, one might wonder why we use regularization. The reasons are twofold.

First, with no or too little regularization, numerical (interpolation-dependent) artifact patterns arise (see case (i)). The effect is comparable to the well-known checkerboarding in classical topology optimization with discrete density fields [75]. The chosen FE discretization leads to artificially stiff results, and the projection of such laminated lattices onto a finite scale would result in disconnected lattices. Regularization alleviates this problem. Alternatively, the problem could be avoided by increasing the element interpolation order. However, we here choose the regularization to control the length scale and restrict our finite elements to linear interpolation for simplicity.

Second, the continuously described RUCs may feature abrupt changes of the design variables (e.g., when crossing finite element boundaries on the macroscale). When projecting those onto a finite discrete



(a) Compliance versus regularization constant. For a low regularization constant the compliance converges to a minimum, while for high regularization constants the compliance plateaus at its maximum.

(b) Effective density for the optimized cantilever beam based on a tetragonal lattice for different relaxation constants c_p , as indicated by the markers in (a). Discretization: 80x40 elements.

Figure 8: Influence of the regularization constant c_p .

lattice, this may either locally break the assumption of quasi-periodicity (see Equation 2) or require high resolution of the discrete projection (in fact, infinite resolution in the case of discrete design variable jumps, so $\mu \rightarrow 0$). The regularization constant gives us control over the locally permitted change of the unit cell in the lattice and hence guarantees a finite length scale ($\mu > 0$) of the discrete lattice.

In comparison with optimization results of other topology optimization schemes, the compliance for the tetragonal lattice with regularizations $c_p = 10^{-13}$ ($c_p = 10^{-12}$, $c_p = 10^{-11}$) is 34.9% (36.6%, 71.8%) higher than the analytical solution (49.35) in [76] and 14.1% (15.5%, 45.3%) higher than the benchmark (58.35) in [37]. This is expected, as the topology space for the tetragonal unit cell description is the most limited of this study. It can reproduce the same unit cell topology as in [37], but it lacks the possibility to tune the directionality by adjusting the widths of each beam in a unit cell. Moreover, in [77] it was shown that the optimal orientation of an orthotropic material – like the tetragonal lattice (see Figure 3) – aligns with the principal stress directions. Here, α governs the unit cell orientation and indeed aligns beams with the principle stress directions. One may argue that this knowledge could be used in the optimization process. However, when the other RUC parameters (β , γ , and λ) are subject to optimization, $\alpha = 0$ does not necessarily point in the direction of highest stiffness (see Figure 3). In the following sections we will study the influence of changing orthotropy through changes of β and γ .

Discrete lattice

Following the projection approach described in Section 2.4, we construct the spatially-variant tetragonal lattice from the design variable fields in Figure 19 with different length scales μ . Examples are presented in Figure 9.

To evaluate the performance of the projection method, we calculate the compliance of the discrete lattice (cf. (24)) subjected to the boundary value problem depicted in Figure 4b. In Figure 10 we compare the discrete compliance \mathcal{C}_D to the previously obtained continuum compliance \mathcal{C}_C at different regularization intensities. Note that at a length scale of $\mu = 1/320$ the lattice contains more than 200,000 elements. Direct optimization of such high-resolution discrete structures would be very time-demanding, while the desired resolution follows (almost) for free from this multiscale approach (especially since changing the length scale μ does not require solving a new topology optimization problem but is merely a change in postprocessing).

The discrete compliance converges towards the continuum approximation for all cases. Depending on the regularization strength, the projected lattice compliance is within 30% of the optimization result for a coarse length scale of $\mu \approx 1/80$ at $c_p = 10^{-10}$, $\mu \approx 100$ at $c_p = 10^{-11}$, and within 20% of the optimization result for a length scale of $\mu \approx 1/150$ at $c_p = 10^{-10}$, and $\mu \approx 1/170$ at $c_p = 10^{-11}$. For the lowest regularization ($c_p = 10^{-13}$), the discrete compliance is still $> 7\%$ higher for the highest considered resolution ($\mu = 1/320$).

The convergence behavior indicates that – for arbitrary regularization – the discrete compliance will ultimately near the continuum compliance when the length scale approaches zero ($\mu \rightarrow 0$); a small offset is expected to stem from the inevitable differences in both clamping and loading conditions between the formulations of the continuum and the discrete problem (see Figure 4a and Figure 4b).

In summary, optimization of the tetragonal-lattice cantilever beam reached minimized compliance values close to those of comparable studies in the literature – but still above the reported minima. This is attributed to a lack of directional stiffness tunability in the tetragonal RUC definition and our choice of λ . Therefore, we proceed to enrich the truss design space by considering the orthorhombic lattice family.

4.2 Orthorhombic lattice family

In addition to tailoring the local unit cell orientation through angle α as for the tetragonal lattices in Section 4.1, the orthorhombic lattice family (see Table 1) allows us to tune the anisotropy of the lattice through design variable γ , as shown in Figure 3. As before, we first discuss the continuum solution, before demonstrating discrete lattices.

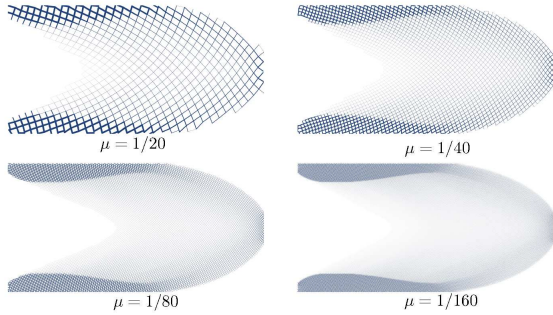


Figure 9: Tetragonal lattice cantilever beam at different length scales for $c_p = 10^{-12}$. For large values of μ , the structure resembles gradually the density field in Figure 19. At $\mu = 1/160$ the lattice consists of more than 120,000 elements.

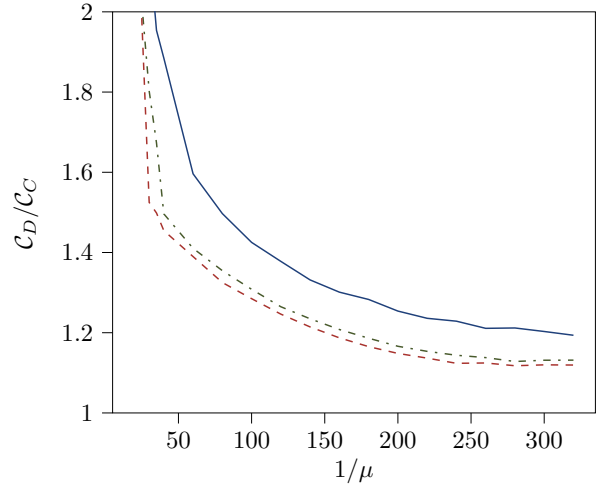


Figure 10: Convergence of the discrete compliance C_D to the continuum approximation C_C for regularization constants $c_p = 10^{-13}$ (solid, blue), $c_p = 10^{-12}$ (dash-dotted, green), and $c_p = 10^{-11}$ (dashed, red).

Continuum

Analogous to Section 4.1, we solve the optimization problem (10), now subjected to orthorhombic RUC constraints (see Table 1), using a continuum mesh of 400x200 bilinear elements. The resulting design variables for regularization constants $c_p = \{10^{-11}, 10^{-12}, 10^{-13}\}$ are presented in Figure 20. Examples are shown in Figure 11. The corresponding compliance values are included in Table 2.

In comparison to the tetragonal lattice, the compliance is up to 7% lower. Comparing to [37] (where no local volume constraint was used), the result at $c_p = 10^{-13}$ is within 6% difference, which is notable given the constraints on local volume fraction ($\bar{\rho}(\mathbf{X}) \leq 0.5$) shown in Table 1.

These results are promising, but they should be interpreted with caution, as some of the beams in the design become relatively thick (as a consequence of high local densities). This stretches the beam slenderness assumption. We refer to A for a detailed study of suitable beam slenderness ratios in compliance with the chosen Timoshenko-Ehrenfest beam model. If we allow for relatively high local densities, then (as shown in A.2) we accept local beam stiffness overpredictions of around 10%. This may result in potentially underestimated structural compliance values. As we are primarily presenting an optimization framework, where homogenization and RUC definition is interchangeable, respectively, we here accept these uncertainties.

