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Composting and compost utilization: 
Accounting of greenhouse gases and global warming contributions

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Abstract
Greenhouse gas (GHG) emissions related to composting of organic waste and use of compost was assessed from a waste management perspective. The GHG accounting for composting includes use of electricity and fuels, emissions of methane and nitrous oxide from the composting process, and savings obtained by the use of the compost. The GHG account depends on waste type and composition (kitchen organics, garden waste), technology type (open systems, closed systems, home composting), the efficiency of off-gas cleaning at enclosed composting systems, and the use of the compost. The latter is an important issue and is related to the long term binding of carbon in the soil, to related effects in terms of soil improvement and to what the compost substitutes; this could be fertilizer and peat for soil improvement or for growth media production. The overall Global Warming Factor (GWF) for composting therefore varies between significant savings (-900 kg CO$_2$-equivalents tonne$^{-1}$ wet waste (ww)) and a net load (300 kg CO$_2$-equivalents tonne$^{-1}$ ww). The major savings are obtained by use of compost as a substitute for peat in the production of growth media. However, it may be difficult for a specific composting plant to document how the compost is used and what it actually substitutes for. Two cases representing various technologies were assessed showing how GHGs accounting can be done when specific information and data are available.

Keywords: Composting, greenhouse gases, global warming, CO$_2$ accounting, UOD tables
1. Introduction

Composting is a common treatment of biodegradable waste. Approximately 2000 composting facilities for household organic wastes are in operation in Europe, 40% of which are only treating garden waste (ECN, 2008). Composting is a relatively simple, durable and inexpensive technology for stabilising and reducing biodegradable waste (Crowe et al., 2002). Composting could be an important technology in developing countries, where the waste usually has high content of wet organic materials. However, composting is also a suitable treatment option for biological waste in developed countries. For example, in the Netherlands, 97% of source separated biowaste is treated in composting facilities (Brinkmann et al., 2004). A range of technologies is in operation worldwide, from unmanaged static piles to highly engineered systems with automatic turning and treatment of the released gases in biofilters.

In a global warming (GW) context, composting contributes to emissions as well as to avoided emissions. Greenhouse gases (GHGs) are released from composting facilities due to degradation of organic matter and due to energy used by heavy machinery used for turning and managing of the waste. The finished product (compost) can be used on land. The benefit is twofold: the use of inorganic fertilizers is avoided and carbon is bound to soil. Compost can also replace peat in the production of growth media and thus avoid the emissions occurring during peat extraction and subsequent mineralization under aerobic conditions (Boldrin et al., 2009b).

The purpose of this paper is to describe composting of waste from a GW perspective and provide information about processes and data useful in accounting GHG emissions. The GHGs accounting is done as suggested by Gentil et al. (2009) distinguishing between Upstream, Operation and Downstream (UOD) contributions and between fossil and biogenic carbon dioxide (CO₂). A schematic representation of the assessed system and the alternative options for use of compost is presented in Figure 1.

![Figure 1 – Schematic representation of the assessed system.](image)

According to the Kyoto protocol, GHG emissions should be reported annually on a national basis. The 2006 IPCC Guidelines for National Greenhouse Gas Inventories (Eggleston et al., 2006) provides detailed guidelines on how to estimate the annual GHG emissions from biological treatment of waste. Default values have been reported for GHG emissions from biological treatment of waste with no further specification of technology and waste type. This paper will summarize estimated emissions from composting and provide likely ranges for both direct and indirect emissions. Such contributions are in this study called Global Warming Factors (GWFs) and are normalized to CO₂-equivalents (eq.) tonne⁻¹ wet waste (ww). Estimated GWFs can be used for different GHG emission reporting mechanisms, having different scopes and boundaries, as described in Gentil et al. (2009). Three different technologies have
been assessed (open, enclosed and home composting) and two cases have been presented with detailed information on all contributions of GHG emissions. Composting in developing countries is unfortunately not completely covered, because despite composting is widely practiced in such countries, data availability on process inventories is still very scarce. For instance, recently Liamsanguan & Gheewala (2008) and Zhao et al. (2009) performed two LCA studies on municipal solid waste management in Thailand and China: in both cases inventory data regarding composting were taken from literature and/or databases because of lack of specific data.

2. Overview of solid waste composting technologies

The following paragraphs provide a general description of the key characteristics of the principal organic waste composting technologies. The main focus is on the issues that are considered important with respect to GW and GHGs accounting.

The composition and characteristics of the feedstock are very important for both designing and operating the composting plant and for the final quality of the compost (Haug, 1993). GHG emissions from the plant will also depend on the various types of machinery used in open or closed facilities, the turning rates, types of emission controls, and the internal temperature/moisture conditions. Theoretically, any kind of biodegradable waste can be composted. Practically, only a few waste fractions are composted in relevant amounts. Composting systems are also based on a broad spectrum of technologies, with individual technologies customized to specific waste fractions.

Table 1 presents the organic waste fractions and the technologies covered by this study. In this table, we try to define the level of relevance of a technology with respect to a waste fraction. This study focuses on Municipal Solid Waste (MSW), but the results could eventually apply to other waste fractions having similar characteristics. For the sake of simplicity, we have aggregated different organic waste fractions in two main fractions, defined as:

- Food waste: source separated food and organic fractions of market wastes.
- Garden and park waste: coming from private gardens and public parks. It consists of grass from lawn mowing, hedge cuttings, prunings, and leaves; from a process perspective, other materials with similar composition may be assimilated, e.g. crop residues, bark and forestry waste. Also paper, mostly made of cellulose, shows similar behavioural patterns

<table>
<thead>
<tr>
<th>Technology</th>
<th>Food waste</th>
<th>Garden waste</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Open technologies</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Windrow</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Static pile</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Mat</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td>Vermicomposting</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td><strong>Enclosed technologies</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Channel and cell</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td>Aerated pile</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Brikollari</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td><strong>Reactor technologies</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Tunnel reactor</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Box and container</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td>Rotating drum</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td>Tower</td>
<td>X</td>
<td></td>
</tr>
<tr>
<td><strong>Other</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Home composting</td>
<td>X</td>
<td>X</td>
</tr>
</tbody>
</table>
In many countries, household food waste and garden waste are collected together in a fraction called “VFG” (Vegetable, Fruit, Garden) or “biowaste” which can be composted. In many cases, food waste and garden waste are mixed on purpose at the composting plant, so that garden waste provides structure to the feedstock. In this study, the two fractions will be kept separated. Allocation of emissions could be carried out according to the ratio of food and garden waste in the composting feedstock.

Different approaches have been used to classify composting technologies. The most common distinction is whether the degradation takes place outdoor, in enclosed buildings or in private gardens (home composting or backyard composting as it is also called).

2.1. Open technologies
In open technologies composting is performed in outdoor facilities. The gaseous emissions are in general neither collected nor treated, but released to the atmosphere. Open technologies are in general simpler and less engineered than enclosed technologies.

Windrow and mat composting
In windrow composting, waste is placed in triangular or trapezoidal windrows. Ventilation could be natural (diffusion and convection) or active (forced or vacuum-induced aeration). Turning of the windrows is often necessary and in most cases performed with a turning machine or a front loader. Turning results in increased porosity and homogenization of compost in terms of moisture and ensures that all compost is exposed to high temperature. The frequency of turning may influence the composting time, especially of those materials with tendency to clog. The size and shape of the windrows are determined by the turning equipment and the type of aeration. Mat composting is a variation of windrow composting, where layers of feedstock with different characteristics are laid on top of each other and the bulky materials are placed at the bottom to facilitate bottom-up convective ventilation.

Static pile composting
Static piles have the shape of a truncated pyramid and are not agitated nor turned. Ventilation is assured by sufficient material porosity, which could be reached by using bulking agents. In alternative, active ventilation is also possible by placing aeration pipes or blowers directly in the piles or at their base.

