



Bureau, Emil; Schilder, Frank; Avrutin, Viktor; Starke, Jens; Santos, Ilmar; Thomsen, Jon Juel

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Emil Bureau DTU Mech. Eng.



Jens Starke
DTU Mathematics



Frank Schilder DTU Mathematics



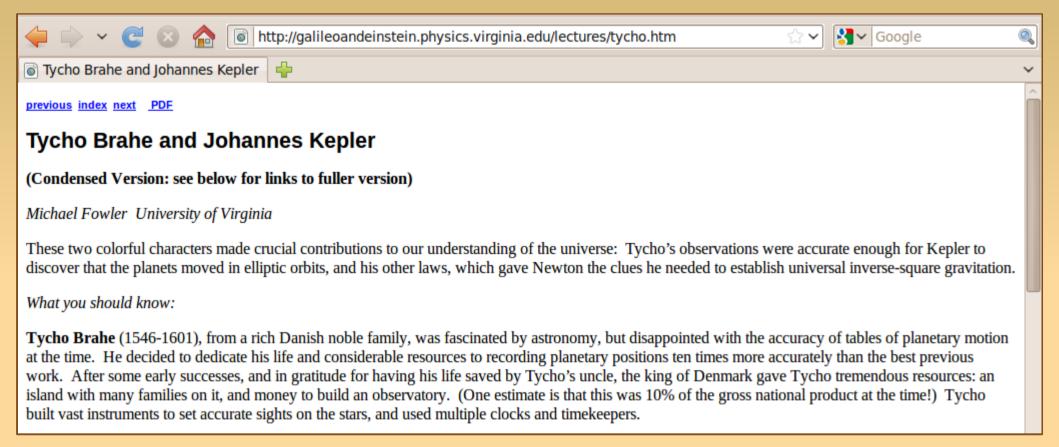
Ilmar Santos DTU Mech. Eng.



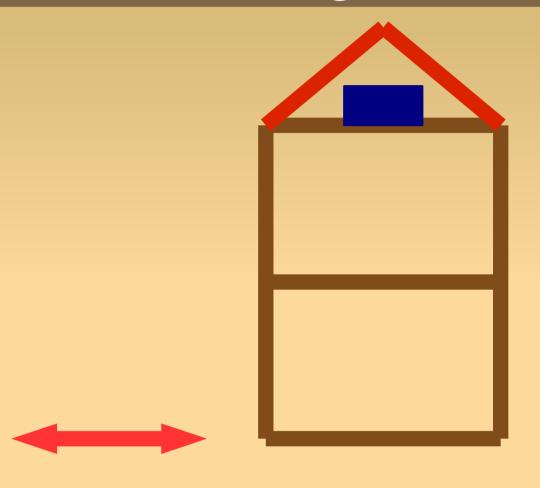
Viktor Avrutin IPVS Stuttgart

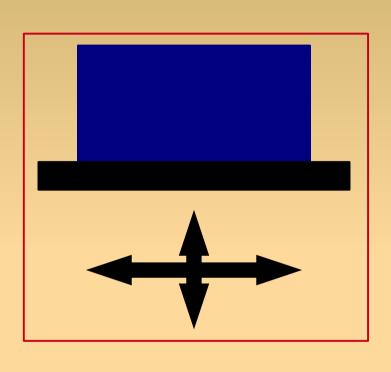


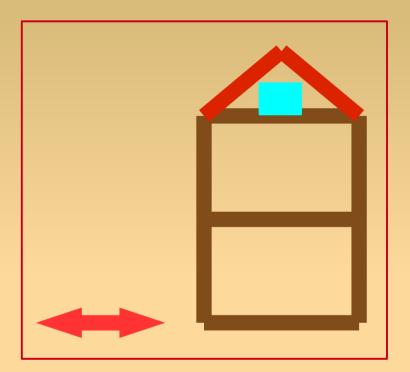
Jon Juel Thomsen DTU Mech. Eng.

