



Uncertainty quantification of critical speed for railway vehicle dynamics

Bigoni, Daniele

Publication date:
2012

Document Version
Publisher's PDF, also known as Version of record

[Link back to DTU Orbit](#)

Citation (APA):
Bigoni, D. (2012). Uncertainty quantification of critical speed for railway vehicle dynamics. Sound/Visual production (digital)

General rights

Copyright and moral rights for the publications made accessible in the public portal are retained by the authors and/or other copyright owners and it is a condition of accessing publications that users recognise and abide by the legal requirements associated with these rights.

- Users may download and print one copy of any publication from the public portal for the purpose of private study or research.
- You may not further distribute the material or use it for any profit-making activity or commercial gain
- You may freely distribute the URL identifying the publication in the public portal

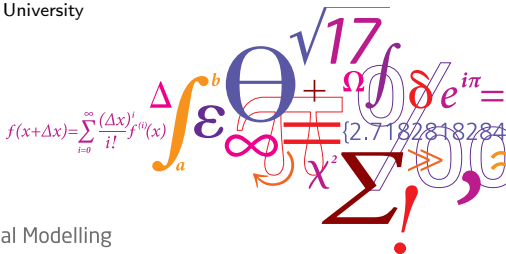
If you believe that this document breaches copyright please contact us providing details, and we will remove access to the work immediately and investigate your claim.

Uncertainty quantification of critical speed for railway vehicle dynamics

PhD student: D. Bigoni¹

Supervisors: A. P. Engsig-Karup¹, H. True¹, J.S. Hesthaven²

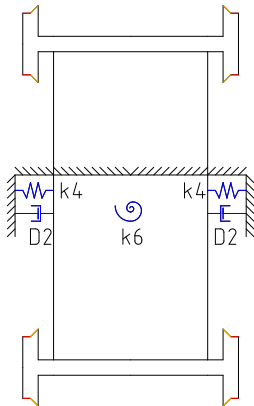
¹The Technical University of Denmark, ²Brown University



Railway vehicle dynamics - Euler's formulation¹

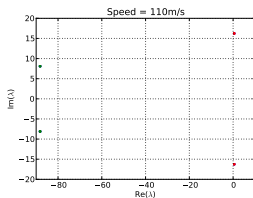
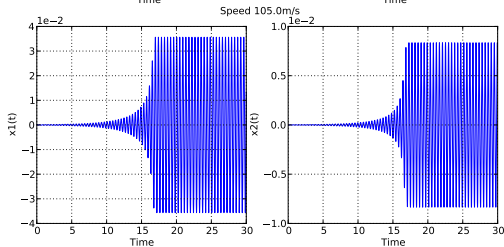
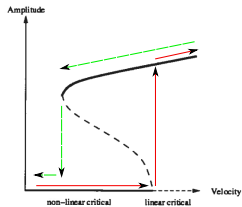
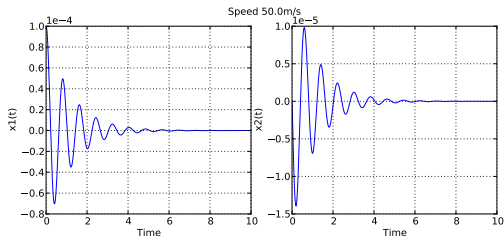
$$\begin{aligned}
 m\ddot{\vec{x}}_1 + 2D_2\dot{\vec{x}}_1 + 2k_4\vec{x}_1 + 2F_X(\xi_{x1}, \xi_{y1}) + 2F_X(\xi_{x2}, \xi_{y2}) &= 0 \\
 I\ddot{\vec{x}}_2 + k_6\vec{x}_2 + 2ha [F_X(\xi_{x1}, \xi_{y1}) - F_X(\xi_{x2}, \xi_{y2})] + \\
 + a [F_Y(\xi_{x1}, \xi_{y1}) + F_Y(\xi_{x2}, \xi_{y2})] &= 0
 \end{aligned}$$

where F_X and F_Y are the creep forces, and determine a non-linear coupling of \vec{x}_1 and \vec{x}_2 . Among other components, these forces involve also the running velocity v of the vehicle, the conicity of the wheels and the wheel-rail friction.