2.2. Enclosed technologies
In enclosed systems, the composting process takes place in an enclosed building. This facilitates the possibility of controlling the exhaust gases and a common treatment is filtration of the air in biofilters. In most of the enclosed technologies (including reactor technologies) the retention time is limited which means that curing of the material in open windrows or piles is often required afterwards.

Channel and cell composting
In channel composting, the raw material is placed in enclosed windrows which are individually controlled. The channels are separated by walls, which usually also are used as tracks for the turning machines. If the channels are short they are called cells. The compost material is moved from one end to the other (or from one channel to the next) during the process and it is actively aerated and turned with various frequencies (e.g. every day or every other day).
Aerated pile
Aerated pile composting is similar to the open windrow technology. The difference is that aerated pile composting takes place in an enclosed building and that turning is done with automated turning machines. An aeration system is normally installed underneath the piles to ensure a proper flow of oxygen. The difference between the channel and cell technology and the aerated pile technology is that the aerated pile is not placed in channels which can be individually controlled.

2.3. Reactor technologies
Reactor technologies (also called in-vessel systems) are a variant of enclosed technologies and they are assessed together with the enclosed technologies in this paper. Due to a smaller head space above the compost, the volume of exhaust gases that needs to be treated in a reactor is smaller. There is better control of the exhaust gases compared to enclosed technologies and a biofilter is almost always installed.

Tunnel composting
Tunnel reactors are used for composting organic MSW, sewage sludge and manure. Generally there is good process control and the exhaust gases are controlled and recirculated to prevent atmospheric emissions and increase homogenization of internal conditions (e.g. temperature and moisture). Some systems are static and some are agitated and the level of process control also varies significantly.

Rotating drum composting
Rotating drum composting is a reactor technology that is primarily used for organic MSW. As the name indicates, this composting technology ensures constant movement (rotation) of the material and concurrent aeration, which results in a very quick breakdown of organic materials in MSW, after which (retention time from 1-10 days) they easily can be separated from non-compostable materials and sent to the next process/curing stage. One of the drawbacks of this technology is the relatively large electricity requirements for the rotation.

2.4 Home composting
In home composting (also called backyard composting) handling of waste is undertaken at a private level. Because the composting is performed with minimal equipment (plastic composters, wooden boxes, homemade enclosures using fencing) and very different levels of control, an average home composting process can hardly be defined. One main advantage of home composting is that no external energy is required for transport or processing. The key point from a GW perspective is to ensure proper “blending” of different materials and to ensure that the heap is sufficiently bulky and aerated, which avoids significant production/release of methane (CH₄).

3. Composting technologies, GHG emissions and GWFs
The GHG emissions are defined in terms of:
- Direct emissions, directly linked to activities at the composting site and the degradation of the waste.
- Indirect emissions or avoided emissions taking place outside the composting site. These are:
  - Upstream activities such as production of materials and electricity used at the site, the provision of fuels used on the site and the construction of the facilities.
**Downstream activities such as avoided emissions when substituting peat or fertilizer or binding of carbon in the soil when compost is applied on land.**

GHG emissions are reported according to the technology type and the waste type. Emission factors (EFs) for electricity provision, fuel provision and fuel combustion are taken from Fruergaard et al. (2009) and presented in Table 2. The emission factor for electricity is very dependent on the fuel mix used and whether or not there is co-generation (use of heat), thus it varies a lot from country-to-country as well as from technology-to-technology. The range we have used in our estimations is based on low and high averages for the Nordic countries and Central Europe (Fruergaard et al., 2009).

Table 2 - Emission factors (EFs) relevant in GHG accounting for composting.

<table>
<thead>
<tr>
<th>Type of process/emission</th>
<th>Emission factor</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Provision of diesel oil</td>
<td>0.4-0.5 kg CO$_2$-eq litre$^{-1}$ diesel</td>
<td>Fruergaard et al. (2009)</td>
</tr>
<tr>
<td>Combustion of diesel oil</td>
<td>2.7 kg CO$_2$-eq litre$^{-1}$ diesel</td>
<td>Fruergaard et al. (2009)</td>
</tr>
<tr>
<td>Provision of electricity</td>
<td>0.1-0.9 kg CO$_2$-eq kWh$^{-1}$</td>
<td>Fruergaard et al. (2009)</td>
</tr>
<tr>
<td>Production of N fertilizer</td>
<td>4.7-13.0 kg CO$_2$-eq kg N$^{-1}$</td>
<td>Table 10</td>
</tr>
<tr>
<td>Production of P fertilizer</td>
<td>0.5-3.1 kg CO$_2$-eq kg P$^{-1}$</td>
<td>Table 10</td>
</tr>
<tr>
<td>Production of K fertilizer</td>
<td>0.4-1.5 kg CO$_2$-eq kg K$^{-1}$</td>
<td>Table 10</td>
</tr>
<tr>
<td>Production of peat</td>
<td>550-1197 kg CO$_2$-eq tonne$^{-1}$ peat</td>
<td>Section 3.3</td>
</tr>
</tbody>
</table>

**3.1. Indirect upstream emissions**

The upstream contributions to GW are for the composting system related to:

- Provision of fuels: production and transport of fuels are assumed to be 0.4-0.5 kg CO$_2$ litre$^{-1}$ diesel (Fruergaard et al., 2009).
- Variable use of electricity for lighting on the site, administration buildings, and electrical equipment for the treatment of waste. The amount of electricity use can vary a lot, depending on the composting technology under consideration. In general, open technologies use less electricity than closed technologies. Typical values for open technologies are in the range of 0.023-19.7 kWh tonne$^{-1}$ of ww (Finnveden et al., 2000; Recycled Organics Unit, 2003; Komilis & Ham, 2004; EC, 2006; Fisher, 2006; Boldrin et al., 2009a; Cabaraban et al., 2008), but values are mostly in the lower part of the range. The electricity use for managing a reactor composting plant is in the range of 9-65 kWh tonne$^{-1}$ ww (Smith et al., 2001; Baky & Eriksson, 2003; NIRAS, 2004; Brinkmann et al., 2004; EC, 2006; Fisher, 2006; Güereca et al., 2006; Cabaraban et al., 2008; EASEWASTE database), while Komilis & Ham (2004) report 16.1-16.9 kWh tonne$^{-1}$ ww of electricity used for facilities where windrows are placed on an enclosed composting pad. GHG emissions from the use of electricity can be calculated using emission factors reported in Table 2. Very little data is available in literature and therefore no data are included in this paper.

**3.2. Direct emissions**

Direct emissions from composting can be divided into two main categories: emissions from fuel combustion and gaseous emissions occurring in different phases of waste treatment due to degradation/mineralization of the organic material. In the next paragraphs, the release of the following compounds is described and estimated: fossil CO$_2$, biogenic CO$_2$, CH$_4$ and nitrous oxide (N$_2$O).

Direct CO$_2$ emissions from fossil fuel combustion are mainly from shredders, front loaders and turning equipment. Fuel consumption is generally larger in open technologies than in enclosed
technologies. Typical values for diesel consumption in open technologies are in the range 0.4-6.0 litre diesel tonne\(^{-1}\) ww (Smith et al., 2001; USEPA, 2006; Recycled Organics Unit, 2003; Komilis & Ham, 2004; EC, 2006; Fisher, 2006; Boldrin, 2007; Kranert & Gottschall, 2007; Boldrin et al., 2009a), but in most cases a consumption around 3 litres tonne\(^{-1}\) ww is reported. For enclosed technologies diesel consumption is reported being 0.13-3.0 litre tonne\(^{-1}\) ww (Komilis & Ham, 2004; EC, 2006; Fisher, 2006), but typically in the lower end of the range. GHG emissions from fuel combustion can be calculated using emission factors reported in Table 2. The combustion of fuels from collection and transportation of waste and compost is not included here, since this issue is covered in Eisted et al. (2009). Avoided collection and transportation of waste is one of the main benefits in terms of GHG emissions of home composting, as also assessed in Fisher (2006).