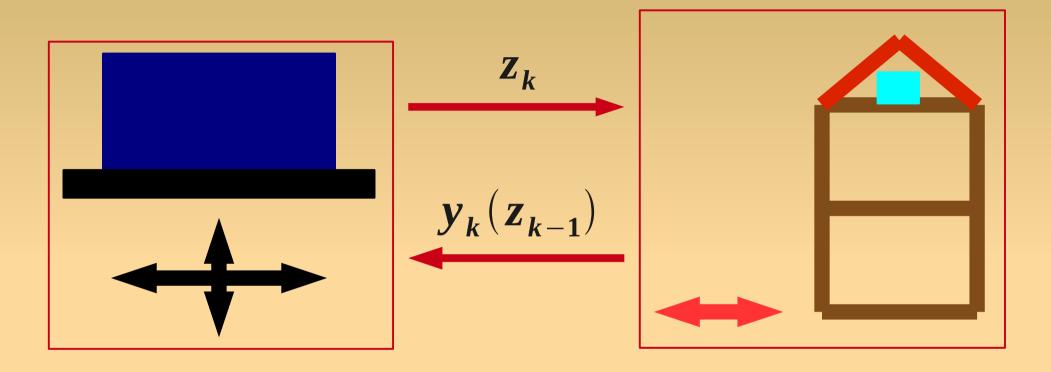


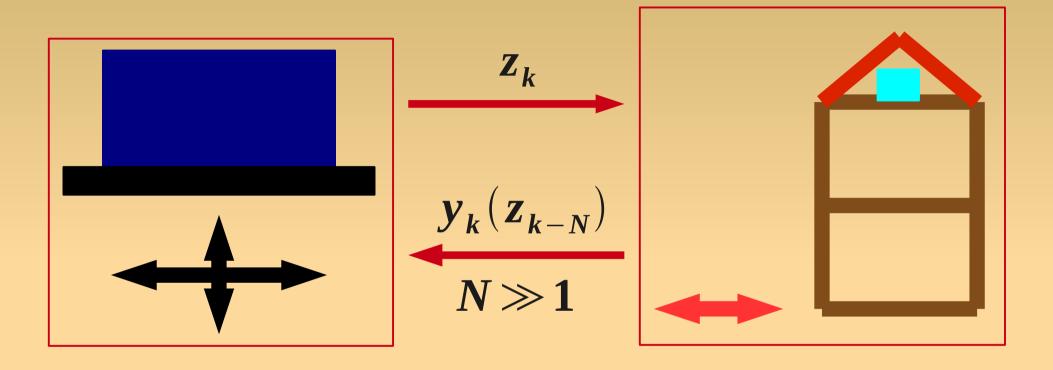








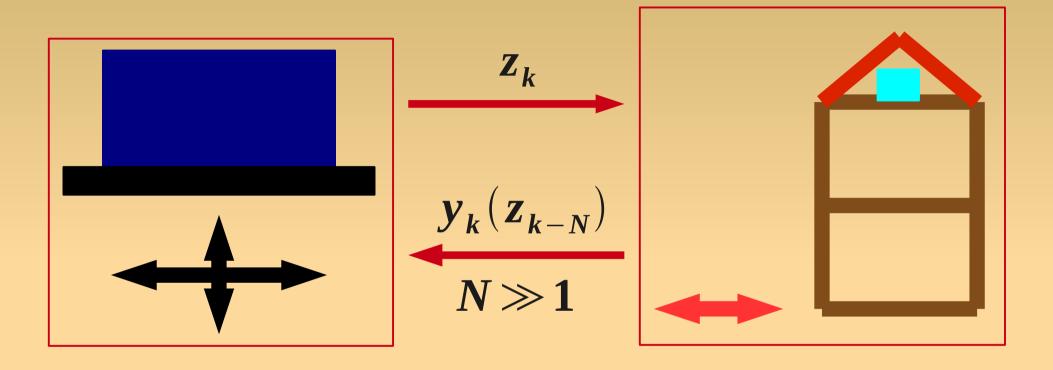


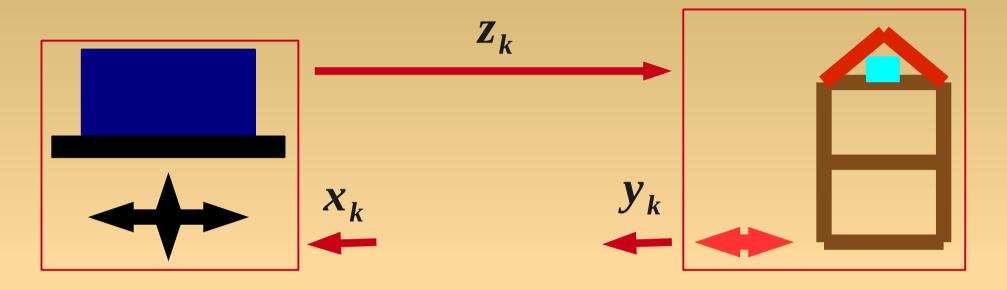


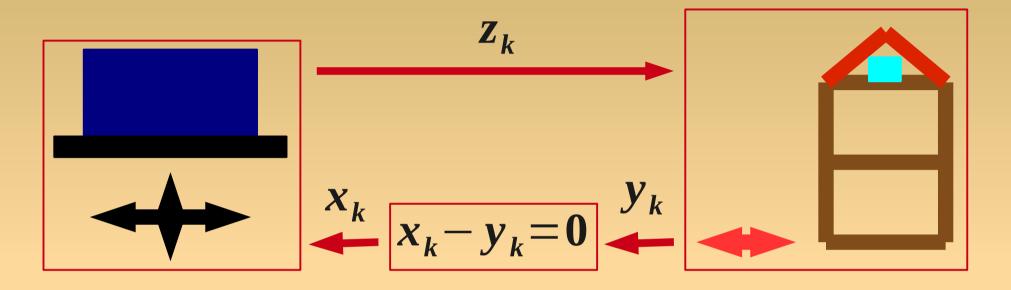
Sources of delay in dynamic sub-structuring:

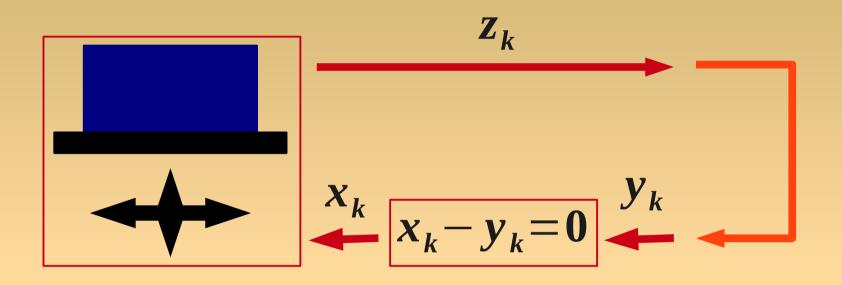
- Computation time of time step of model
- Delayed actuation of physical experiment

This delay is usually sufficiently large to destabilise the combined system.