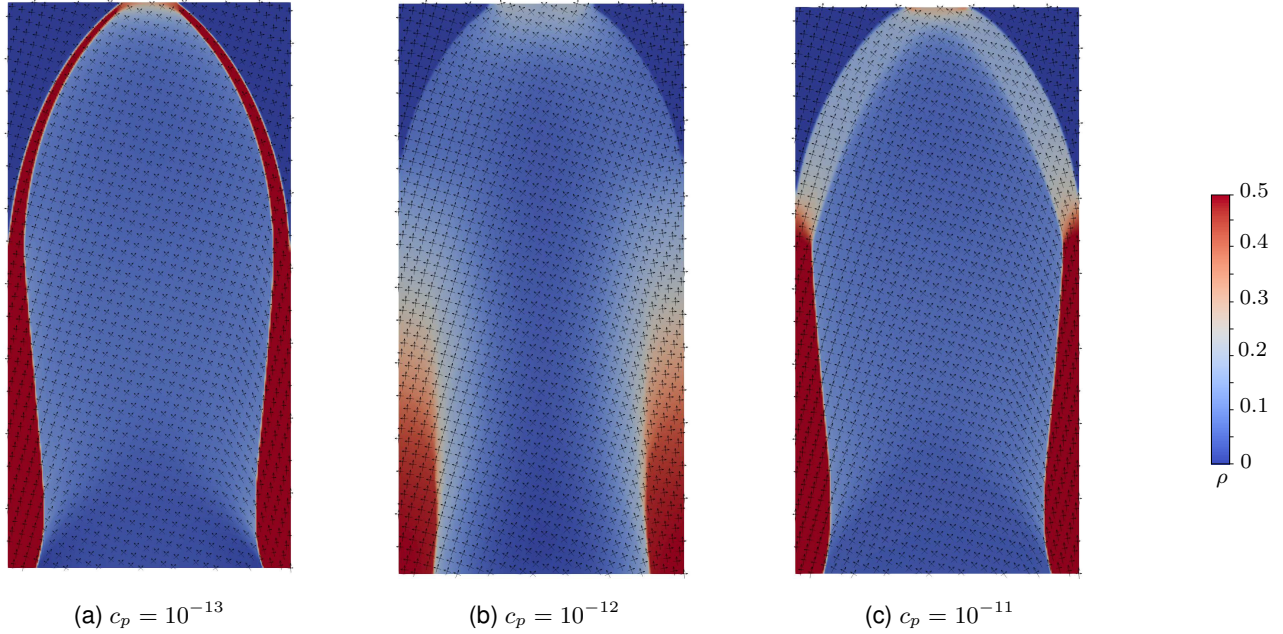


Figure 11: Optimized orthorhombic-lattice cantilever beam for different regularization constants. Local Bravais bases are indicated by arrows, and the density is shown by the color code. The arrows are scaled and shown at selected locations for readability. Resolution: 400x200 elements. All plots are rotated by 90° . Full design variable fields can be found in [Figure 20](#).

Discrete lattice

Analogous to the tetragonal lattice, we project the design variable fields presented in [Figure 20](#) onto different finite scales. Results are shown in [Figure 12](#). As the α -fields in [Figure 11](#) indicated, the projections are similar in orientation to the tetragonal case. The anisotropy of the orthorhombic lattice compared to the tetragonal lattice is more pronounced but equal in directionality (see [Figure 3](#)). In [77] it was shown that the optimal orientation of an orthotropic composite coincides with the principal stress directions. Therefore for similar orthotropic directionality the orientation must be same.

In addition, the free design variable γ allows to pronounce the directionality which is strongly utilized towards the supports, where the principle stresses are high. Results indicate that a larger range for γ , allowing for even more strongly pronounced directionality, would allow for further minimization of the compliance. However, a RUC that spans more space in one direction than in the other also requires smaller length scales to approach the continuum compliance. Furthermore, the approximation concerns regarding the chosen homogenization approach based on slender beams (discussed in [A](#)) increase with decreasing slenderness. As a trade-off we hence choose to restrict γ to the given interval ($0.5 \leq \gamma \leq 2$).

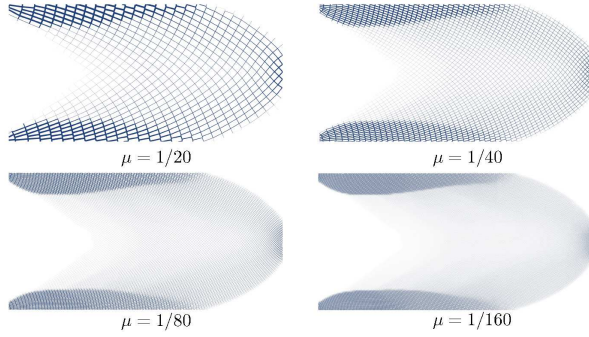


Figure 12: Orthorhombic-lattice cantilever beam at different length scales μ for $c_p = 10^{-12}$.

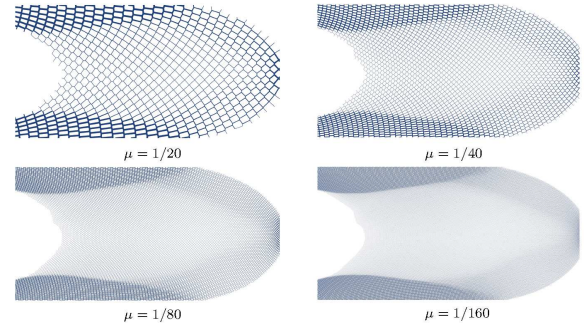


Figure 13: Monoclinic-lattice cantilever beam at different length scales μ for $c_p = 10^{-12}$.

4.3 Monoclinic lattice family

In an ultimate step, we enrich the set of design variables ψ by additionally allowing the parameter β to be optimized (see Table 1) and study its influence on the truss design and on the effective compliance. β not only pronounces the orthotropy (in addition to γ), but it also changes the topology of the elastic surface and introduces asymmetry (see Figure 3).

Continuum

Analogous to the previous lattice families, we solve the optimization problem (10), subjected to the monoclinic RUC constraints of Table 1, on a continuum mesh of 400x200 bilinear elements. The optimized design variable fields for moderate regularization constants $c_p = \{10^{-11}, 10^{-12}\}$ are summarized in Figure 21 and Figure 22. Examples are shown in Figure 14. Both configurations emerge from the orthorhombic initial guess. The resulting compliance values are, again, included in Table 2.

In terms of the compliance, the optimized monoclinic lattice performs worse than the optimized orthorhombic and tetragonal lattices when starting from homogeneous initial conditions. By contrast, when using the results from the orthorhombic lattice optimizations as an initial guess, all design variables, including the monoclinic design parameter β , remain almost unchanged and hence the same compliance is attained. The additional design parameter hence worsens the challenge of finding a good initial guess, since more local minima of the optimization problem arise and the gradient-based optimization approach converges into the closest to the initial guess. Therefore, no solution with better performance than the orthorhombic lattice family could be found. In fact, some of the local minima can be higher than those of the more constrained orthorhombic lattice (cf. Table 2). This finding is in line with previous studies (e.g. [78] and [74]), which suggested that the orthorhombic lattice family is performing close to theoretical limits. The