The main gaseous emission from composting is biogenic CO\(_2\) which, in national inventories, is accounted for as part of the natural carbon cycle with land-use change and forestry estimates; thus it is not counted as a waste sector emission (Eggleston et al., 2006). The main GHGs that contribute to global warming are CH\(_4\) and N\(_2\)O. The release of these gases depends on the technology, the waste input and above all the management of the process. A properly blended starting mix will avoid incurring additional losses of N, whilst properly designed and managed forced aeration and a timely turning (when needed) will avoid triggering production and subsequent release of CH\(_4\). The differences in carbon (C) and nitrogen (N) contents in the different waste factions are presented in Table 3.

Table 3 - Typical carbon and nitrogen contents of the different waste types considered.

<table>
<thead>
<tr>
<th>Compound</th>
<th>Unit</th>
<th>Food waste</th>
<th>Reference</th>
<th>Garden waste</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Carbon (C)</td>
<td>kg tonne(^{-1}) ww</td>
<td>100-365</td>
<td>3,4,5</td>
<td>93-250</td>
<td>2,3,4</td>
</tr>
<tr>
<td></td>
<td>kg tonne(^{-1}) dm</td>
<td>249-491</td>
<td>1,3,4,5,6</td>
<td>150-460</td>
<td>1,2,3,4</td>
</tr>
<tr>
<td>Nitrogen (N) total</td>
<td>kg tonne(^{-1}) ww</td>
<td>3.7-13</td>
<td>3,4,5</td>
<td>2.3-17</td>
<td>2,3,4</td>
</tr>
<tr>
<td></td>
<td>kg tonne(^{-1}) dm</td>
<td>10-26</td>
<td>3,4,5,6</td>
<td>17-75</td>
<td>2,3,4</td>
</tr>
</tbody>
</table>


Some facilities (enclosed technologies) might be equipped with odour removal devices. A common and inexpensive treatment is filtration of exhausts in biofilters. The efficiencies of biofilters depend on air flow, load, residence time, materials and design (Powelson et al., 2006; Chung, 2007). For facilities with biofilters, the removal efficiencies (\(\eta\)) for CH\(_4\) are reported to be between 47-100 % (Daleno et al., 1997; Baky & Eriksson, 2003; Powelson et al., 2006). More controversial data are found regarding N\(_2\)O: 90% removal is reported by Daleno et al. (1997) and Baky & Eriksson (2003), while both Clemens & Cuhls (2003) and Amlinger et al. (2008) report that biofilters could be a source of N\(_2\)O, especially when ammonia (NH\(_3\)) loads are high. If the technology does not include a biofilter (for example open technologies), the \(\eta\) is set to zero in equation (3) and (4).

The amounts of carbon (\(C_{\text{release}}\), kg) and nitrogen (\(N_{\text{release}}\), kg) that are emitted to the atmosphere during composting can be calculated from the inputs of carbon (\(C_{\text{input}}\), kg) and nitrogen (\(N_{\text{input}}\), kg) and the fractional loss of the elements (\(C_{\text{loss%}}\)) and (\(N_{\text{loss%}}\)):

\[
C_{\text{release}} = C_{\text{input}} \times C_{\text{loss%}} \quad \text{(Equation 1)}
\]

\[
N_{\text{release}} = N_{\text{input}} \times N_{\text{loss%}} \quad \text{(Equation 2)}
\]
The total mass of C or N lost during composting (as % of input mass) can be measured at composting facilities or found in literature and then used in equation (1) and (2) to calculate emissions. Alternatively, emissions could be estimated via a mass balance, calculating the difference between contents in input and output from the composting process. The latter approach is, however, very uncertain.

Several studies have investigated or reported degradation of organic matter and C during composting (Table 4). Production of mature compost requires degradation of 40-83 % of the carbon contained in the compost. Most of this carbon is emitted as biogenic CO\textsubscript{2}, relatively small percentages are emitted as CH\textsubscript{4}, as explained later. If biofilters are present, part of such CH\textsubscript{4} could be oxidized and additional biogenic CO\textsubscript{2} is generated. An overview of CO\textsubscript{2} emissions from composting of organic matter is presented in Table 5.

### Table 4 - Organic matter and carbon degradation during composting as reported in literature.

<table>
<thead>
<tr>
<th>Substance</th>
<th>Degradation (%)</th>
<th>Reference</th>
<th>Comment</th>
</tr>
</thead>
<tbody>
<tr>
<td>Carbon</td>
<td>50-70</td>
<td>Dalemo et al. (1997)</td>
<td>Waste type not specified</td>
</tr>
<tr>
<td>Carbon</td>
<td>83</td>
<td>Hellebrand (1998)</td>
<td>Garden waste</td>
</tr>
<tr>
<td>Carbon</td>
<td>68</td>
<td>Smith et al. (2001)</td>
<td>Waste type not specified</td>
</tr>
<tr>
<td>Carbon</td>
<td>40-60</td>
<td>Crowe et al. (2002)</td>
<td>Waste type not specified</td>
</tr>
<tr>
<td>Carbon</td>
<td>66-70</td>
<td>Ham &amp; Komilis (2003)</td>
<td>Food waste</td>
</tr>
<tr>
<td>Carbon</td>
<td>50</td>
<td>Fisher (2006)</td>
<td>Both windrow and in-vessel</td>
</tr>
<tr>
<td>Carbon</td>
<td>64</td>
<td>Boldrin (2007)</td>
<td>Garden waste</td>
</tr>
<tr>
<td>Carbon</td>
<td>56</td>
<td>Andersen et al. (2009)</td>
<td>Garden waste</td>
</tr>
<tr>
<td>Organic matter</td>
<td>50</td>
<td>Edelmann et al. (2000)</td>
<td>60% kitchen waste, 40% garden waste</td>
</tr>
<tr>
<td>Organic matter</td>
<td>75</td>
<td>Cabaraban et al. (2008)</td>
<td>Waste type not specified</td>
</tr>
</tbody>
</table>

### Table 5 - CO\textsubscript{2}-biogenic emissions from degradation of organic matter during composting.

<table>
<thead>
<tr>
<th>Technology</th>
<th>Waste type</th>
<th>CO\textsubscript{2} emission (kg tonne\textsuperscript{-1} ww)</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Open</td>
<td>Garden</td>
<td>118-413</td>
<td>1,2,3</td>
</tr>
<tr>
<td></td>
<td>Biowaste</td>
<td>43-173</td>
<td>1,4,5</td>
</tr>
<tr>
<td>Closed</td>
<td>Biowaste</td>
<td>250-390</td>
<td>2</td>
</tr>
<tr>
<td>Home composting</td>
<td>Biowaste</td>
<td>139-215</td>
<td>1</td>
</tr>
<tr>
<td>Not specified</td>
<td>Not specified</td>
<td>98-563\textsuperscript{*}</td>
<td>6</td>
</tr>
</tbody>
</table>

1. Amlinger et al. (2008)
3. Andersen et al. (2009)
4. Gronauer et al. (1997)

The gaseous N losses during composting could be quite variable, depending on specific conditions of the process, such as the C/N ratio and the nature of N in the feedstock (influencing availability of N) as well as temperature, pH and aeration rate (determining NH\textsubscript{3} evaporation). For instance, losses in the range 26-51% of the initial N content are reported for biowaste (Beck-Friis et al., 2000; NIRAS, 2004), while only 1.7 % of initial N is emitted in gaseous form in case of garden waste (Hellebrand, 1998). Finnvveden et al. (2000) estimate a leakage of nitrogen to 7.5 % of the initial N for a composting plant working in negative pressure.
Methane (CH$_4$) is formed in anaerobic pockets of the compost material. The total loss of CH$_4$ (CH$_4$$_{\text{release}}$, kg) is estimated from the total loss of carbon (C$_{\text{release}}$, kg), the percentage of carbon that is lost as CH$_4$ (CH$_4$$_{\text{emitted}}$) and the efficiency of the biofilter ($\eta$).

$$CH_{4,\text{release}} = C_{\text{release}} \times CH_{4,\text{emitted}} \times (1 - \eta) \times \frac{16}{12}$$ (Equation 3)

Edelmann et al. (2000) reports 5.1-13.5% of the degraded C emitted as CH$_4$ depending on the management of the composting process. Lower values are found in other studies, as presented in Table 6, where quantification of emissions is also attempted. It is worth noting that Smith et al. (2001), USEPA (2006), Recycled Organics Unit, 2003 and Cabaraban et al. (2008) assume that no CH$_4$ emissions occur during composting, despite Clemens & Cuhls (2003) reports that CH$_4$ emissions occur even in well aerated processes. Home composting is not well covered by literature, but Smith et al. (2001) assumes no CH$_4$ is emitted. Whilst it is reasonable to assume that a certain release of CH$_4$ does actually occur, optimisation of processes at compost sites is supposed to minimize the emissions, relative to figures reported in older studies. Hence adoption of lowest values for BAT technologies and process management seems reasonable for modern facilities.