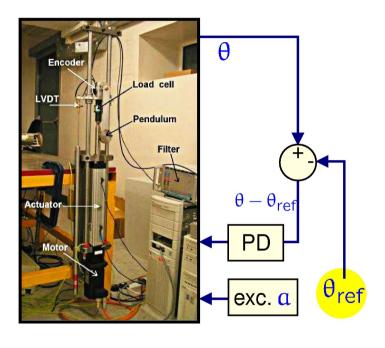




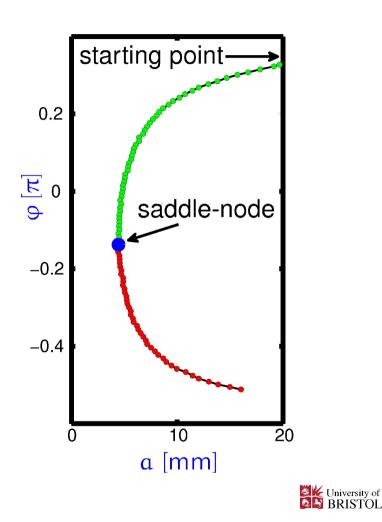
Vertically excited pendulum

Set-up

feedback control for angle θ reference signal θ_{ref}



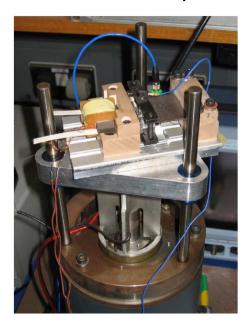
Continuation of rotations

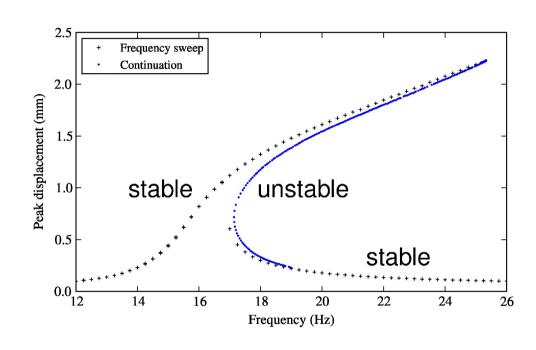


Sieber and Krauskopf, Nonlinear Dynamics, 2008 Sieber, Krauskopf, Wagg, Neild and Gonzalez-Buelga, JCND, 2011