¹H.True and C.Kaas-Petersen 1983

Railway vehicle dynamics - Hunting



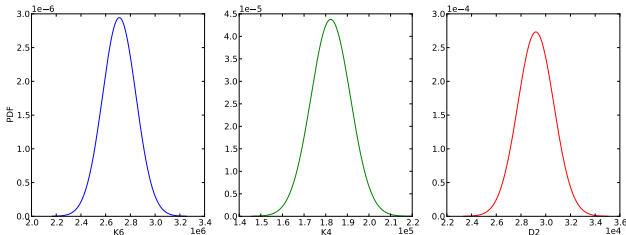
Railway vehicle dynamics - Stochastic Model

Let's now assume that the suspension components k_6 , k_4 and D_2 are known within a certain level of accuracy and model this by:

$$k_6 \sim \mathcal{N}(3.44 \cdot 10^6, 2.96 \cdot 10^{10}), \quad (\text{std. of approx. } 5\%)$$

$$k_4 \sim \mathcal{N}(9.12 \cdot 10^4, 4.15 \cdot 10^7), \quad (\text{std. of approx. } 7\%)$$

$$D_2 \sim \mathcal{N}(1.46 \cdot 10^4, 1.07 \cdot 10^6), \quad (\text{std. of approx. } 7\%)$$



What are the dynamics of the system under these conditions?

Uncertainty Quantification - Traditional Approaches

Analytical Methods

- Moment Equation

- Perturbation Method

Pros.: recover the exact solution

Cons.: problem-dependent, cumbersome

Sampling Methods

- (MC) Monte Carlo – $\mathcal{O}(N^{-1/2})$

- (QMC) Quasi Monte Carlo – $\mathcal{O}\left((\log N)^d / \sqrt{N}\right)$

- (MCMC) Markov Chain Monte Carlo

Pros.: general applicability, MC convergence independent from dimensionality d

Cons.: very slow convergence

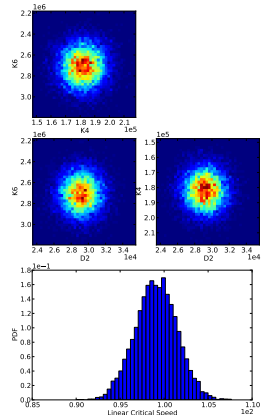


Figure: Linear critical speed distribution using 10^4 realizations for MC method.

UQ - Generalized Polynomial Chaos (gPC)²

Let Y be a r.v. with CDF $F_Y(y)$. Use the N th-degree gPC expansion of the random parameters and the solution

$$Y_N = \sum_{k=0}^N \hat{a}_k \Phi_k(Z), \quad \hat{a}_k = \frac{1}{\gamma_k} \int_{I_Z} F_Y^{-1}(F_Z(z)) \Phi_k(z) dF_Z(z)$$

$$u_N(t, Z) = \sum_{k=0}^N \hat{u}_k(t) \Phi_k(Z)$$

$$\begin{cases} \mathbb{E} [\partial_t u_N(t, Z) \Phi_k(Z)] = \mathbb{E} [f(u_N) \Phi_k(Z)], & D \times (0, T] \\ \hat{u}_k(0) = \frac{1}{\gamma_k} \mathbb{E} [u(0, Z) \Phi_k(Z)], & D \times \{t = 0\} \end{cases}$$

$$\mu_u(t) \approx \mathbb{E} [u_N(t, Z)] = \hat{u}_0(t)$$

$$\mathbf{Var} [u(t, Z)] \approx \mathbf{Var} [u_N(t, Z)] = \sum_{k=1}^N \gamma_k \hat{u}_k^2(x, t)$$

where $\mathbb{E} [f(Z)] = \int_{I_Z} f(z) dF_Z(z)$ and $\{\phi_i(Z)\}_{i=0}^N$ are **proper** orthonormal basis.