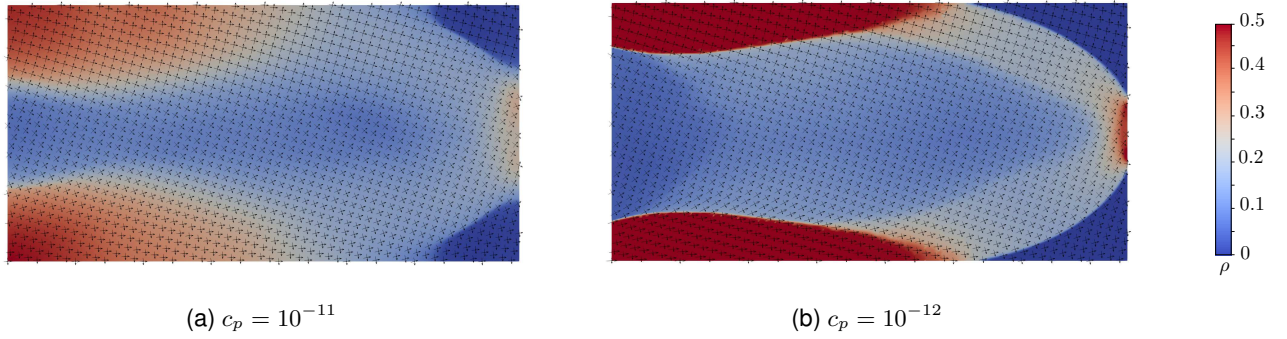


Figure 14: Monoclinic-lattice cantilever beam for different regularization values. Local Bravais bases are indicated by arrows, and the density is shown by the color code. The arrows are scaled and shown at selected locations for readability. Resolution: 400x200 elements. Full design variable fields can be found in [Figure 21](#).

monoclinic lattice family includes these results and, in principle, better informed initial guesses may lead to an improvement in terms of the global compliance lower than the presented one.

Discrete

The projections of the design variable fields in [Figure 21](#) onto different finite scales are shown in [Figure 13](#). The resulting lattice has a slight asymmetry, due to the asymmetric effective properties of monoclinic RUCs (see [Figure 3](#)) and shows different underlying RUC topologies.

The additional design parameter β introduces asymmetry in the RUC anisotropy. This anisotropy reflects in non-rectangular RUCs in the discrete projection and different orientations of the RUCs in comparison to the tetragonal and orthorhombic lattices. The monoclinic lattice family hence shows the most complex lattice architecture yields higher compliance values than previous results.

5 CONCLUSION

Cellular materials show enormous promise as light-weight materials spanning a wide mechanical property space. While the large design freedom allows for target-specific structural integration of spatially variant microstructures, it also poses a challenging inverse-design problem with respect to computational costs and manufacturability.

We presented a two-scale topology optimization scheme for complex macroscale boundary value problems, which guarantees compatible and manufacturable networks of spatially-variant cellular networks. The approach leverages crystallographic principles for continuous and generic unit cell definitions in arbitrary dimensions (here illustrated, without loss of generality, in 2D). The approach is suitable for a wide range of

microscale constitutive descriptions, including, e.g., analytical, numerical, or ML-based constitutive laws as well as tabulated material data. We here explored an FE²-type numerical homogenization approach, which derives the effective constitutive response from a discrete structural unit cell on the microscale.

We demonstrated the framework by optimizing spatially-variant trusses in 2D for minimum compliance. A semi-analytical homogenized continuum model allowed for computationally efficient structural optimization on a regular laptop, while providing architectures of high resolution. The assumptions intrinsic in the underlying slender-beam theory put constraints on the beam slenderness and hence on the volume density of the RUC. While the Timoshenko-Ehrenfest beam theory has proven to accurately represent beam behavior at low slenderness, the nodal joints between beams introduce errors. As shown in the Appendix, we investigated the expected resulting error and expect maximum errors of ca. 10% for local relative density values up to 50%. Even with the imposed constraints, the minimized compliance was within 6% of the comparable (unconstrained) benchmark in [37].

In general, we observed a competition between the regularization of the continuous design variable fields and the length scale of the finite-scale discrete truss in line with the assumption of a separation of scales. For low regularization values, where usually best optimization results are obtained, a very fine length scale is required to ensure similar performance of the discrete lattice versus the continuum prediction. Conversely, if a coarse length scale is required (e.g., by manufacturing constraints), stronger regularization is needed to ensure consistency between the final discrete structure and the continuum approximation.

While the large design freedom in cellular materials offers an enormous mechanical property space, its nonconvex nature requires special attention in topology optimization. Especially, when utilizing a multi-variable parametrization, the optimization is prone to identify only local minima based on the initial guess, which can be far off from the global minimum. To avoid unfavorable local minima, it can be beneficial to explore the design space by optimizing distinct sets of design variables separately before optimizing the whole set. In the case of the monoclinic truss lattice family, we observed that optimization of the (more restricted) orthorhombic lattice family produced better results. We could only reproduce these results with the monoclinic lattice when using the output of the orthorhombic lattice optimization as the initial guess.

Future possible directions include the exploration of different unit cell definitions in 2D and 3D and their use for different target objectives. A natural extension with the utilized nonlinear homogenization framework is the exploration of finite deformations, e.g., for soft robotic applications.

ACKNOWLEDGEMENTS

O.S. was supported by the Villum Foundation through the Villum Investigator Project “InnoTop”.

REFERENCES

- [1] Gibson, L. J., and Ashby, M. F., 1997, *Cellular Solids: Structure and Properties*, 2 ed. Cambridge Solid State Science Series. Cambridge University Press.
- [2] Ashby, M. F., 2016, *Materials Selection in Mechanical Design* Butterworth-Heinemann, Sept. Google-Books-ID: K4h4CgAAQBAJ.
- [3] Evans, A. G., Hutchinson, J. W., Fleck, N. A., Ashby, M. F., and Wadley, H. N. G., 2001, “The topological design of multifunctional cellular metals,” *Progress in Materials Science*, **46**(3), Jan., pp. 309–327.
- [4] Lakes, R., 1993, “Materials with structural hierarchy,” *Nature*, **361**(6412), Feb., pp. 511–515.
- [5] Zheng, X., Lee, H., Weisgraber, T. H., Shusteff, M., DeOtte, J., Duoss, E. B., Kuntz, J. D., Biener, M. M., Ge, Q., Jackson, J. A., Kucheyev, S. O., Fang, N. X., and Spadaccini, C. M., 2014, “Ultralight, ultrastiff mechanical metamaterials,” *Science*, **344**(6190), June, pp. 1373–1377.
- [6] Meza, L. R., Zelhofer, A. J., Clarke, N., Mateos, A. J., Kochmann, D. M., and Greer, J. R., 2015, “Resilient 3d hierarchical architected metamaterials,” *Proceedings of the National Academy of Sciences*, **112**(37), Sept., pp. 11502–11507.
- [7] Fleck, N. A., Deshpande, V. S., and Ashby, M. F., 2010, “Micro-architected materials: past, present and future,” *Proceedings of the Royal Society A: Mathematical, Physical and Engineering Sciences*, **466**(2121), Sept., pp. 2495–2516.
- [8] Schaedler, T. A., and Carter, W. B., 2016, “Architected Cellular Materials,” *Annual Review of Materials Research*, **46**(1), July, pp. 187–210.
- [9] Valdevit, L., Bertoldi, K., Guest, J., and Spadaccini, C., 2018, “Architected materials: Synthesis, characterization, modeling, and optimal design,” *Journal of Materials Research*, **33**(3), Feb., pp. 241–246.
- [10] Schaedler, T. A., Jacobsen, A. J., Torrents, A., Sorensen, A. E., Lian, J., Greer, J. R., Valdevit, L., and Carter, W. B., 2011, “Ultralight Metallic Microlattices,” *Science*, **334**(6058), Nov., pp. 962–965.
- [11] Lakes, R., 1987, “Foam Structures with a Negative Poisson’s Ratio,” *Science (New York, N.Y.)*, **235**(4792), Feb., pp. 1038–1040.
- [12] Sigmund, O., 1994, “Materials with prescribed constitutive parameters: An inverse homogenization problem,” *International Journal of Solids and Structures*, **31**(17), Sept., pp. 2313–2329.