Continuation in an energy harvester

continuation experiment by David Barton and Stephen Burrow





setup

nonlinear frequency response

[Barton & Burrow, ASME 2009 Proceedings]



Barton, Mann and Burrow, J. Vib. Control, accepted manuscript.



Test rig with impact oscillator.

Continuation rests upon the Implicit Function Theorem. Assume we are given an equation of the form

$$F(u,\mu)=0, F:X\times R^m\to Y$$

and we know an initial solution. Then, a continuation algorithm will compute a covering of the solution manifold through the initial solution.

To apply continuation we need to construct a zero problem for our experiment.

Fundamental idea: introduce feed back control that uses

$$0 \stackrel{!}{=} x(t) - z(t)$$

as a control target and apply Newton (like) method to solve the equation

 $x_Q - z_Q = 0$,

where \mathbf{x}_{Q} and \mathbf{z}_{Q} are discretisations of $\mathbf{x}(t)$ and $\mathbf{z}(t)$.

The control scheme must satisfy a number of conditions.

Notation:

- ullet Experiments Y, Z_u
- Measurements $y(\mu, t)$, $z(\mu, t, x(t))$
- Samples $Y(\mu, N) = \{y_0, \dots, y_{N-1}\}, Z_u(\mu, N, x)$

1. Consistent:

$$Y \equiv Z_0$$

[Continuous?, Smooth?]

1. Consistent:

$$Y \equiv Z_0$$

2. Locally stabilising: any equilibrium state y of Y must become an asymptotically stable equilibrium state of Zu. In other words, if a controlled experiment Zu with control target

$$0 \stackrel{!}{=} y(t) - z(t)$$

is initialized close to an equilibrium state of Y, then the state z must converge to the state y over time.

3. Non-invasive: $||u|| \le \delta ||x-z||$, $x \in U_{\varepsilon}(y)$

Remember, the control target is 0 = x(t) - z(t), so any linear control scheme will typically be consistent and non-invasive.

In many applications a PD controller will be locally stabilising.

In our implementation we use Simulink's PID block, which is nonlinear and time-dependent, but locally monotonic around 0.

Discretisation.

$$\Phi_{o}: \mathbb{R}^{N} \rightarrow \mathbb{R}^{2Q+1}, \quad \Phi_{o}^{-1}: \mathbb{R}^{2Q+1} \rightarrow \mathbb{C}^{\infty}$$

$$c \in \mathbb{R}^{2Q+1}, \ x(t) := \Phi_Q^{-1}(c)$$

$$u(t) := G(x(t)) := PD(x(t) - z(t))$$

$$F(c,\mu)$$
:= $\Phi_Q(Z_u(\mu,N,G(\Phi_Q^{-1}(c))))-c$

Proof of concept.

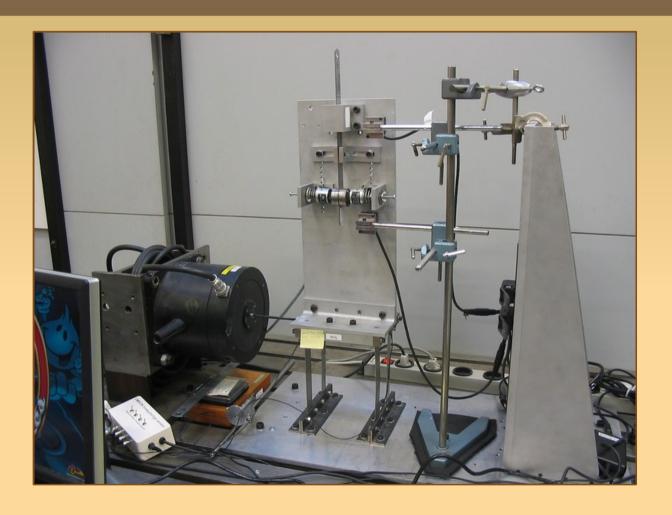
$$\|\mathbf{u}\| = \|\mathbf{P}\mathbf{D}(\mathbf{x} - \mathbf{z})\|$$

