Coupling in reflector arrays

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Published in:
IEEE Transactions on Antennas and Propagation

Link to article, DOI:
10.1109/TAP.1968.1139291

Publication date:
1968

Document Version
Publisher's PDF, also known as Version of record

Citation (APA):

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COMMUNICATIONS

This back-scattering cross section will be to the dipoles and propagating along the section for an incident wave polarized parallel normal to the plane containing the dipoles.

The purpose of the present communication is to demonstrate that this is true for a Van Atta reflector consisting of four half-wave dipoles arranged on a line. Some theoretical studies of the influence of coupling in Van Atta reflector arrays have been carried out previously [2]–[4]. In this communication, theoretical results obtained by using the methods described in [2]–[4] will be compared with experimental results. In contrast to previous experimental results [4] which have been presented as normalized, the results described here are absolute. Before the experimental results are described, some theoretical gain for circular and elliptical arrays,” Proc. IEEE (London), vol. 114, pp. 589–594, May 1967.

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Coupling in Reflector Arrays

For many applications, such as echo enhancement and satellite communication, reflectors which have a maximum of reradiation back in the direction of arrival of an incident wave are needed. In 1955, Van Atta [1] proposed a reflector with this property. The reflector consists of antenna elements properly arranged and connected by transmission lines. In order to reduce the space occupied by a reflector array, it is desirable to arrange the array antennas as close to each other as possible. However, in this case coupling between the array antennas will reduce the reflecting properties of the reflector array.

The purpose of the present communication is to demonstrate that this is true for a Van Atta reflector consisting of four half-wave dipoles arranged on a line. Some theoretical studies of the influence of coupling in Van Atta reflector arrays have been carried out previously [2]–[4]. In this communication, theoretical results obtained by using the methods described in [2]–[4] will be compared with experimental results. In contrast to previous experimental results [4] which have been presented as normalized, the results described here are absolute. Before the experimental results are described, some theoretical remarks will be given.

Theory

For a linear Van Atta reflector consisting of \( n \) parallel half-wave dipoles, we will determine the maximum back-scattering cross section for an incident wave polarized parallel to the dipoles and propagating along the normal to the plane containing the dipoles. This back-scattering cross section will be determined when coupling is neglected. Then there are two fields which add up to give the cross section. First, the field due to scattering from the dipoles when they receive the incident wave; second, the field due to the interconnections between the dipoles [4]. If the length of the transmission lines is chosen to be an unequal number of half a wavelength, these two fields add in phase and we have the maximum cross section for normal incidence. It is well-known that for one dipole, the back-scattering cross section of the field due to scattering is \( 0.20\pi \). Since the field intensity due to the interconnecting transmission lines is of the same magnitude as the field intensity due to scattering, the maximum back-scattering cross section of one dipole is \( 4 \times 0.20\pi \), i.e., the maximum back-scattering cross section for normal incidence is \( 0.80\pi \) for the Van Atta reflector. This result shows that if a certain space is available, the cross section increases with the square of the number of dipoles arranged within the space. However, the cross section cannot be increased indefinitely, because coupling will reduce the back-scattering cross section when the dipoles are

Fig. 1. The experimental Van Atta reflector.

Fig. 2. Back-scattering cross section for normal incidence as a function of the length of the transmission lines. Distance between the dipoles equals 8 cm.

Fig. 3. Back-scattering cross section for normal incidence as a function of the distance between the dipoles. Length of the transmission lines is about 0.400 \( \lambda \).
This is done in order to determine easily the transmission lines connecting the dipoles. The reflection cross section for normal incidence. A Van Atta reflector consisting of four parallel half-wave reflectors has a maximum back-scattering which the maximum does not occur for the length of slot-fed dipoles with open-ended transmission lines. This result is shown in Fig. 2 and is in agreement with the theory. It is seen that there is a maximum of reflection when the length of the transmission lines is an integer.