- [13] Milton, G. W., and Cherkaev, A. V., 1995, "Which Elasticity Tensors are Realizable?," *Journal of Engineering Materials and Technology*, **117**(4), 10, pp. 483–493.
- [14] Huang, X., Radman, A., and Xie, Y. M., 2011, "Topological design of microstructures of cellular materials for maximum bulk or shear modulus," *Computational Materials Science*, **50**(6), Apr., pp. 1861–1870.
- [15] Bückmann, T., Thiel, M., Kadic, M., Schittny, R., and Wegener, M., 2014, "An elasto-mechanical unfeelability cloak made of pentamode metamaterials," *Nature Communications*, **5**(1), p. 4130.
- [16] Wadley, H., Dharmasena, K., Chen, Y., Dudt, P., Knight, D., Charette, R., and Kiddy, K., 2008, "Compressive response of multilayered pyramidal lattices during underwater shock loading," *International Journal of Impact Engineering*, **35**(9), Sept., pp. 1102–1114.
- [17] Hussein, M. I., Leamy, M. J., and Ruzzene, M., 2014, "Dynamics of Phononic Materials and Structures: Historical Origins, Recent Progress, and Future Outlook," *Applied Mechanics Reviews*, **66**(4), 05 040802.
- [18] Zelhofer, A. J., and Kochmann, D. M., 2017, "On acoustic wave beaming in two-dimensional structural lattices," *International Journal of Solids and Structures*, **115–116**, pp. 248–269.
- [19] Clausen, A., Wang, F., Jensen, J. S., Sigmund, O., and Lewis, J. A., 2015, "Topology Optimized Architectures with Programmable Poisson's Ratio over Large Deformations," *Advanced Materials*, **27**(37), pp. 5523–5527 _eprint: <https://onlinelibrary.wiley.com/doi/pdf/10.1002/adma.201502485>.
- [20] Symons, D. D., and Fleck, N. A., 2008, "The Imperfection Sensitivity of Isotropic Two-Dimensional Elastic Lattices," *Journal of Applied Mechanics*, **75**(5), Sept.
- [21] Montemayor, L. C., Wong, W. H., Zhang, Y.-W., and Greer, J. R., 2016, "Insensitivity to Flaws Leads to Damage Tolerance in Brittle Architected Meta-Materials," *Scientific Reports*, **6**, Feb., p. 20570.
- [22] Thomsen, C. R., Wang, F., and Sigmund, O., 2018, "Buckling strength topology optimization of 2D periodic materials based on linearized bifurcation analysis," *Computer Methods in Applied Mechanics and Engineering*, **339**, Sept., pp. 115–136.
- [23] Pham, M.-S., Liu, C., Todd, I., and Lertthanasarn, J., 2019, "Damage-tolerant architected materials inspired by crystal microstructure," *Nature*, **565**(7739), Jan., pp. 305–311.
- [24] Cadman, J. E., Zhou, S., Chen, Y., and Li, Q., 2013, "On design of multi-functional microstructural materials," *Journal of Materials Science*, **48**(1), Jan., pp. 51–66.
- [25] Osanov, M., and Guest, J. K., 2016, "Topology Optimization for Architected Materials Design," *Annual Review of Materials Research*, **46**(1), pp. 211–233.
- [26] Jain, A., Ong, S. P., Hautier, G., Chen, W., Richards, W. D., Dacek, S., Cholia, S., Gunter, D., Skinner,

- D., Ceder, G., and Persson, K. A., 2013, "Commentary: The Materials Project: A materials genome approach to accelerating materials innovation," *APL Materials*, **1**(1), July, p. 011002.
- [27] Sigmund, O., 2000, "A new class of extremal composites," *Journal of the Mechanics and Physics of Solids*, **48**(2), Feb., pp. 397–428.
- [28] Berger, J. B., Wadley, H. N. G., and McMeeking, R. M., 2017, "Mechanical metamaterials at the theoretical limit of isotropic elastic stiffness," *Nature*, **543**, Feb, pp. 533 EP –.
- [29] Sigmund, O., and Jensen, J. S., 2003, "Systematic design of phononic band-gap materials and structures by topology optimization," *Philosophical Transactions of the Royal Society of London A: Mathematical, Physical and Engineering Sciences*, **361**(1806), May, pp. 1001–1019.
- [30] Bilal, O. R., and Hussein, M. I., 2011, "Ultrawide phononic band gap for combined in-plane and out-of-plane waves," *Physical Review E*, **84**(6), Dec. arXiv: 1111.1457.
- [31] Pasini, D., and Guest, J. K., 2019, "Imperfect architected materials: Mechanics and topology optimization," *MRS Bulletin*, **44**(10), p. 766–772.
- [32] Kochmann, D. M., Hopkins, J. B., and Valdevit, L., 2019, "Multiscale modeling and optimization of the mechanics of hierarchical metamaterials," *MRS Bulletin*, **44**(10), p. 773–781.
- [33] Aage, N., Andreassen, E., Lazarov, B. S., and Sigmund, O., 2017, "Giga-voxel computational morphogenesis for structural design," *Nature*, **550**(7674), Oct., pp. 84–86.
- [34] Lazarov, B., Wang, F., and Sigmund, O., 2016, "Length scale and manufacturability in density-based topology optimization," *Archives of Applied Mechanics*, **86**, pp. 189–218.
- [35] Milton, G. W., 1986, "Modelling the Properties of Composites by Laminates," In *Homogenization and Effective Moduli of Materials and Media*, J. L. Ericksen, D. Kinderlehrer, R. Kohn, and J.-L. Lions, eds., The IMA Volumes in Mathematics and its Applications, Springer New York, pp. 150–174.
- [36] Träff, E., Sigmund, O., and Groen, J., 2018, "Simple single-scale microstructures based on optimal rank-3 laminates," *Structural and Multidisciplinary Optimization*, **59**, pp. 1021–1031.
- [37] Groen, J. P., and Sigmund, O., 2018, "Homogenization-based topology optimization for high-resolution manufacturable microstructures," *International Journal for Numerical Methods in Engineering*, **113**(8), pp. 1148–1163.
- [38] Rodrigues, H., Guedes, J., and Bendsoe, M., 2002, "Hierarchical optimization of material and structure," *Structural and Multidisciplinary Optimization*, **24**(1), Aug., pp. 1–10.
- [39] Coelho, P. G., Fernandes, P. R., Guedes, J. M., and Rodrigues, H. C., 2008, "A hierarchical model for concurrent material and topology optimisation of three-dimensional structures," *Structural and Multi-*

- disciplinary Optimization*, **35**(2), Feb., pp. 107–115.
- [40] Sivapuram, R., Dunning, P. D., and Kim, H. A., 2016, “Simultaneous material and structural optimization by multiscale topology optimization,” *Structural and Multidisciplinary Optimization*, **54**(5), Nov., pp. 1267–1281.
- [41] Wang, Y., Xu, H., and Pasini, D., 2017, “Multiscale isogeometric topology optimization for lattice materials,” *Computer Methods in Applied Mechanics and Engineering*, **316**, Apr., pp. 568–585.
- [42] Xia, L., and Breitkopf, P., 2014, “Concurrent topology optimization design of material and structure within FE2 nonlinear multiscale analysis framework,” *Computer Methods in Applied Mechanics and Engineering*, **278**, Aug., pp. 524–542.
- [43] Khanoki, S. A., and Pasini, D., 2012, “Multiscale design and multiobjective optimization of orthopedic hip implants with functionally graded cellular material,” *Journal of biomechanical engineering*, **134**(3), p. 031004.
- [44] Wang, Y., Arabnejad, S., Tanzer, M., and Pasini, D., 2018, “Hip Implant Design With Three-Dimensional Porous Architecture of Optimized Graded Density,” *Journal of Mechanical Design*, **140**(11), Nov.
- [45] Schumacher, C., Bickel, B., Rys, J., Marschner, S., Daraio, C., and Gross, M., 2015, “Microstructures to control elasticity in 3d printing,” *ACM Transactions on Graphics*, **34**(4), July, pp. 136:1–136:13.
- [46] Chen, D., Skouras, M., Zhu, B., and Matusik, W., 2018, “Computational discovery of extremal microstructure families,” *Science Advances*, **4**(1), Jan., p. eaao7005.
- [47] Radman, A., Huang, X., and Xie, Y. M., 2013, “Topology optimization of functionally graded cellular materials,” *Journal of Materials Science*, **48**(4), Feb., pp. 1503–1510.
- [48] Zhu, B., Skouras, M., Chen, D., and Matusik, W., 2017, “Two-Scale Topology Optimization with Microstructures,” *arXiv:1706.03189 [cs]*, June arXiv: 1706.03189.
- [49] Du, Z., Zhou, X.-Y., Picelli, R., and Kim, H. A., 2018, “Connecting Microstructures for Multiscale Topology Optimization With Connectivity Index Constraints,” *Journal of Mechanical Design*, **140**(11), Nov.
- [50] Panetta, J., Zhou, Q., Malomo, L., Pietroni, N., Cignoni, P., and Zorin, D., 2015, “Elastic textures for additive fabrication,” *ACM Transactions on Graphics*, **34**(4), July, pp. 135:1–135:12.
- [51] Schury, F., Stingl, M., and Wein, F., 2012, “Efficient Two-Scale Optimization of Manufacturable Graded Structures,” *SIAM Journal on Scientific Computing*, **34**(6), Jan., pp. B711–B733.
- [52] Sanders, E. D., Aguiló, M. A., and Paulino, G. H., 2018, “Multi-material continuum topology optimization with arbitrary volume and mass constraints,” *Computer Methods in Applied Mechanics and*