²D.Xiu and G.Karniadakis 2004

UQ - gPC on Railway Vehicle Dynamics

The N -th order gPC expansion of the problem is given by

$$\begin{cases} \mathbb{E} [\partial_t u_{1,N} \phi_k] = \mathbb{E} [u_{2,N} \phi_k] \\ \mathbb{E} [\partial_t u_{2,N} \phi_k] = -2\mathbb{E} [D_{2,N} u_{2,N} \phi_k] - 2\mathbb{E} [k_{4,N} u_{1,N} \phi_k] \\ \quad - 2\mathbb{E} [(F_X(\xi_{x1}, \xi_{y1}) + F_X(\xi_{x2}, \xi_{y2})) \phi_k] \\ \mathbb{E} [\partial_t u_{3,N} \phi_k] = \mathbb{E} [u_{4,N} \phi_k] \\ \mathbb{E} [\partial_t u_{4,N} \phi_k] = -\mathbb{E} [k_{6,N} u_{3,N} \phi_k] - 2ha\mathbb{E} [(F_X(\xi_{x1}, \xi_{y1}) - F_X(\xi_{x2}, \xi_{y2})) \phi_k] \\ \quad - a\mathbb{E} [(F_Y(\xi_{x1}, \xi_{y1}) + F_Y(\xi_{x2}, \xi_{y2})) \phi_k] \end{cases}$$

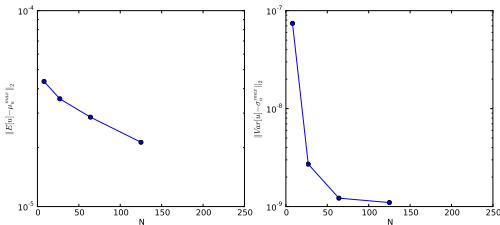
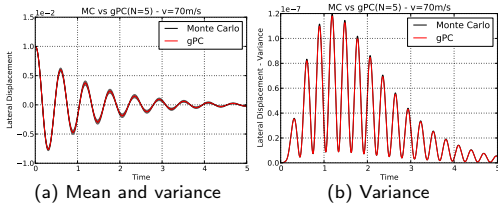
where k is a multi index such that

$$u_{i,N}(t, Z) = \sum_{|k| \leq N} \hat{u}_k(t) \Phi_k(Z), \quad i = 1, \dots, 4$$

We obtain a system of $K = \sum_{i=0}^N \binom{i+(d-1)}{(d-1)}$ coupled equations that can be treated using standard ODE solvers. The following table shows how this number scales:

| N | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|---------|---|----|----|-----|-----|-----|-----|
| $d = 1$ | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| $d = 2$ | 3 | 6 | 10 | 15 | 21 | 28 | 36 |
| $d = 3$ | 4 | 10 | 20 | 35 | 56 | 84 | 120 |
| $d = 4$ | 5 | 15 | 35 | 70 | 126 | 210 | 330 |
| $d = 5$ | 6 | 21 | 56 | 126 | 252 | 462 | 792 |

UQ - gPC on Railway Vehicle Dynamics



Pros: Elegant formulation, one single solution of the system, optimal accuracy

Cons: Intrusive and cumbersome to implement, non-linearities must be treated carefully, **weak on time-dependent problems** (but there exist improvements).

UQ - Probabilistic Collocation Methods (PCM)

Solve the deterministic ODE on a "proper" set $\Theta_M = \{Z^{(j)}\}_{j=1}^M$ of nodes in the random space:

$$\begin{cases} \partial_t u(t, Z^{(j)}) = f(u), & D \times (0, T] \\ u(0) = u_0, & D \times \{t = 0\} \end{cases}$$

This will give $u^{(j)} = u(t, Z^{(j)})$ solutions on which we can apply interpolation rules or projection rules. Let's consider the discrete projection:

$$u_N(Z) = \sum_{|k| \leq N} \hat{u}_k(t) \Phi_k(Z)$$

$$\hat{u}_k(t) = \frac{1}{\gamma_k} \mathbb{E}[u(t, Z) \phi_k(Z)] = \frac{1}{\gamma_k} \int u(z) \phi_k(z) dF_Z(z)$$