Table 6 - CH4 emissions during composting of organic waste.

<table>
<thead>
<tr>
<th>Technology</th>
<th>Waste</th>
<th>CH4-C (%) degraded C</th>
<th>Reference</th>
<th>CH4 emission (kg tonne$^{-1}$ ww)</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Open</td>
<td>Garden</td>
<td>2.1-2.7</td>
<td>1,2,3</td>
<td>0.05-6.8</td>
<td>1,3,4</td>
</tr>
<tr>
<td></td>
<td>Biowaste</td>
<td>0.8-2.5</td>
<td>4</td>
<td>0.03-1.5</td>
<td>4,7,8,9</td>
</tr>
<tr>
<td>Enclosed</td>
<td>Biowaste</td>
<td>2.4-3</td>
<td>5,6</td>
<td>0.02-1.8</td>
<td>4,5,7,8,9</td>
</tr>
<tr>
<td>Home composting</td>
<td>Biowaste</td>
<td>2.0-3.6</td>
<td>4</td>
<td>0.8-2.2</td>
<td>4</td>
</tr>
<tr>
<td>Not specified</td>
<td>Not spec.</td>
<td></td>
<td></td>
<td>0.03-8*</td>
<td>10,11</td>
</tr>
</tbody>
</table>


* not used in the UOD tables

Nitrous Oxide (N$_2$O) is primarily formed in anaerobic pockets where an oxygen gradient occurs (Beck-Friis et al., 2000) as a by-product of both nitrification and denitrification (Eggleston et al., 2006). Nitrous Oxide is mainly produced in the later stage of the composting process, when the readily available C has been consumed (He et al., 2000). The release of N$_2$O (N$_2$O$_{\text{release}}$, kg) can be calculated in the same way as CH$_4$, where N$_2$O$_{\text{emitted}}$ is the fraction of input nitrogen lost as N$_2$O during the composting process:

$$N_2O_{\text{release}} = N_{\text{release}} \times N_2O_{\text{emitted}} \times (1 - \eta) \times \frac{44}{28}$$ (Equation 4)

In literature N$_2$O emissions are reported on a total N basis or degraded N basis. Some examples are reported in Table 7. In other studies, N$_2$O is not included in the accounting of GHG emissions (Smith et al., 2001; Recycled Organics Unit, 2003). Any other GHGs than CO$_2$, CH$_4$ and N$_2$O are very unlikely to occur at compost sites, hence are not covered in this paper.
Table 7 – N2O emissions during composting of organic waste.

<table>
<thead>
<tr>
<th>Technology</th>
<th>Waste</th>
<th>N2O-N (％input N)</th>
<th>N2O-N (％degraded N)</th>
<th>Reference</th>
<th>N2O emission (g tonne⁻¹ ww)</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Open</td>
<td>Garden</td>
<td>0.5-1.8</td>
<td>0.8-23</td>
<td>1,2,3</td>
<td>25-178</td>
<td>2,3,4,5</td>
</tr>
<tr>
<td></td>
<td>Biowaste</td>
<td>0.1-0.7</td>
<td>2-17</td>
<td>4,5,6</td>
<td>7.5-252</td>
<td>4,7,8,9</td>
</tr>
<tr>
<td>Enclosed</td>
<td>Biowaste</td>
<td>1.8</td>
<td>10</td>
<td>10-120</td>
<td>4,9,10,11</td>
<td></td>
</tr>
<tr>
<td>Home composting</td>
<td>Biowaste</td>
<td>0.95-1.25</td>
<td>14-15</td>
<td>4</td>
<td>192-454</td>
<td>4</td>
</tr>
<tr>
<td>Not spec</td>
<td>Not spec</td>
<td></td>
<td></td>
<td>10-600</td>
<td>12,13,14</td>
<td></td>
</tr>
</tbody>
</table>

3. Andersen et al. (2009)  
4. Amlinger et al. (2008)  
5. Finnveden et al. (2000)  
6. Dalemo et al. (1997)  
10. Gronauer et al. (1997)  
12. Eggleston et al. (2006)  
* not used in the UOD tables

3.3. Indirect downstream emissions

In this paper we consider GHG emissions only for two possible alternative uses of the compost produced from treatment of organic waste:

- Compost used in growth media in substitution of peat;
- Compost used on land as a soil amendment.

Downstream inventory does not include incineration of screened residues, landfilling of screened residues and/or compost, or the use of compost in landscaping works and/or in landfill topcovers. Estimation regarding incineration and landfilling could be done according to Astrup et al. (2009) and Manfredi et al. (2009).

Use on land of compost

Compost materials contain organic matter, which can be characterized as readily degradable, slowly degradable and stable organic matter. When degradable organic matter is oxidized, CO₂ is emitted to the atmosphere. The stable organic matter has a turnover of 100 to 1000 years and thus a fraction of the C is bound in soil for long periods (Smith et al., 2001; Favino & Hogg, 2008) and removed from the C cycle. This bound C can be seen as a sink of CO₂ (as if it is removed from the atmosphere) and it can be credited as an avoided downstream emission of CO₂ to the waste management system (Marmo, 2008). If C_{input} (kg) is the C content in compost and C_{bind} is the fraction of C which is “stable”, then the sink of CO₂ (CO₂_{bind}; kg) can be calculated as:

\[ CO₂_{bind} = C_{input} \times C_{bind} \times \frac{44}{12} \]  
(Equation 5)

The C still bound to soil after 100 years is estimated to be 2-10 % of the input in compost (Smith et al., 2001; Brinkmann et al., 2004; Fisher, 2006), while Bruun et al. (2006) estimated 9-14 % depending on the soil type and the crop rotation.

The C content in compost is in the order 56-386 kg tonne⁻¹ ww (Table 8), which means that 1-54 kg C tonne⁻¹ ww could be bound in soil, equivalent to 4-198 kg CO₂-equ tonne⁻¹ compost. Carbon binding is thus in the order of 2-79 kg CO₂-equ tonne⁻¹ of food waste and 3-73 kg CO₂-equ tonne⁻¹ of garden waste, assuming mass losses during the composting process of 60 % and 30 % respectively. This estimation is somewhat lower than that provided by ICF (2005), which reports 270 kg CO₂-equ tonne⁻¹ ww is bound in soil, regardless of the type of waste and the composition of the compost.
Table 8 - Typical carbon and nutrients (N, P, K) content of different compost types.