Engineering, **340**, Oct., pp. 798–823.

- [53] Zhang, X. S., Chi, H., and Paulino, G. H., 2020, “Adaptive multi-material topology optimization with hyperelastic materials under large deformations: A virtual element approach,” *Computer Methods in Applied Mechanics and Engineering*, **370**, Oct., p. 112976.
- [54] Sanders, E. D., Pereira, A., and Paulino, G. H., 2021, “Optimal and continuous multilattice embedding,” *Science Advances*, Apr. Publisher: American Association for the Advancement of Science.
- [55] Dunning, P. D., Brampton, C. J., and Kim, H. A., 2015, “Simultaneous optimisation of structural topology and material grading using level set method,” *Materials Science and Technology*, **31**(8), June, pp. 884–894.
- [56] Greifstein, J., and Stingl, M., 2016, “Simultaneous parametric material and topology optimization with constrained material grading,” *Structural and Multidisciplinary Optimization*, **54**(4), Oct., pp. 985–998.
- [57] Allaire, G., Geoffroy-Donders, P., and Pantz, O., 2019, “Topology optimization of modulated and oriented periodic microstructures by the homogenization method,” *Computers & Mathematics with Applications*, **78**(7), Oct., pp. 2197–2229.
- [58] Xu, L., and Qian, Z., 2021, “Topology optimization and de-homogenization of graded lattice structures based on asymptotic homogenization,” *Composite Structures*, **277**, Dec., p. 114633.
- [59] Kumar, T., and Suresh, K., 2020, “A density-and-strain-based K-clustering approach to microstructural topology optimization,” *Structural and Multidisciplinary Optimization*, **61**(4), Apr., pp. 1399–1415.
- [60] Pantz, O., and Trabelsi, K., 2008, “A Post-Treatment of the Homogenization Method for Shape Optimization,” *SIAM Journal on Control and Optimization*, Mar.
- [61] Wu, J., Wang, W., and Gao, X., 2019, “Design and Optimization of Conforming Lattice Structures,” *IEEE Transactions on Visualization and Computer Graphics*, pp. 1–1 arXiv: 1905.02902.
- [62] Wu, J., Sigmund, O., and Groen, J. P., 2021, “Topology optimization of multi-scale structures: a review,” *Structural and Multidisciplinary Optimization*, **63**(3), Mar., pp. 1455–1480.
- [63] Glaesener, R. N., Lestringant, C., Telgen, B., and Kochmann, D. M., 2019, “Continuum models for stretching- and bending-dominated periodic trusses undergoing finite deformations,” *International Journal of Solids and Structures*, **171**, Oct., pp. 117–134.
- [64] Rumpf, R. C., and Pazos, J., 2012, “Synthesis of spatially variant lattices,” *Optics Express*, **20**(14), July, pp. 15263–15274.
- [65] Groen, J., Stutz, F., Aage, N., Bærentzen, J., and Sigmund, O., 2020, “De-homogenization of optimal

- multi-scale 3d topologies,” *Computer Methods in Applied Mechanics and Engineering*, **364**, p. 112979.
- [66] Xue, D., Zhu, Y., Li, S., Liu, C., Zhang, W., and Guo, X., 2020, “On speeding up an asymptotic-analysis-based homogenisation scheme for designing gradient porous structured materials using a zoning strategy,” *Structural and Multidisciplinary Optimization*, pp. 1–17.
- [67] Geoffroy-Donders, P., Allaire, G., and Pantz, O., 2020, “3-d topology optimization of modulated and oriented periodic microstructures by the homogenization method,” *Journal of Computational Physics*, **401**, p. 108994.
- [68] Kittel, C., 1986, *Introduction to solid state physics*, 8th ed. Wiley.
- [69] Bravais, A., 1850, “Mémoire sur les systèmes formés par des points distribués régulièrement sur un plan ou dans l’espace,” *J. École polytechnique*, **19**, pp. 1—128.
- [70] Wigner, E., and Seitz, F., 1933, “On the Constitution of Metallic Sodium,” *Physical Review*, **43**(10), May, pp. 804–810.
- [71] Crisfield, M. A., 1990, “A consistent co-rotational formulation for non-linear, three-dimensional, beam-elements,” *Computer methods in applied mechanics and engineering*, **81**(2), pp. 131–150.
- [72] Borrvall, T., 2001, “Topology optimization of elastic continua using restriction,” *Archives of Computational Methods in Engineering*, **8**(4), Dec., pp. 351–385.
- [73] Svanberg, K., 1987, “The method of moving asymptotes—a new method for structural optimization,” *International Journal for Numerical Methods in Engineering*, **24**(2), pp. 359–373.
- [74] Sigmund, O., Aage, N., and Andreassen, E., 2016, “On the (non-)optimality of Michell structures,” *Structural and Multidisciplinary Optimization*, **54**(2), Aug., pp. 361–373.
- [75] Sigmund, O., and Petersson, J., 1998, “Numerical instabilities in topology optimization: A survey on procedures dealing with checkerboards, mesh-dependencies and local minima,” *Structural Optimization*, **16**(1), pp. 68–75.
- [76] Chan, A. S. L., 1962, “The Design of Michell Optimum Structures,” p. 43.
- [77] Pedersen, P., 1989, “On optimal orientation of orthotropic materials,” *Structural optimization*, **1**(2), June, pp. 101–106.
- [78] Groen, J. P., Wu, J., and Sigmund, O., 2019, “Homogenization-based stiffness optimization and projection of 2d coated structures with orthotropic infill,” *Computer Methods in Applied Mechanics and Engineering*, **349**, June, pp. 722–742.

A HOMOGENIZATION BASED ON BEAMS

The utilized homogenization approach of [63] is based on modeling the RUC by beam elements, which imply rigid (welded) connections at junctions. Beam theory is generally deemed applicable whenever the length of a beam is much larger than its width, i.e., when the slenderness $L/w \gg 1$. In addition, assuming rigid connections between beams neglects nodal effects such as stress concentrations at nodes or overlaps between connected beams. These assumptions, however, are challenged when modeling RUCs with high volume fractions $\bar{\rho}$, implying relatively thick beams. To evaluate the applicability of the applied homogenization approach, we present in this section a discussion of the influence of the effective RUC density on the approximation of homogenized quantities and ways to extend the applicable range. For all calculations we assume a rectangular beam cross-section with out-of-plane thickness $t = 1$, Young's modulus $E = 1$, Poisson's ration $\nu = 0.3$, and the Timoshenko shear coefficient for rectangular cross-sections $\kappa = 1.2$ (all normalized for simplicity).

A.1 Beam slenderness

As the beam is the smallest building block of the RUC, the exactness of the beam element has primary relevance. Generally well-known beam formulations include the theories of Euler-Bernoulli and Timoshenko-Ehrenfest. To evaluate their accuracy for low slenderness ratios L/w , we evaluate, using both formulations, the strain energy of a 2D cantilever beam of length $L = 1$ and varying thickness w . The beam is clamped at one end and loaded by a constant displacement at the other end. For comparison, we establish a reference by resolving the cantilever beam (20 elements over the width w) with square bilinear finite elements, assuming isotropic linear elasticity under the plane-stress assumption.

