Integration of Heat Pumps and Cogeneration in the Future Energy System

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Integration of Heat Pumps and Cogeneration in the Future Energy System

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Thermal Energy Section

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Introduction

• Political objectives for utility production are to reduce CO$_2$ emissions and increase security of supply.

Several solutions are proposed:

1. High amount of intermittent electricity production from wind turbines and PV.
2. Replacement of coal with biomass in thermal units.
4. ...
Introduction

• Political objectives for utility production are to reduce CO₂ emissions and increase security of supply.
  Several solutions are proposed:
  1. High amount of intermittent electricity production from wind turbines and PV.
  2. Replacement of coal with biomass in thermal units.
  4. ... 

• Differently from “old“ CO₂ reduction measures (“The Danish Example“):
  1. The Production objectives for thermal power plants will be changed towards higher production of heat.
  2. Combined Heat and Power (CHP) plants in DK are required to fulfill heat demand in timeperiods were electricity production is not favourable.
  3. New heat production facilities will be required: Biomass boilers, heat pumps, etc.
Combined Heat and Power basics

- CHP-plants are the most efficient utility technology available today (in terms of exergy efficiency).
- High boiler efficiencies.
- High utilisation factor.
- Advanced flue gas cleaning.
- Easy flexibility between heat and power production, the trade off in an extraction power plant is typically 7-9 (can be compared to COP of a heat pump).

- Heat losses in DH network.
- Subject to boiler ramp rates.
Electricity and heat demand concurrency

- Coproduction allows higher efficiency and lower prices, but bad coherence between demand timeframe.
- Methods to decouple the prod. constraints of both heat and electricity may prove valuable.
  - electricity storage
  - heat storage
  - heat pumps
  - ...

![Graph showing heat and electricity demand over time]

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Electricity and heat demand concurrency

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  - ...

![Graph: Heat demand vs. Electricity demand over time]
Electricity and heat demand concurrency

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- Methods to decouple the prod. constraints of both heat and electricity may prove valuable.
  - electricity storage
  - heat storage
  - heat pumps
  - ...

![Electricity demand 2011](solid line)  
![Residual from wind](dashed line)
Electricity and heat demand concurrency

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- Methods to decouple the prod. constraints of heat and electricity may prove valuable.
  - electricity storage
  - heat storage
  - heat pumps
  - ...

![Graph of electricity demand](image-url)
Introduction of heat pumps in DH-systems

- The use of low cost electricity can expand the feasible production of heat in the PQ-diagram.
- Introduction of a Heat Pump with 50 MW capacity and a COP of 2.6 [-] at AVV1 results in a higher area of the feasible zones by 26.6%

- The changed operation of the system is the focus of further studies
- Preliminary study show that introduction of 100-300 MW Heat pump capacity in the Copenhagen Area allow an approx. 1-2 % fuel reduction of the power plants of Eastern Denmark.
Introduction of heat pumps in DH-systems

- Five possible heat pump configurations have been identified for a system with DH networks.
Optimal heat pump design for configuration 1

- A thermoeconomic (exergoeconomic) comparison is conducted to evaluate the optimal heat pump design for the configuration and temperature of DH-network.
- 7 different working fluids are examined (R134a, R1234ze, R290, R407C, R600a, R717 and R744)
- The minimized cost of heat is calculated for each individual configuration and later compared in order to find the optimum.
Log mean temperatures

Heat reservoirs change temperature, i.e. log mean temperatures are required.

- Log mean temperature of sink
  \[
  \bar{T}_{lm,\text{sink}} = \frac{(T_{h,o} - T_{h,i})}{(\ln(T_{h,o}) - \ln(T_{h,i}))}
  \]

- Log mean temperature of source
  \[
  \bar{T}_{lm,\text{source}} = \frac{(T_{c,o} - T_{c,i})}{(\ln(T_{c,o}) - \ln(T_{c,i}))}
  \]

- COP Lorenz
  \[
  COP_{\text{Lorenz}} = \frac{\bar{T}_{lm,\text{sink}}}{(\bar{T}_{lm,\text{sink}} - \bar{T}_{lm,\text{source}})}
  \]