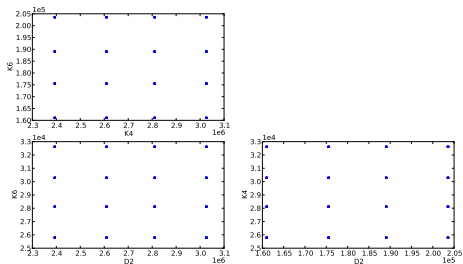
where the integral can be computed by cubature rules using the "properly" selected set of nodes Θ_M . Then statistics can be easily obtained:

$$\mu_u(t) \approx \mathbb{E}[u_N(t, Z)] = \hat{u}_0(t)$$

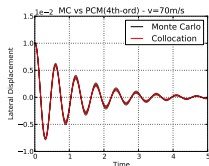
$$\mathbf{Var}[u(t, Z)] \approx \mathbf{Var}[u_N(t, Z)] = \sum_{|k| \leq N} \gamma_k \hat{u}_k^2(x, t)$$

Target: **obtain the "best" statistics out of the smallest number of simulation!**

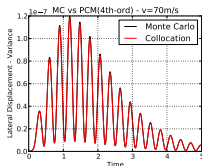
UQ - PCM on Railway Vehicle Dynamics



(c) Collocation points, $N = 3$



(d) Mean and variance



(e) Variance

Figure: PCM vs. Monte Carlo

Hermite polynomials are chosen as basis for the projection/cubature. Projection with these polynomials can be highly accurate, using proper Gauss quadrature nodes and weights, for which analytical formulas exist.

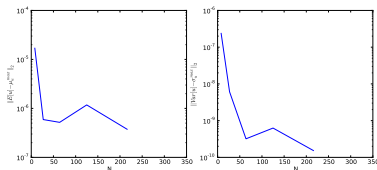
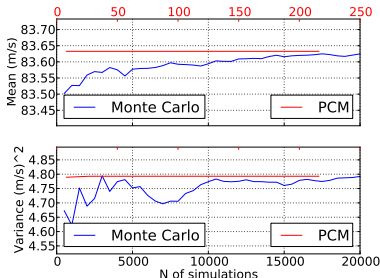
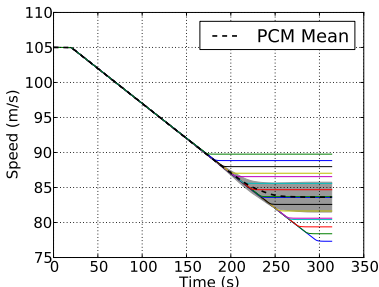


Figure: PCM convergence to highest accuracy (mean and variance).

UQ - PCM for Critical Speed statistics

Let's extend the dynamical system in order to obtain a "controlled" ramping method:

$$\begin{cases} \ddot{u}_1 = \ddot{u}_2 \\ m\ddot{u}_2 = -2D_2\dot{u}_2 - 2k_4\dot{u}_1 - 2F_X(\xi_{x1}, \xi_{y1}) - 2F_X(\xi_{x2}, \xi_{y2}) \\ \ddot{u}_3 = \ddot{u}_4 \\ I\ddot{u}_4 = -k_6\dot{u}_3 - 2ha [F_X(\xi_{x1}, \xi_{y1}) - F_X(\xi_{x2}, \xi_{y2})] - \\ \quad - a [F_Y(\xi_{x1}, \xi_{y1}) + F_Y(\xi_{x2}, \xi_{y2})] \\ \dot{v} = \begin{cases} 0 & \text{if } t < t_{st} \vee \|\vec{u}\|_2 < \varepsilon_{min} \\ -\|\vec{u}\|_2 & \text{if } \|\vec{u}\|_2 < \varepsilon_{max} \\ -\varepsilon_{max} & \text{otherwise} \end{cases} \end{cases}$$



Outlook - Future work

UQ on **Railway vehicle dynamics**

- Uncertainty quantification with Sparse Grids
- Uncertainty quantification on a realistic model
- Parameter space compression and compressed sensing

UQ on **Free Water Wave Dynamics**

- Parametrization of random fields

Other applications of Uncertainty Quantification