$$\leq \delta \|\mathbf{x} - \mathbf{z}\|$$

$$\leq \delta \kappa \|\boldsymbol{\Phi}_{\infty}(\mathbf{x}) - \boldsymbol{\Phi}_{\infty}(\mathbf{z})\|$$

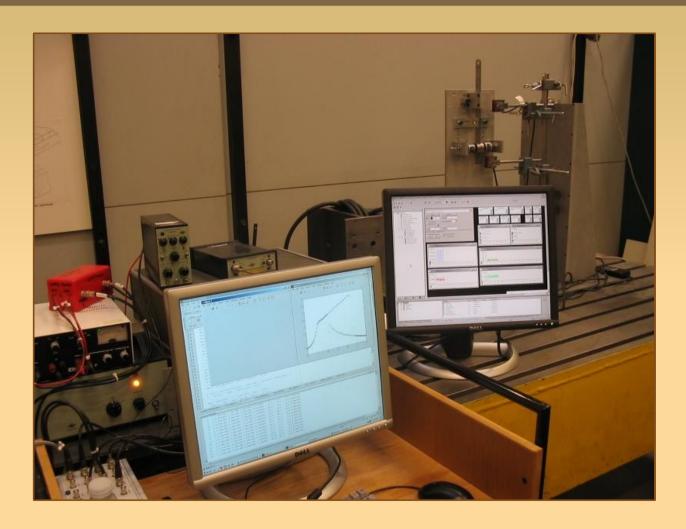
$$\leq \delta \kappa \|\mathbf{F}(\mathbf{c}, \boldsymbol{\mu})\| + \mathbf{R}_{\mathbf{Q}+1}$$

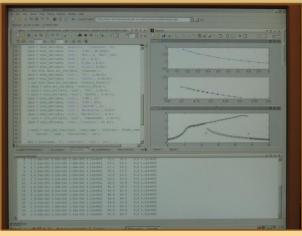
Example: Impact Oscillator

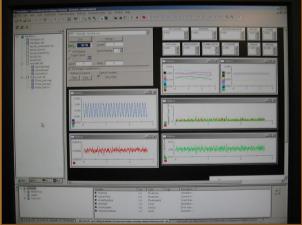




Example: Impact Oscillator



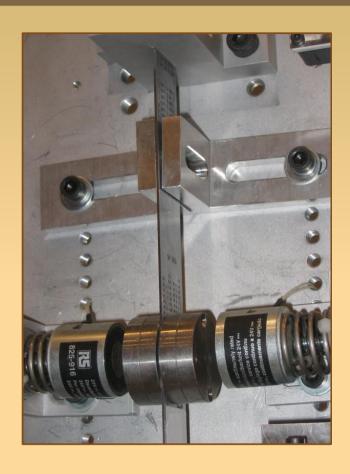


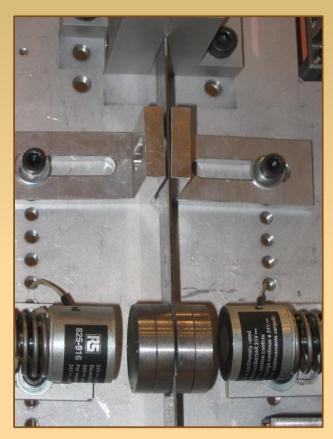


Example: Duffing Oscillator

Simulations by Viktor.

Experimental results.





Current and Future Work

Matlab toolbox for:

- Guided simulations
- Guided experiments
- Equation free methods

Techniques for:

- Measuring stability
- Detecting bifurcations
- Branch-switching etc.

Current and Future Work

Unstable solutions are useful!

Pyragas control:
$$0 \stackrel{!}{=} z(t) - z(t-T)$$

Sieber control:
$$0 \stackrel{!}{=} y(t) - z(t)$$

Very simple (low-tech) auto-adaptive control schemes.

Exploit, don't destroy natural dynamics!