Next, with the length of the transmission lines adjusted to about 0.40λ + pλ, the cross section is measured when the equispacing is decreased in steps of 8 cm between the dipoles, the cross section is measured as a function of the length of the transmission lines. The results are shown in Fig. 3. The main results to be described were obtained when an identical grid array of circular waveguides was excited as a single mode was propagating in the H-plane of scan. In this case the array-scattering matrix is proportional to the radiated field components

\[ \Phi_j = \sqrt{1 - T_j^2 - T_j} \cdot \left( \sum_{n=-\infty}^{\infty} \sum_{m=-\infty}^{\infty} a_{nm} W_{nm} \cdot E_{da} \right) \]

where the angles θ and φ are the usual polar coordinate angles associated with the x, y, z coordinate system. T_x and T_y are the beam-pointing directional cosines with respect to the x and y axis (the ground plane). The transmission coefficients of the array-scattering matrix are proportional to the radiated field components

\[ T_0 = \sqrt{V_{00}/V_1 E_0} \]

and

\[ T_0 = \sqrt{V_{00}/V_1 E_0} \]

when only a circular TM_{11} mode is excited on the aperture. The results to be described were obtained by numerically solving the vector two-dimensional integral equation for the planar array of circular waveguides [7].

We solve for the unknown tangential electric field E at the aperture A of the circular waveguides. The \( \{\Phi_j\} \) and \( \{W_{nm}\} \) are, respectively, the circular waveguide modes [7], [8] and the periodic free-space modes required by Floquet's Theorem (p = 1 denotes a TE mode, p = 2 a TM mode). The \( Y_1 \) and \( Y_{nm} \) are the respective modal admittances.

Acknowledgment

The author wishes to express his appreciation to the Radiation Laboratory, University of Michigan, Ann Arbor, for the use of their microwave anechoic chamber for the experimental study carried out during his stay at the laboratory.

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Manuscript received June 21, 1968

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A Note on the Radiation Characteristics and Forced Surface Wave Phenomena in Triangular-Grid Circular Waveguide Phased Arrays

Abstract—Forced surface wave resonances are shown to occur in dielectric-free 45-degree triangular-grid circular waveguide phased arrays. Similar surface wave phenomena were observed in an identical grid array of rectangular waveguides in the H-plane of scan. In the circular waveguide array, however, the resonance is observed in the E-plane and is shown to be an isolated point. This isolation is further illustrated by observing certain vector symmetries in the radiation patterns.

Considerable effort has been devoted towards developing an understanding of certain anomalous resonances [1]–[7] which occur in phased-array antennas. These phenomena are manifested by total internal reflection and consequently no radiation of power by the antenna at particular angles of scan. While the existence of these phenomena was, to a degree, expected for dielectric-covered phased arrays under certain conditions [1], [2], it has been shown that they can also occur in dielectric-free brick arrays of rectangular waveguides [3], [4] and in equilateral triangular arrays of circular waveguides [7]. The brick array of rectangular waveguides and a circular array with an identical grid both exhibit forced surface wave phenomena, but in different planes of scan. The results to be described were obtained by numerically solving the vector two-dimensional integral equation for the planar array of circular waveguides [7]:

\[ \sum_{j=1}^{J} A_j Y_j \Phi_j = \sum_{j=1}^{J} Y_j \Phi_j \int_A \Phi_j E_{da} \]

where the angles θ and φ are the usual polar coordinate angles associated with the x, y, z coordinate system. T_x and T_y are the beam-pointing directional cosines with respect to the x and y axis (the ground plane). The transmission coefficients of the array-scattering matrix are proportional to the radiated field components

\[ T_0 = \sqrt{V_{00}/V_1 E_0} \]

and

\[ T_0 = \sqrt{V_{00}/V_1 E_0} \]

when only a circular TE_{11} mode is excited on the aperture. The unitary condition for the scattering matrix determines the proportionality constants.

In the brick array analyzed earlier [3], [4], which is a single mode was propagating in the waveguide, surface wave resonances were observed in the H-plane of scan. In contradistinction, however, when an identical grid array of cylindrical waveguides is excited as shown in Fig. 1, we note that a forced surface wave resonance is present in the E-plane of scan before the first grating lobe (denoted by the vertical arrows) appears. The magnitude of the reflection is plotted versus the differential steering phases ϕ_x or ϕ_y along the x or y coordinates. They are proportional to T_x and T_y [7]. In the H-plane scan, no such resonance is observed although |R_z| is very nearly one at grazing incidence (the heavy arrow). Small changes in the wavelength do not greatly alter the results except that total reflection at grazing incidence is observed in the H-plane at other wavelengths.

In addition, it is of interest to note that, unlike the results found for the brick array of rectangular waveguides, the surface wave resonances found here (in the E-plane here and for other planes in different grids [7]) occur at isolated points in the scan plane. This