<table>
<thead>
<tr>
<th>Compound</th>
<th>Unit</th>
<th>From food waste</th>
<th>From garden waste</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Value</td>
<td>Reference</td>
<td>Value</td>
</tr>
<tr>
<td>Carbon (C)</td>
<td>kg tonne⁻¹ ww</td>
<td>63-386</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td>kg tonne⁻¹ dm</td>
<td>191-470</td>
<td>1,2,3,4</td>
</tr>
<tr>
<td>Nitrogen (N) total</td>
<td>kg tonne⁻¹ ww</td>
<td>6.0-21.5</td>
<td>1,4,5,6,7,8</td>
</tr>
<tr>
<td></td>
<td>kg tonne⁻¹ dm</td>
<td>9-28</td>
<td>1,3,4,5,6,7,9</td>
</tr>
<tr>
<td>Phosphorous (P)</td>
<td>kg tonne⁻¹ ww</td>
<td>1.8-4.7</td>
<td>1,4,5,6,7</td>
</tr>
<tr>
<td></td>
<td>kg tonne⁻¹ dm</td>
<td>1.8-9.3</td>
<td>1,3,4,5,6,7</td>
</tr>
<tr>
<td>Potassium (K)</td>
<td>kg tonne⁻¹ ww</td>
<td>6.0-13.4</td>
<td>1,4,7</td>
</tr>
<tr>
<td></td>
<td>kg tonne⁻¹ dm</td>
<td>3.4-23</td>
<td>1,3,4,6,7</td>
</tr>
</tbody>
</table>


Compost contains nutrients which can displace the use of mineral fertilizer produced by industrial processes (most often N, P, and K fertilizers). This assumes, however, that the compost is used rationally as part of a fertilization plan. Typical N, P, and K contents of food waste compost and garden waste compost are reported in Table 8.

The utilization efficiencies of the organic and mineral nutrients depend on different factors such as the mineralization rate after application, the type of soil and type of crop. The substitution ratios could thus vary between 0 and 1. The amount of mineral fertilizers displaced (Mass

\[
\text{Mass}_{\text{disp}} = \text{Input}_{\text{nutrient}} \times \text{Subs}_{\text{eff}}
\]

(Equation 6)

Substitution ratios for N, P, and K are reported in literature (Dalemo et al., 1998; Vogt et al., 2002; Brinkmann et al., 2004; Hansen et al., 2006):

- N: 20-60%
- P: 90-100%
- K: 100%

An estimation of the amount of mineral fertilizer replaced by the use of compost is done by combining substitution coefficients and N, P, and K contents reported in Table 8. Results are reported in Table 9. Similarly, Crowe et al. (2002) estimates that per tonne of ww 2.5-10 kg N, 0.5-1 kg P and 1-2 kg K can be recovered through composting.

Table 9 – Potential amount of inorganic fertilizers replaceable by use of compost.

<table>
<thead>
<tr>
<th>Waste type</th>
<th>Waste input (kg)</th>
<th>Compost output (kg)</th>
<th>Inorganic fertilizer replacement (kg tonne⁻¹ treated waste)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Food</td>
<td>1000</td>
<td>400</td>
<td>0.5-5.2, 0.6-1.9, 2.4-5.4</td>
</tr>
<tr>
<td>Garden</td>
<td>1000</td>
<td>700</td>
<td>0.5-3.4, 0.6-2.8, 3.5-9.7</td>
</tr>
</tbody>
</table>
The production of mineral fertilizer implies the use of energy and other materials resulting in emissions of GHG. GW contributions from production of commercial fertilizers are reported in literature and databases (see Table 10). Typical GHG emissions per kg of nutrients produced are 4.75-13.0 kg CO₂-eq for N fertilizers, 0.52-3.09 kg CO₂-eq for P and 0.38-1.53 kg CO₂-eq for K. The variability between different sources is at least partially due to the energy mix considered for electricity production. Combining such EFs (Table 2) with the amount of inorganic fertilizer replaced previously described, saved emissions can be estimated as: 4-81 kg CO₂ tonne⁻¹ of food waste and 4-67 kg CO₂ tonne⁻¹ of garden waste.

Table 10 - GHG emissions for production of mineral fertilizers (kg CO₂-eq kg⁻¹ nutrient).

<table>
<thead>
<tr>
<th>N</th>
<th>P</th>
<th>K</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>11.5-13.0</td>
<td>1.74-1.90</td>
<td>0.69-0.79</td>
<td>Hansen et al. (2006)</td>
</tr>
<tr>
<td>8.65</td>
<td>1.28-2.72</td>
<td>0.53-1.53</td>
<td>Ecoinvent</td>
</tr>
<tr>
<td>7.49</td>
<td>1.20</td>
<td>1.16</td>
<td>GEMIS</td>
</tr>
<tr>
<td>5.29</td>
<td>0.52</td>
<td>0.38</td>
<td>Smith et al. (2001)</td>
</tr>
<tr>
<td>4.75-10.77</td>
<td>3.095</td>
<td>0.56</td>
<td>Audsley et al. (1997)</td>
</tr>
<tr>
<td>5.34-9.56</td>
<td>0.8-2.48</td>
<td>-</td>
<td>Wood &amp; Cowie (2004)</td>
</tr>
</tbody>
</table>

Application of treated organic waste to land (Use-On-Land, UOL) can result in emissions of N₂O. The amount of N₂O emitted is proportional, among other things, to the amount of N applied with compost. If N_input is the content of nitrogen (kg) per tonne of compost and N₂O%N is the fraction of nitrogen converted to N₂O, then the release of N₂O (N₂O_UOL kg) to air per tonne of WW can be calculated as:

\[ N_2O_{UOL} = N_{input} \times N_2O_{%N} \times \frac{44}{28} \]  

(Equation 7)

Different studies report that 1.0-2.2 % of the nitrogen applied with compost is emitted as N₂O (Dalemo et al., 1998; Vogt et al., 2002; Brinkmann et al., 2004; Bruun et al., 2006; Eggleston et al., 2006). Fisher (2006) assumes that no GHG is emitted after the spreading of compost.

Using composition data from Table 8 and assuming 60 % mass loss for food waste and 30 % for garden waste during the composting process, emissions of N₂O after spreading of compost on land can be estimated to be 38-297 g N₂O tonne⁻¹ of food waste and 43-194 g N₂O tonne⁻¹ of garden waste.

The foregoing, basically refers to a possible release of N from organic fertilisers during periods in which vegetation is not able to take N in. Other authors, instead, have actually remarked the possibility of an overall reduction of N₂O from farmlands where compost is used. This mostly refers to the possibility to replace a readily available source of N with a slow-release one, which avoids creation of an excessive N pool in the soil susceptible of forming N₂O. Favino and Hogg (2008) have for instance derived a potential saved emission in the range of 20-201 g N₂O tonne⁻¹ of compost (assuming avoided N₂O emission between 0.05% and 0.5% of the total N applied through mineral fertilisers), equivalent to 8-81 g N₂O tonne⁻¹ of food waste and 14-141 g N₂O tonne⁻¹ of garden waste.

Spreading of compost on land involves some fuel consumption. Dalemo et al. (1997) reports that diesel consumption for spreading of solid residues is 444 MJ ha⁻¹, i.e. 12 litre ha⁻¹. If the EU Nitrate Directive is fulfilled (i.e. 170 kg N ha⁻¹, EEC (1991)), maximum allowed compost application would be 8-
28 tonne ha\(^{-1}\) for food waste and 21-44 tonne ha\(^{-1}\) for garden waste. Assuming the mass losses during compost as above, the spreading would result in 0.17-0.60 litre tonne\(^{-1}\) of food waste and 0.19-0.40 litre tonne\(^{-1}\) of garden waste. In the case of home composting, spreading is assumed to be done manually (no fuel consumption is reported).

The use of compost on land can have further benefits on GW for downstream effects of its application. Beside savings of inorganic fertilizers and carbon binding, spreading of compost on land can result in increased water retention of the soil (reduced irrigation), reduced herbicides/biocides requirements, improved soil structure, and reduced erosion. All these aspects could implicate some GHG savings, which are not quantified in this paper because of lack of data or of the high uncertainty related to that (i.e. local conditions, use, agricultural methods, etc...). However, it is worth noticing that some estimates allocate an important part of benefits for GW coming from application of compost, to these induced effects on soils.