A comparison of the strain energy inside the bent cantilever beam is shown in Figure 15. Both beam implementations converge to the exact solution for $L/w \gg 1$. With increasing w/L , Euler-Bernoulli beam theory exceedingly overestimates the strain energy. In contrast, Timoshenko-Ehrenfest beam theory shows significantly better agreement and generally tends to underestimate the strain energy. For $w/L = 0.5$, Euler-Bernoulli beam theory overestimates the energy by roughly 27%, while Timoshenko-Ehrenfest stays within a 5% error margin for the full range of slenderness ratios up to $w = L$.

We conclude that Euler-Bernoulli beam theory is not suited for modeling beams with low slenderness ratio L/w . In contrast, when accepting a maximum error of 5%, Timoshenko-Ehrenfest beam theory is applicable for a wide range of slenderness ratios and even for extreme cases ($w = L$). Therefore, all following discussions (and the truss optimization studies) are based on Timoshenko-Ehrenfest beam theory.

A.2 Node influence

Truss networks consist of many beams that are connected to each other through nodes. While the previous section confirmed the validity of beam theory for an individual beam, we here investigate the influence of nodes on the approximation of homogenized properties using beam elements. Generally, the influence of nodes is neglected when using beam models, assuming a slenderness ratio of $L/w \gg 1$. However, when beams are not slender, or equivalently when the density $\bar{\rho}$ of the RUC is high, the influence of the nodes on the effective mechanical properties cannot be neglected.

In Figure 16, we introduce three variants for approximating the geometry of a RUC with non-slender beams. As in classical beam theory, all variants assume that the node is rigid and hence described well by Timoshenko-Ehrenfest theory. In variant A, beams connect from node centroid to node centroid; beams overlap at nodes (this is the standard approach). In variant B, the overlapping nodes are accounted for by assuming beams whose effective length is not from node centroid to node centroid but the reduced length between nodes without overlapping volumes. Variants A and B present the soft and stiff extremes (lower and upper bounds), respectively. Finally, variant C is a compromise, where the overlap of beams at each node is chosen such that the volume of all beams in a RUC matches the volume fill fraction according to the effective density $\bar{\rho}$, which defines the effective beam length (between those of variants A and B). Note

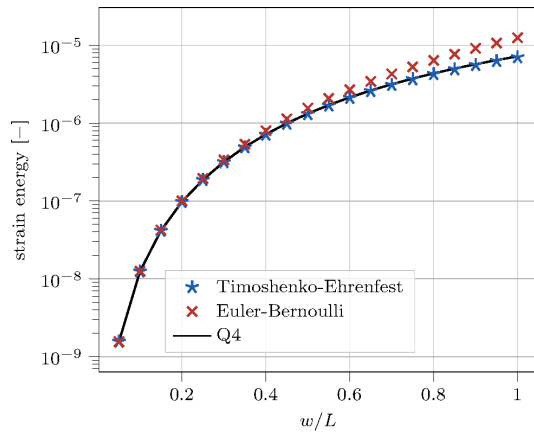


Figure 15: Total strain energy of a cantilever beam (clamped at one end, loaded by a constant deflection at the other end) for varying slenderness w/L . The fully resolved result is shown in black (solid line), compared to results obtained from Timoshenko-Ehrenfest beam theory (blue stars) and Euler-Bernoulli beam theory (red crosses).

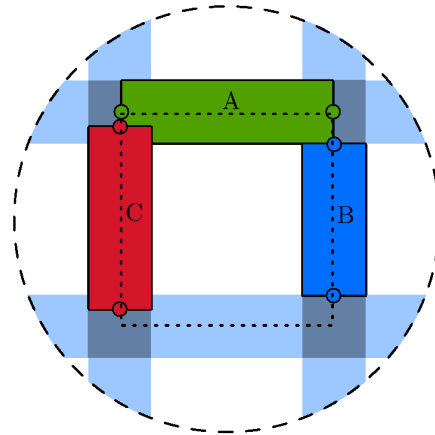


Figure 16: Different node treatments in a square RUC ($\bar{\rho} = 0.5$): variant A ignores the overlap of beams at a node (dark areas) and uses a beam element from node center to node center. In variant B the nodes are assumed rigid and beams have the effective length between nodes without overlap. Variant C is a volume-preserving compromise between variants A and B.

that, when $L/w \gg 1$, all three variants must converge to the same solution.

The influence of the three variants on the effective stiffness is demonstrated for the square and hexagon RUCs, as representatives of stretching- and bending-dominated RUCs, in Figure 17. As a reference, we calculated the effective directional Young's modulus of fully discretized (ref) RUCs, also shown in Figures 17a to 17d, with classical homogenization assuming periodic boundary conditions and linear elasticity under the plane-stress assumption. These reference values are indicated as black solid lines. The directional Young's modulus based on truss homogenization [63] for the three variants A, B, C are shown in green, blue, and red, respectively.

The results confirm that for low effective density (e.g., $\bar{\rho} = 0.1$) all three variants converge to the fully-resolved reference solution. Variant A converges from below, variant B converges from above, and there is no clear trend for variant C. For the large density $\bar{\rho} = 0.5$, the trends are the same, but the deviations are

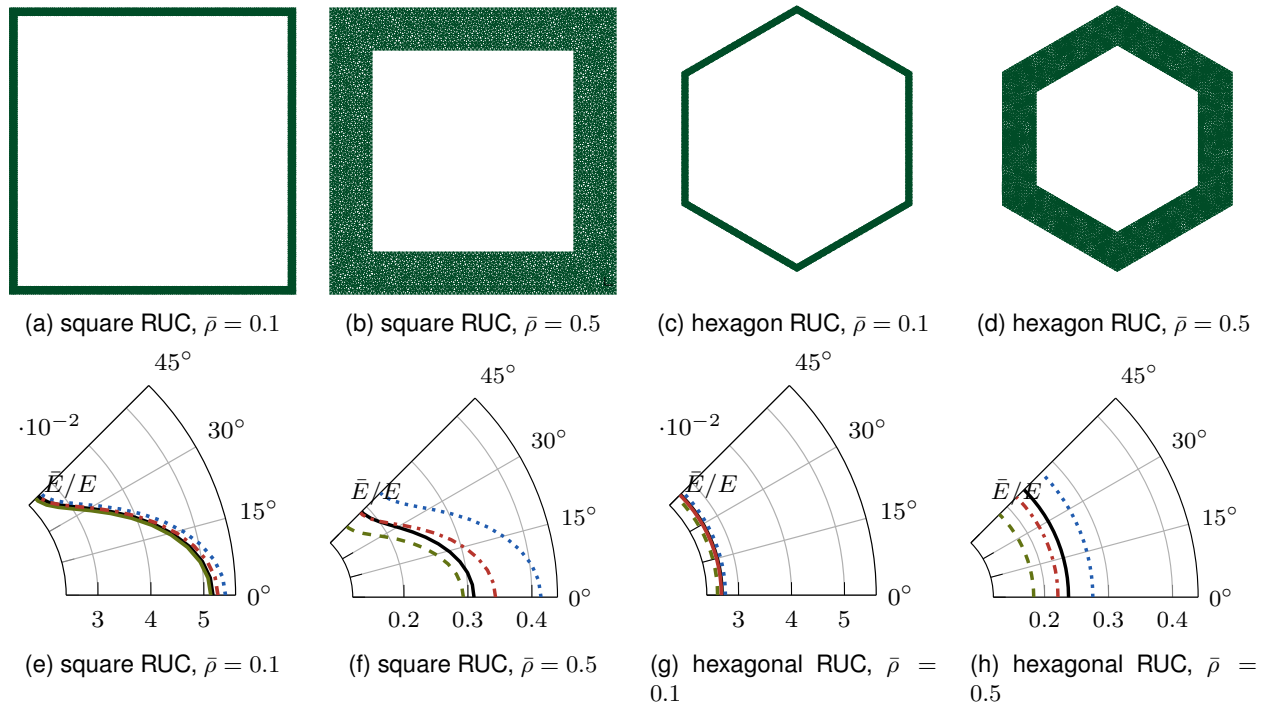


Figure 17: Influence of the node treatment on the effective directional Young's modulus for different effective RUC densities and topologies. Figures 17a to 17d show the CST mesh of the square RUC ($\alpha = 0$, $\beta = \pi/2$, $\gamma = 1$) and hexagonal RUC ($\alpha = 0$, $\beta = \pi/3$, $\gamma = 1$), each for $\bar{\rho} = 0.1$ and $\bar{\rho} = 0.5$. Figures 17e to 17h show the respective directional Young's moduli based on homogenization of the shown RUCs (black solid lines) and obtained from the modified beam representation in variant A, ignoring the overlap at nodes (green dashed lines), assuming rigid nodes in variant B (blue dotted lines), and volume-preserving node overlaps in variant C (red dash-dotted lines). Exploiting symmetry, only half of the first quadrant is shown in each elastic modulus plot.