- Lorenz efficiency
  \[
  \eta_{\text{Lorenz}} = \frac{COP_{\text{HP}}}{COP_{\text{Lorenz}}}
  \]
Assumptions in heat pumps thermoeconomics

- Purchased Equipment Cost (PEC):
  - Open type compressor PEC = $f(\text{working fluid; swept volume})$
  - Electrical motor with a fixed efficiency PEC= $f(\text{shaft work})$
  - Heat exchanger PEC= $f(\text{Area})$ [Yan et. al. 1998],[Yan et. al. 1999],[Martin 1996]
  - Expansion valve PEC=0
- Total Capital Investment of a component is 4.16 higher than PEC of the component to account for additional cost [Bejan et al. 1996].
- Electricity and natural gas prices correspond to the price of fuel (with variations) and taxes considering the heat pump operated by CHP-producer.
- Interest and Inflation Rate is fixed (7 % and 2.13 %)
- Technical lifetime of entire system: 15 years
- Operation Hours: 1400 hours/year
The impact of the optimisation procedure

- In this example, the sink temperatures are fixed, and the source temperature is varied.
- R600a is investigated with four fixed pinch temperatures and compared to the optimal solution where the combined cost of the plant is minimised.
- In the optimal solution the evaporator and condenser can have different pinch temperatures.
Operation limits of current components

- Components are subject to mechanical and thermal stresses.
- The different component limits are identified for each working fluid.

<table>
<thead>
<tr>
<th>Refrigerant</th>
<th>Cond. pressure °C</th>
<th>Lubrication max. temp. °C</th>
</tr>
</thead>
<tbody>
<tr>
<td>R134a</td>
<td>82,8</td>
<td>170</td>
</tr>
<tr>
<td>R1234ze</td>
<td>96,1</td>
<td>170</td>
</tr>
<tr>
<td>R290</td>
<td>74,1</td>
<td>170</td>
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<tr>
<td>R407C</td>
<td>64,5</td>
<td>170</td>
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<tr>
<td>R600a</td>
<td>119,2</td>
<td>170</td>
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<tr>
<td>R717</td>
<td>90,79</td>
<td>170</td>
</tr>
<tr>
<td>R744</td>
<td>140 bar</td>
<td>170</td>
</tr>
</tbody>
</table>
Minimised cost of heat - Comparison

![Graph showing cost vs. Log Mean Temperature Lift for different refrigerants (R134a, R1234ze, R290, R407C, R600a, R717, R744).]
Minimised cost of heat - Comparison

Log Mean Temperature Lift

\[ C_{\text{heat}} [\text{EUR/MWh}] \]

- R134a
- R1234ze
- R290
- R407C
- R600a
- R717
- R744

Log Mean Temperature Lift

0 10 20 30 40 50 60 70 80

60 40 20 0

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Corresponding COP

![Graph showing COP values for different refrigerants.]

- R134a
- R1234ze
- R290
- R407C
- R600a
- R717
- R744

Log Mean Temperature Lift vs. COP

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Corresponding Lorenz efficiency

Log Mean Temperature Lift vs. Lorenz efficiency for various refrigerants:
- R134a
- R1234ze
- R290
- R407C
- R600a
- R717
- R744
Corresponding Lorenz efficiency

Log Mean Temperature Lift

Lorenz efficiency [\%]

R134a
R1234ze
R290
R407C
R600a
R717
R744
Parametric study of assumptions and temperature levels
Summary

- Efficient heat pumps can be used to decouple the constraints of electricity and heat production and address the high energy efficiency needed to match political targets.
- This presentation only includes configuration 1.
- For a fixed log mean temperature lift, the heat pumps can be ranked based on the cost of heat, where R717 has lowest cost.
- Most applicable heat pump solutions present higher cost than a natural gas boiler.
- \( \text{COP}_{HP} < \text{COP}_{CHP} \)
- Reasonable to expect a span of 1 between upper and lower performance on COP.
- Considering applicable equipment, a lower limit of 0.3 of Lorenz efficiency can be expected. In some cases 0.4 of Lorenz efficiency can be achieved.