**Peat substitution**

Compost produced from organic waste can be a potential alternative to peat in the production of growth media. Compost can dilute peat at different ratios, depending on the type of growth media, and up to 50 % (Prasad & Maher, 2006), although this typically refers to professional growth media, whereas media for amateur gardening may include up to 100% compost. The substitution is usually done on a 1:1 volume basis (Mathur & Voisin, 1996), i.e. a certain volume of peat (e.g. 1 m\(^3\)) is substituted by an equivalent volume of compost (1 m\(^3\)). Avoiding use of peat saves GHG emissions occurring during the extraction, transportation and use (i.e. degradation) of peat materials. Different studies estimated GHG emissions within a 100 year period from all phases of the peat life cycle for some European countries: around 970 kg CO\(_2\)-eq are emitted per tonne of peat used in Denmark (Boldrin et al., 2009b), 621-1197 kg CO\(_2\) tonne\(^{-1}\) of peat are emitted in the German scenario (Kranert & Gottschall, 2007), while 550 kg CO\(_2\) tonne\(^{-1}\) of peat are estimated in a Dutch study (Brinkmann et al., 2004). Part of the variability could be explained with the origin of peat and related transportation distances. In Smith et al. (2001) it is estimated that 823 kg CO\(_2\) are emitted per tonne of peat, without including land preparation, extraction and transportation in their calculations.

Considering different compost and peat densities, it is here assumed that 1 tonne of compost can replace the use of 0.2-1 tonne of peat. Avoided emissions are thus in the order of 110-1197 kg CO\(_2\)-eq tonne\(^{-1}\) of compost used in growth media preparation instead of peat (44-479 kg CO\(_2\)-eq tonne\(^{-1}\) of food waste and 77-838 kg CO\(_2\)-eq tonne\(^{-1}\) of garden waste). Such an estimate is much higher than the 16.2 kg CO\(_2\)-eq tonne\(^{-1}\) of compost reported by Barton et al. (2008). In addition, the use of compost in growth media preparation could also replace some mineral fertilizers otherwise added to the mix (Boldrin et al., 2009b). Such estimation is not included here, but it could be carried out in the same way described above for the use of compost on land.

Compost used in growth media is eventually degraded and the C contained is released to atmosphere as biogenic CO\(_2\). According to the C content in compost reported in Table 8, the emission of biogenic CO\(_2\) is estimated in the range 231-1415 kg CO\(_2\) tonne\(^{-1}\) compost for food waste and 205-741 kg CO\(_2\) tonne\(^{-1}\) compost for garden waste. Considering the mass losses during the composting process, the emission is estimated to be 92-566 kg CO\(_2\) tonne\(^{-1}\) ww for food waste and 143-518 kg CO\(_2\) tonne\(^{-1}\) ww for garden waste. Emissions of N\(_2\)O related to use of compost in growth media is not reported or mentioned anywhere. It is here assumed it is the same as for the use on land case: 38-297 g N\(_2\)O tonne\(^{-1}\) of food waste treated and 43-194 g N\(_2\)O tonne\(^{-1}\) of garden waste treated.
4. Results and discussion

Results of GW contribution for the composting process are presented in Upstream, Operation and Downstream (UOD) tables for three overall technologies:

- Open technologies (mix of garden waste and food waste or solely garden waste) with no collection or treatment of the gases (Table 11).
- Enclosed technologies (food and garden waste) including both enclosed technologies and reactor technologies as defined above. In some cases a biofilter is used for exhaust treatment (Table 12).
- Home composting (mix of vegetable kitchen waste and some garden waste) (Table 13).

The contributions to global warming by biogenic CO₂ are calculated according to the criteria set by Christensen et al. (2009), i.e. Global Warming Potential (GWP) = 0. The GWP of CO₂-fossil is 1, the GWP for CH₄ is 25 (1 kg of CH₄ = 25 kg of CO₂) and 298 for N₂O (1 kg of N₂O = 298 kg of CO₂) (Solomon et al., 2007).

The downstream emissions have been estimated allocating emissions according to the nutrient contents (e.g. high N content results in large mineral fertilizer savings but also higher N₂O emissions).

The results show that energy issues (electricity and diesel) have a minor relevance in the GHG accounting of composting technologies. Moreover, if the electricity emission factor is low-medium then the GHG emissions related to use of electricity and fuel are quite similar for open and enclosed technologies. GHG emissions due to degradation of organic matter during the composting process (direct) seem to depend both on the management and on the type of technology. Proper blending of input feedstock, and optimised adoption of forced aeration may minimise the production of GHGs, whilst treatment for removal of CH₄ and N₂O could result in large improvements in the system compared to open systems where gaseous emissions are not treated.

Downstream emissions represent the crucial factor in GHG accounting for different composting systems. Use of compost for peat substitution has a large potential for emission savings and from a GW perspective it could be preferable to the use of compost on land. Among the different mineral fertilizer included in the evaluation, nitrogen is the one potentially leading to large savings.

When comparing different types of waste, the main conclusion is that garden waste has lower energy requirements and lower emissions than food waste, but also less potential benefits because of the lower content of nutrients.

Only a few studies regarding direct gaseous emissions from home composting are available. If such figures were confirmed, home composting would perform better than large facilities, both because of no energy requirements and avoided collection and transportation (the latter is not quantified here). Assumptions made on the use of home compost and what it substitutes for could introduce additional uncertainty. A more thorough survey is recommended.

Aggregated results presented in Table 11, Table 12 and Table 13 are in line with figures reported in other reports. Smith et al. (2001) reports net fluxes of GHGs: -37 kg CO₂-eq tonne⁻¹ ww for open composting, -32 kg CO₂-eq tonne⁻¹ ww for enclosed composting and -58 kg CO₂-eq tonne⁻¹ ww for home composting. Fisher (2006) reports GWFs in the order of 13 kg CO₂-eq tonne⁻¹ ww for windrow composting and 12 kg CO₂-eq tonne⁻¹ ww for in-vessel composting, while a factor of -202 kg CO₂-eq tonne⁻¹ ww was found in Chen & Lin (2008). A common aspect of these studies is that they do not show the variability of emission factors. This is mainly because they make precise assumptions even when analysing complex and heterogeneous situations, such as a national waste management policy.

Two examples have been selected to better illustrate the use and interpretation of the UOD tables and to show how GWFs of composting can be calculated if data are available on the various contributing processes. The two cases are: reactor composting of biowaste and windrow composting of garden waste.
Composting of household biowaste is extensively covered by a Dutch study (Brinkmann et al., 2004). In the Netherlands in 2004, 86 % of the source separated biowaste was composted in enclosed system, while the remaining 14 % was composted in open windrow systems. The average electricity consumption in Dutch facilities was 32 kWh tonne\(^{-1}\) ww and 400 kg of compost were produced out of every tonne of separately collected biowaste. Gas emissions, after biofilter, were estimated to be 195 g CH\(_4\) tonne\(^{-1}\) of biowaste and 101 g N\(_2\)O tonne\(^{-1}\) of biowaste. According to the emission factors reported in Table 2 the GWF of upstream activities is 3.2-28.8 kg CO\(_2\)-eq tonne\(^{-1}\) ww and the GWF of direct emissions is 35 kg CO\(_2\)-eq tonne\(^{-1}\) ww. The compost produced contained 9.4 kg N tonne\(^{-1}\), 4.8 kg P\(_2\)O\(_5\) tonne\(^{-1}\) (i.e. 2.1 kg P tonne\(^{-1}\)) and 8.1 kg K\(_2\)O tonne\(^{-1}\) (i.e. 6.7 kg K tonne\(^{-1}\)). The substitution ratios are assumed to be 60 % for N, 90 % for P and 100 % for K. Substitution of mineral fertilizers would save emissions in the order \(30\) kg CO\(_2\)-eq tonne\(^{-1}\) of compost (\(12.1-35.8\) kg CO\(_2\)-eq tonne\(^{-1}\) ww as collected waste). N\(_2\)O emissions from application of compost on land were assumed to be 1.25 % of the applied nitrogen, which means 47 g N\(_2\)O tonne\(^{-1}\) ww (or 14 kg CO\(_2\)-eq tonne\(^{-1}\) ww). Carbon binding was reported to save 24.2 kg CO\(_2\)-eq tonne\(^{-1}\) ww. In modelling peat substitution, it was estimated that 1 tonne of compost could replace 830 kg of peat and 550 kg CO\(_2\)-eq tonne\(^{-1}\) were emitted during peat life cycle. Considering the mass loss, saving from peat substitution were thus in the order of 183 kg CO\(_2\)-eq tonne\(^{-1}\) ww. As for the use of compost on land, an emission of 47 g N\(_2\)O tonne\(^{-1}\) ww from compost degradation was also assumed here. The results are summarized in Table 14.