more severe. Variant A underestimates the directional stiffness of the square RUC by maximally 5%, variants B and C overestimate the directional stiffness by up to 34% and 11%, respectively. For the hexagonal RUC, variant B still overestimates the directional stiffness by 16%, and variants A and C underestimate the stiffness by 23% and 7%, respectively.

The comparison is extended to the full homogenized orthotropic elasticity tensor C of the RUC (having 3×3 components, using Voigt notation in 2D). Results are shown in Figure 18 with the fully discretized reference solution indicated by C^{ref} . As expected, the errors shown in Figure 18a and Figure 18d converge to zero in the limit of low densities $\bar{\rho}$. For $\bar{\rho} = 0.5$ the error of variant B ($> 30\%$) is highest in the square, and variant A shows the largest error in the hexagon ($> 20\%$). For the C_{11} -entry, Figure 18b and Figure 18e) confirm the observations from the directional Young's moduli (cf. Figure 17): with decreasing $\bar{\rho}$, variant A converges from below, variant B from above, and variant C is scattered around the reference values. Lastly, we compare a measure for the shear stiffness in form of invariant $(C_{11} + C_{22})/2 - (C_{12} + 2C_{66})$, as presented by [77]. When the invariant assumes a negative value, the shear stiffness is regarded as relatively high and could indicate artificial shear stiffening. By contrast, a positive value indicates a relatively low shear stiffness. In Figure 18f, we observe a constant zero invariant for the hexagon, whereas the square RUC loses relative shear stiffness with increasing $\bar{\rho}$, as shown in Figure 18c.

A.3 Applicability of beam-based homogenization

We showed in A.1 that the Timoshenko-Ehrenfest beam theory provides accurate results up to low slenderness values (thick beams), so that we deem this model applicable for the homogenization of RUCs with relatively high filling fraction $\bar{\rho}$. In A.2, we observed that the nodes in a RUC can be assumed rigid for relatively low $\bar{\rho}$. However, the error increases drastically for increasing $\bar{\rho}$. Clear trends are observable: Variant A consistently underestimates the reference, while variant B consistently overestimates the effective properties. Variant C lies in between those two bounds. No artificial effects, such as shear stiffening, could be detected.

In conclusion, one must carefully evaluate the acceptable error when choosing to homogenize RUCs with high $\bar{\rho}$ while assuming rigid nodes (as done in this study based on Timoshenko-Ehrenfest beam theory). For this optimization study, we chose to use variant C as a compromise and accept maximum local errors on the order of 10% by allowing for local relative densities $\rho(\mathbf{X})$ up to 50%.

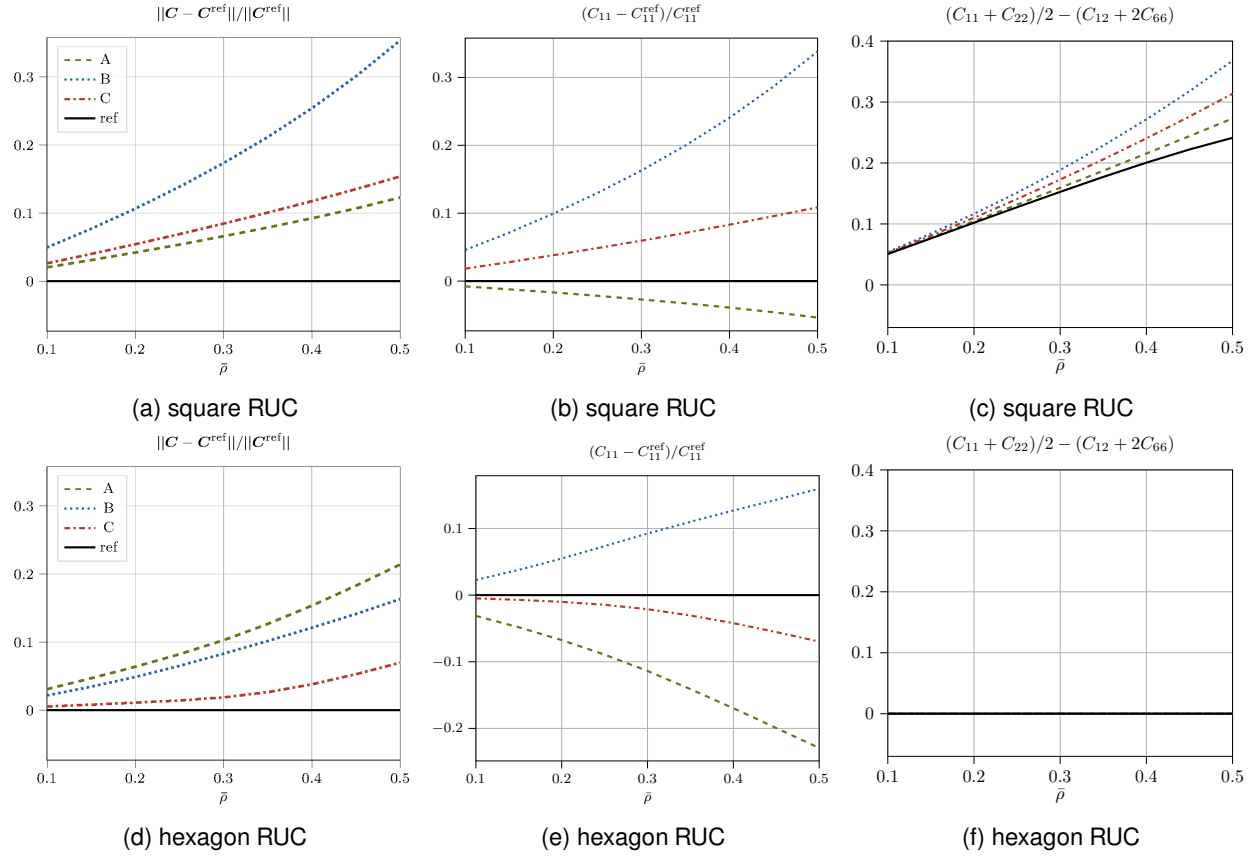


Figure 18: Influence of effective density and node treatment on estimating the elasticity tensor, comparing the results of beam elements of variants A, B, and C to the fully-meshed reference solution (using Voigt notation in 2D for the stiffness tensor components).

B CONTINUUM DESIGN VARIABLE FIELDS

All studied design variable fields are shown in Figures 19, 20 and 21.