Another composting technology was covered extensively in a Danish study (Boldrin et al., 2009a). A facility in Aarhus (Denmark) treated garden waste in an open windrow system with no gas treatment. The mass loss during composting was 28 %. The direct emissions consisted of fossil CO\(_2\) from diesel combustion during turning and gaseous emissions from degradation of the waste material. These have been measured at the site (Andersen et al., 2009) and the GWF of the direct emissions was 119 kg CO\(_2\)-eq tonne\(^{-1}\) ww (81 kg CO\(_2\)-eq tonne\(^{-1}\) ww for CH\(_4\) emissions, 30 kg CO\(_2\)-eq tonne\(^{-1}\) ww for N\(_2\)O emissions and 8 kg CO\(_2\)-eq tonne\(^{-1}\) ww from diesel combustion). The indirect upstream emissions were minor and only related to provision of diesel and electricity and added up to 1.2 kg CO\(_2\)-eq tonne\(^{-1}\) ww. Compost composition was: 82.7 kg C tonne\(^{-1}\), 5.1 kg N tonne\(^{-1}\), 1.3 kg P tonne\(^{-1}\) and 12.0 kg K tonne\(^{-1}\). The substitution ratios were assumed to be 20 % for N, 100 % for P and 100 % for K. Substitution of mineral fertilizers would save emissions in the order 7.3-25.7 kg CO\(_2\)-eq tonne\(^{-1}\) ww. N\(_2\)O emissions from application of compost on land were assumed to be 1.4 % of the applied nitrogen, equivalent to 51.3 g N\(_2\)O tonne\(^{-1}\) ww (i.e. 15.3 kg CO\(_2\)-eq tonne\(^{-1}\) ww). Carbon binding was 14 %, i.e. 30.6 kg CO\(_2\)-eq tonne\(^{-1}\) ww treated were saved. In modelling peat substitution, it was estimated that 1 tonne of compost could replace 292 kg of peat and 970 kg CO\(_2\)-eq tonne\(^{-1}\) were emitted during the life cycle of peat utilization (Boldrin et al., 2009b). Considering the mass loss, savings from peat substitution were thus in the order of 192 kg CO\(_2\)-eq tonne\(^{-1}\) ww. An emission of 51.3 g N\(_2\)O tonne\(^{-1}\) ww from compost degradation was here also assumed. The results are summarized in Table 14.

Table 4 summarizes the two examples representing different technologies (enclosed vs. open) and different waste types (biowaste vs. garden waste). Different indirect upstream GWFs reflect the lower use of energy in open systems, whilst the GWFs of the direct emissions demonstrate the benefits of treating the exhaust in enclosed systems. Greater savings from fertilizer substitution in the Dutch case are due to both a higher content of nutrients in biowaste and the higher utilization rate for nitrogen assumed in that specific study compared with the Danish case. Results for peat substitution are similar, despite different assumptions.
Table 11 - Greenhouse gas account and global warming contribution for open composting technologies (values expressed per tonne of wet waste (ww) composted).

<table>
<thead>
<tr>
<th>Indirect: Upstream</th>
<th>Direct: Waste Management</th>
<th>Indirect: Downstream</th>
</tr>
</thead>
<tbody>
<tr>
<td>GWF (kg CO₂ eq tonne⁻¹ ww):</td>
<td>GWF (kg CO₂ eq tonne⁻¹ ww):</td>
<td>GWF (kg CO₂ eq tonne⁻¹ ww):</td>
</tr>
<tr>
<td>0.2 to 4.4 (low)</td>
<td>3 to 242</td>
<td>-145 to +19 (use on land)</td>
</tr>
<tr>
<td>0.2 to 20 (high)</td>
<td></td>
<td>-880 to +44 (peat)</td>
</tr>
<tr>
<td>CO₂ eq (kg tonne⁻¹ ww):</td>
<td>CO₂ eq (kg tonne⁻¹ ww):</td>
<td>CO₂ eq (kg tonne⁻¹ ww):</td>
</tr>
<tr>
<td>• Diesel provision: 0.16 to 2.4 (GWP: 1)</td>
<td>• CO₂-biogenic: 0 (GWP: 0)</td>
<td>• Use on land:</td>
</tr>
<tr>
<td>• Electricity provision (GWP: 1):</td>
<td>• CH₄ emissions: 0.8 to 169 (GWP: 25)</td>
<td>• Provision of diesel: 0.1 to 0.25 (GWP: 1)</td>
</tr>
<tr>
<td>o 0.002 to 2 (low)</td>
<td>• N₂O emissions: 2.2 to 73 (GWP: 298)</td>
<td>• CO₂-fossil from diesel combustion: 0.5 to 1.6 (GWP: 1)</td>
</tr>
<tr>
<td>o 0.02 to 18 (high)</td>
<td>• CO₂-fossil from diesel combustion: 1 to 16 (GWP: 1)</td>
<td>• CO₂-biogenic: 0 (GWP: 0)</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Mineral fertilizer substituted: -4 to -81 (GWP: 1)</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• N₂O emissions: -42 to 88 (GWP: 298)</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Carbon binding: -2 to -79 (GWP: -1)</td>
</tr>
<tr>
<td></td>
<td></td>
<td><strong>OR</strong></td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Peat substitution:</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• CO₂-biogenic: 0 (GWP: 0)</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Peat substitution: -44 to -838 (GWP: 1)</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• N₂O emissions: -42 to 88 (GWP: 298)</td>
</tr>
<tr>
<td></td>
<td></td>
<td><strong>OR</strong></td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Peat substitution:</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• CO₂-biogenic: 92 to 566 kg</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Peat substitution: 80 to 700 kg</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• N₂O emissions: -0.14 to 0.3 kg</td>
</tr>
</tbody>
</table>

Accounted (unit tonne⁻¹ ww):
- Provision of diesel: 0.4 to 6.0 l
- Provision of electricity: 0.02 to 19.7 kWh
- CO₂-biogenic: 43 to 413 kg
- CH₄ from process: 0.03 to 6.8 kg
- N₂O from process: 7.5 to 252 g
- Combustion of diesel: 0.4 to 6.0 l
- Use of electricity: 0.02 to 19.7 kWh

Accounted (unit tonne⁻¹ waste):
- Use on land:
  - Combustion of diesel: 0.2 to 0.6 l
  - CO₂-biogenic: 220 to 1217 kg
  - Fertilizer substitution: 0.5 to 5.2 kg N, 0.6 to 2.8 kg P, 2.4 to 9.7 kg K
  - N₂O emissions: -0.14 to 0.3 kg
  - Carbon binding: 1 to 22 kg
- Peat substitution:
  - CO₂-biogenic: 92 to 566 kg
  - Peat substitution: 80 to 700 kg
  - N₂O emissions: -0.14 to 0.3 kg

Not accounted:
- Construction of composting facility
- Bulking agents
- Provision of other materials (oil, detergents, lubricants etc.)
- Any trace gas release
- Landscaping material substitution
- Incineration of screened residues
- Landfilling of screened residues
- Landfilling of compost
- Improved soil quality
Table 12 - Greenhouse gas account and global warming contribution for enclosed composting technologies (values expressed per tonne of wet waste (ww) composted).

<table>
<thead>
<tr>
<th>Indirect: Upstream</th>
<th>Direct: Waste Management</th>
<th>Indirect: Downstream</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>GWF (kg CO₂-eq tonne⁻¹ ww):</strong></td>
<td><strong>GWF (kg CO₂-eq tonne⁻¹ ww):</strong></td>
<td><strong>GWF (kg CO₂-eq tonne⁻¹ ww):</strong></td>
</tr>
<tr>
<td>1 to 8 (low)</td>
<td>5 to 81</td>
<td>-145 to +19 (use on land)</td>
</tr>
<tr>
<td>8.2 to 60 (high)</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**CO₂-eq (kg tonne⁻¹ ww):**
- Diesel provision: 0.05 to 1.2 (GWP: 1)
- Electricity provision (GWP: 1):
  - 0.9 to 6.5 (low)
  - 8.1 to 58.5 (high)
- Use on land:
  - Provision of diesel: 0.1 to 0.25 (GWP: 1)
  - CO₂-fossil from diesel combustion: 0.5 to 1.6 (GWP: 1)
  - CO₂-biogenic: 0 (GWP: 0)
  - Mineral fertilizer substituted: 0.1 to 1 (GWP: 1)
  - N₂O emissions: -0.1 to -0.2 (GWP: 298)
  - Carbon binding: -2 to -79 (GWP: -1)
- Peat substitution:
  - CO₂-biogenic: -92 to -566 kg
  - Peat substitution: -80 to -700 kg
  - N₂O emissions: -0.14 to -0.1 kg
  - Carbon binding: 1 to 22 kg

**Accounted:**
- Provision of diesel: 0.13 to 3 l
- Provision of electricity: 9 to 65 kWh
- CO₂-biogenic: 250 to 390 kg
- CH₄ emissions: 0.2 to 1.8 kg
- N₂O from process: 10 to 120 g
- Combustion of diesel: 0.13 to 3.3 l
- Use of electricity: 9 to 65 kWh
- CO₂-fossil from diesel combustion: 0.4 to 8.0 (GWP: 1)
- Use on land:
  - Provision of diesel: 0.1 to 0.25 (GWP: 1)
  - CO₂-fossil from diesel combustion: 0.5 to 1.6 (GWP: 1)
  - CO₂-biogenic: 0 (GWP: 0)
  - Mineral fertilizer substituted: 0.1 to 1 (GWP: 1)
  - N₂O emissions: -0.1 to -0.2 (GWP: 298)
  - Carbon binding: -2 to -79 (GWP: -1)

**Not accounted:**
- Construction of composting facility
- Bulking agents
- Provision of other materials (oil, detergents, lubricants etc.)
- Landscaping material substitution
- Incineration of screened residues
- Landfilling of screened residues
- Landfilling of compost
- Improved soil quality

**CO₂-eq (kg tonne⁻¹ ww):**
- CO₂-biogenic: 0 (GWP: 0)
- CH₄ emissions: 5 to 46 (GWP: 25)
- N₂O emissions: 0.3 to 35 (GWP: 298)
- CO₂-fossil from diesel combustion: 0.4 to 8.0 (GWP: 1)
- Use on land:
  - Provision of diesel: 0.1 to 0.25 (GWP: 1)
  - CO₂-fossil from diesel combustion: 0.5 to 1.6 (GWP: 1)
  - CO₂-biogenic: 0 (GWP: 0)
  - Mineral fertilizer substituted: -4 to -82 (GWP: 1)
  - N₂O emissions: -42 to 88 (GWP: 298)
  - Carbon binding: -2 to -79 (GWP: -1)
- Peat substitution:
  - CO₂-biogenic: -92 to -566 kg
  - Peat substitution: -80 to -700 kg
  - N₂O emissions: -0.14 to -0.1 kg
  - Carbon binding: 1 to 22 kg
- Peat substitution:
  - CO₂-biogenic: 92 to 566 kg
  - Peat substitution: 80 to 700 kg
  - N₂O emissions: -0.14 to -0.1 kg
Table 13 - Greenhouse gas account and global warming contribution for home composting (values expressed per tonne of wet waste (ww) composted).

<table>
<thead>
<tr>
<th></th>
<th>Indirect: Upstream</th>
<th>Direct: Waste Management</th>
<th>Indirect: Downstream</th>
</tr>
</thead>
<tbody>
<tr>
<td>GWF (kg CO₂-eq tonne⁻¹ ww):</td>
<td>0</td>
<td>77 to 220</td>
<td>-146 to +17 (use on land) -880 to +44 (peat)</td>
</tr>
<tr>
<td>CO₂- eq (kg tonne⁻¹ ww):</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>• CO₂-biogenic:</td>
<td>0 (GWP: 0)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>• CH₄ emissions:</td>
<td>20 to 55 (GWP: 25)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>• N₂O emissions:</td>
<td>57 to 165 (GWP: 298)</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Accounted (unit tonne⁻¹ ww):
- CO₂-biogenic: 139 to 215 kg
- CH₄ from process: 0.8 to 2.2 kg
- N₂O from process: 0.2 to 0.5 kg

Accounted (unit tonne⁻¹ ww):
- Use on land:
  - CO₂-biogenic: 220 to 1217 kg
  - Fertilizer substitution: 0.5 to 5.2 kg N, 0.6 to 2.8 kg P, 2.4 to 9.7 kg K
  - N₂O emissions: -0.14 to 0.3 kg
  - Carbon binding: 1 to 22 kg

OR
- Peat substitution:
  - CO₂-biogenic: 92 to 566 kg
  - Peat substitution: 80 to 700 kg
  - N₂O emissions: -0.14 to 0.3 kg

Not accounted:
- Construction of plastic composter and plastic bucket
- Any trace gas release

Table 14 – Summary of two examples described in the text.

<table>
<thead>
<tr>
<th>Example</th>
<th>Technology</th>
<th>Waste type</th>
<th>Indirect: Upstream</th>
<th>Direct: Waste Management</th>
<th>Indirect: Downstream</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>GWF (kg CO₂-eq tonne⁻¹ ww)</td>
<td>GWF (kg CO₂-eq tonne⁻¹ ww)</td>
<td>GWF (kg CO₂-eq tonne⁻¹ ww)</td>
</tr>
<tr>
<td>Dutch LCA</td>
<td>86 % enclosed facilities</td>
<td>Household biowaste</td>
<td>3.2 (low)</td>
<td>28.8 (high)</td>
<td>35</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>-22.4 to -46.1 (fertilizer) -169 (peat)</td>
</tr>
<tr>
<td>Århus assessment</td>
<td>Windrow composting</td>
<td>Garden waste</td>
<td>1.2</td>
<td>119</td>
<td>-22.6 to -41 (fertilizer) -177 (peat)</td>
</tr>
</tbody>
</table>
5. Conclusions
The GHG accounting for composting of organic waste shows that the contribution to GW depends on several factors, suggesting that the overall emission factor for composting may vary between significant savings (-800 kg CO₂-eq tonne⁻¹ ww) to a net load (300 kg CO₂-eq tonne⁻¹ ww). Significant factors are off-gas cleaning at the composting plant (only possible for enclosed systems) and the use of the compost. The major savings are obtained by use of compost as a substitute for peat in the production of growth media. Garden waste composting generates the most compost per tonne of waste composted and thus may obtain the most savings.

The survey and methodological approach shows how GHGs can be counted for composting. Upstream activities contribute very little and the direct contributions from the composting plant are moderate, in particular if the off-gasses from the facility are treated prior to discharge. The main loads and main savings – and often the latter exceed the former - come from the use of the compost. Although the cases presented shows how these contributions can be calculated, the estimates are associated with extensive uncertainty. Often the use of the compost and what the compost substitutes for are not well known. The principal issues are known but no statistics are available. In addition, the release of N₂O from the compost as it is being used is not well documented and, similarly, the avoided emissions are not well quantified: some authors suggest net savings of N₂O when using compost instead of mineral fertilizers, some others report loads to the environment. The main learning may be that it is extremely important that the compost is used in a rational way substituting for the production and use of other materials (fertilizer and peat) in order to obtain the global warming benefits of composting organic waste.

6. Acknowledgments
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