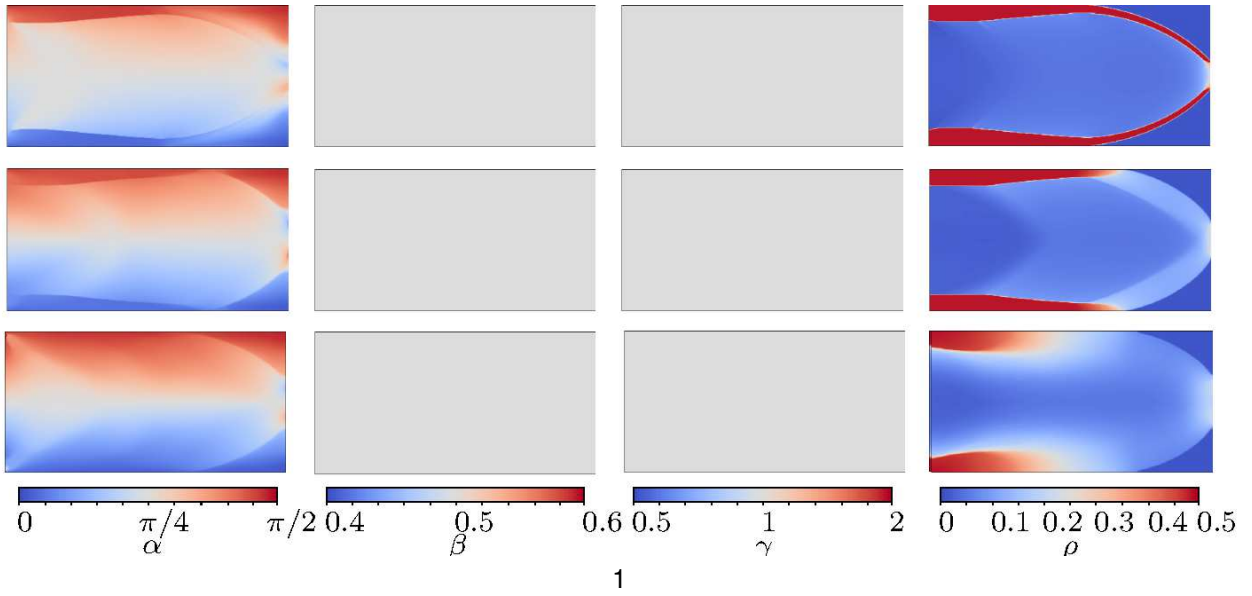


Figure 19: Optimized design variable fields for the tetragonal-lattice cantilever problem, using 400x200 elements. Top: $c_p = 10^{-13}$; middle: 10^{-12} ; bottom: 10^{-11} .

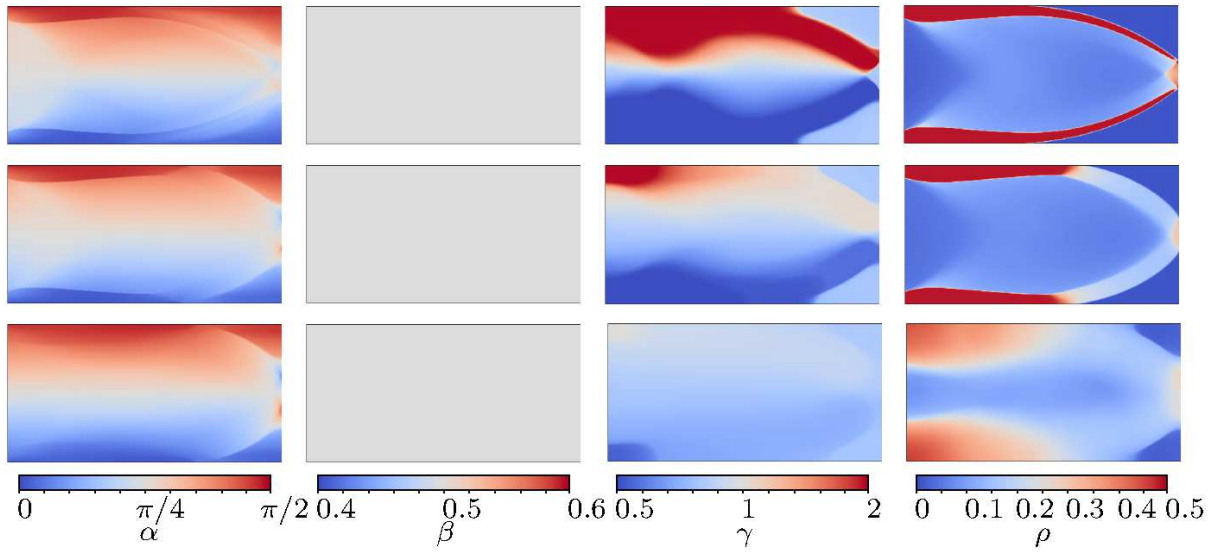


Figure 20: Optimized design variable fields for the orthorhombic-lattice cantilever problem, using 400x200 elements. From top to bottom, $c_p = (10^{-13}, 10^{-12}, 10^{-11})$.

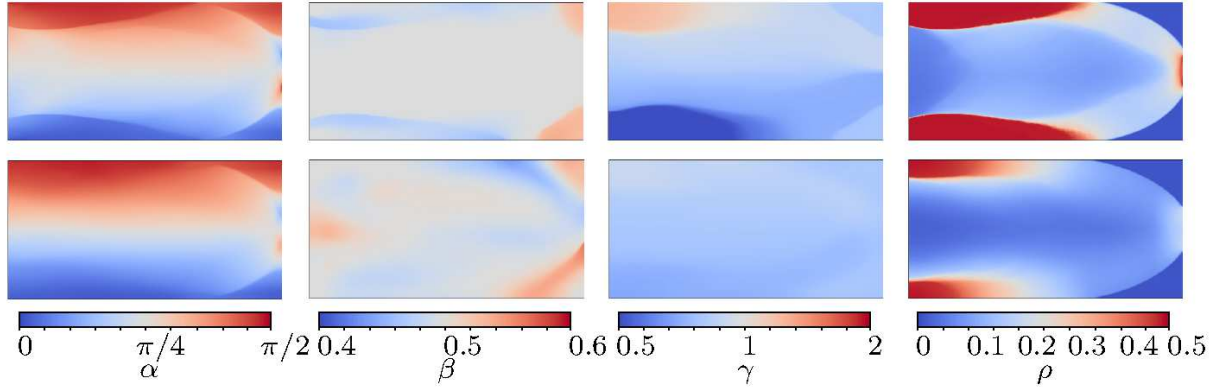


Figure 21: Optimized design variable fields for the monoclinic-lattice cantilever problem, using 400x200 elements and the optimized fields of the for the orthorhombic lattice family as starting guess. From top to bottom, $c_p = (10^{-12}, 10^{-11})$.

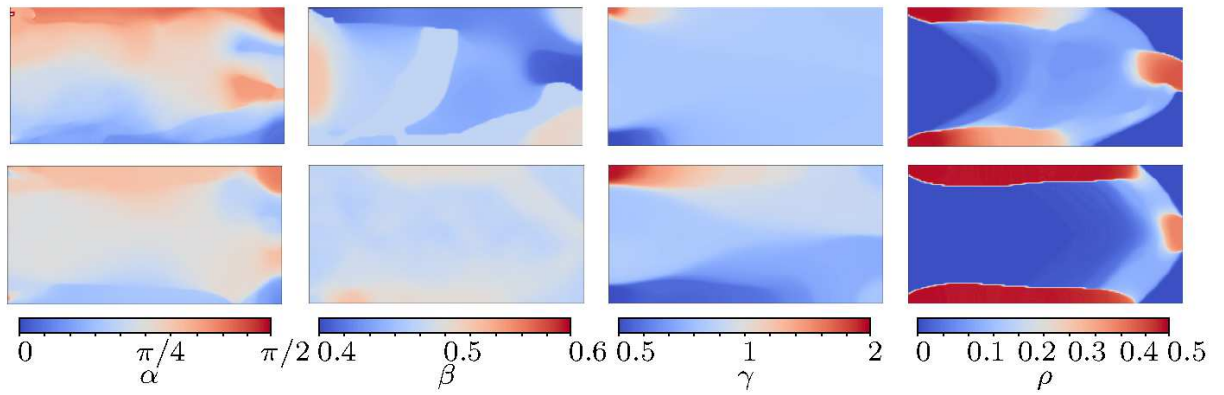


Figure 22: Optimized design variable fields for the monoclinic-lattice cantilever problem, using 400x200 elements and the homogeneous starting guess. From top to bottom, $c_p = (10^{-12}, 10^{-11})$.