Stellar aberration correction and thermoelastic compensation of Swarm μASC attitude observations: A comment to the Express Letter “Mysterious misalignments between geomagnetic and stellar reference frames seen in CHAMP and Swarm satellite measurements”, by Stefan Maus

Herceg, M.; Jørgensen, P. S.; Jørgensen, J. L.

Published in:
Geophysical Journal International

Link to article, DOI:
10.1093/gji/ggx285

Publication date:
2017

Document Version
Publisher's PDF, also known as Version of record

Citation (APA):
Stellar aberration correction and thermoelastic compensation of Swarm \( \mu \text{ASC} \) attitude observations
A comment to the Express Letter “Mysterious misalignments between geomagnetic and stellar reference frames seen in CHAMP and Swarm satellite measurements”, by Stefan Maus

M. Herceg, P.S. Jørgensen and J.L. Jørgensen
DTU Space, Denmark Technical University, DK-2800 Kgs. Lyngby, Denmark. E-mail: mher@space.dtu.dk

Accepted 2017 July 4. Received 2017 June 30; in original form 2017 May 9

SUMMARY
The Swarm constellation of three satellites measures the magnetic signal of the Earth using both a Vector Field Magnetometer and an Absolute Scalar Magnetometer. A Micro Advanced Stellar Compass (\( \mu \text{ASC} \)) mounted on a common, supposedly stable, optical bench precisely determines its inertial attitude. However, comparison of the Inter Boresight Angle shows a relative attitude variation between the \( \mu \text{ASC} \) Camera Head Units. These misalignments between Camera Head Units and a geomagnetic reference frame cannot be explained by incorrect aberration correction (as theorized by Maus). Herceg et al. found them to be caused by thermal gradient sensitivity of the optical bench system, opposing the underlying assumption of perfect platform stability. The results after applying thermal corrections show significant decrease in root mean square, with Inter Boresight Angle of thermally corrected data being nearly flat and clean from any variation caused by thermoelastic effects.

Key words: Magnetic field; Satellite magnetics.

1 INTRODUCTION
The Swarm mission satellites measure the magnetic signal of the Earth using an Absolute Scalar Magnetometer (ASM) and a Vector Field Magnetometer (VFM). While the ASM measures magnetic field strength (and serves to calibrate the VFM instrument), the VFM measures the magnetic field vector. To precisely orient measured magnetic field vector, the three optical heads of the Micro Advanced Stellar Compass (\( \mu \text{ASC} \)) are mounted on the Swarm optical bench (OB) together with the VFM sensor. The \( \mu \text{ASC} \) is an entirely autonomous, internally redundant star tracker, designed and produced by the Measurement and Instrumentation Section at DTU Space Department, Denmark Technical University (Jørgensen et al. 2004). Being one of the most successful star trackers worldwide, the \( \mu \text{ASC} \) has been operating on many satellite missions, and even though subjected to very different orbital and thermal environments, not a single hardware or functional failure has ever occurred.

Swarm satellite orientation can, therefore, be determined from both magnetic field measurements and \( \mu \text{ASC} \) images. These independent measurements can be compared, and ideally, should agree. Maus (2015), these misalignments are associated with deficiencies in the software carrying out the star camera aberration correction, as one of the possible causes, while disregarding any potential thermally induced mechanical instability. To investigate the causes of these misalignments, a study was performed (Herceg et al. 2017) on Swarm relative Camera Head Units (CHU) orientation and its correlation with stellar aberration and thermal variation of the OB system.

The purpose of this comment paper is to summarize the findings given in Herceg et al. (2017) and to explain the misalignments between CHU and a geomagnetic reference frame presented in Maus (2015).

2 SWARM \( \mu \text{ASC} \) OBSERVATIONS
Each Swarm satellite is equipped with three CHU’s, placed on the OB such that the angles between the boresights, referred to as Inter Boresight Angle (IBA), are approximately 90° (Fig. 1). The IBA of each CHU pair is defined as the angle between the Z-axes of the two CHU’s.

The OB is an ultrastable silicon carbide–carbon fiber compound structure (Pereira & Rathband 2012) with the main purpose of
transference of the precisely determined \( \mu \text{ASC} \) attitude to the VFM. Prior to the Swarm launch, exhaustive thermomechanical analyses were carried out to ensure thermal and mechanical stability; however, this stability cannot be monitored directly in flight. Instead, an indirect approach for testing OB stability is used in which the thermal state of the OB is monitored and compared to the IBA variation. The thermal state is observed using the thermistors mounted on different parts of the OB, as shown in Fig. 1.

Before calculating IBA and comparison with thermal variation, attitudes obtained by the Swarm CHU’s have to be corrected for stellar aberration. Generally, the aberration correction is carried out automatically on-board. However, as the Swarm velocity information is not available immediately to the \( \mu \text{ASC} \) instrument, stellar aberration correction is applied on the ground during post-processing (contrary to the claim of Maus 2015). The details describing the algorithms for the Swarm data processing can be found in Tøffner-Clausen & Holmdahl Olsen (2015).

3 MODELLING OF THE THERMOELASTIC EFFECTS OF OPTICAL BENCH

The IBA is the most accurate relative comparison of the CHU stability. Therefore, it is used as a primary means of comparison in the further analysis. This choice is guided by the accuracy of measured orientation, which is highest in CHU pointing direction (along the camera boresight). In the analysis of the IBA stability, the root mean square (RMS) value of the data is used to assess the IBA stability. When comparing the IBA of aberration corrected with uncorrected attitude data, results show significant improvement in stability of the CHU’s (see Fig. 2 for Swarm Alpha results), where RMS of the IBAs is reduced by \( \sim 13 \) arc-seconds.

Ideally, the IBA of aberration corrected attitudes is expected to be constant. However, the IBA on Fig. 2 (red curve) shows a variation which is correlated with a periodicity of temperature observations (Fig. 3). The comparison shows that IBA variation of aberration corrected data has a thermal signature, which has maximum effect when the satellite orbit plane is dawn–dusk oriented (hottest configuration) and minimal in the noon–midnight orbit. The observed thermal variation is causing OB instability, and needs to be modelled using the OB thermistor data (Fig. 3). For that purpose, a thermal compensation model was derived as explained in Herceg et al. (2017).

The temperatures selected for thermal modelling are those observed by the CHU and OB thermistors (THT00029—next to the optical cube, and THT00032—Optical Bench I/F, see Fig. 1), to ensure the correct profile of the thermal gradient.

After applying the thermal correction, the comparison of aberration corrected and thermal corrected data is made (see Fig. 4 for Swarm Alpha, where green dashed line represents the period from 2014 June 16 to 2015 December 3 for which model was determined). Results for Swarm Alpha show the largest correction (Fig. 4) for the first (CHU A—CHU B) and the third (CHU B—CHU C) IBA pair. Both of these IBA pairs have CHU B in common, which indicates that the main correction is applied when CHU B is involved. The
reason for this might be CHU B placement on the OB, where the
CHU mounted on a very edge of the OB may cause such thermal
gradient signatures.

The RMS values given for each panel in Fig. 4 show results
of the complete data set and a version smoothed over 200 s win-
dows (to suppress short-term noise sources). The RMS of the IBA
pairs for Swarm Alpha is reduced down to 2.2 arc-seconds, with
IBA of thermally corrected data being virtually constant. The same
improvement is also notable for the corrected data outside of the
modelling period (green dashed lines on Fig. 4), where stability of
the IBA shows excellent results in thermal effects prediction. Fur-
thermore, the bias per CHU is assumed to be smaller than \( \frac{1}{\sqrt{2}} \) times value presented in Fig. 4, considering the IBAs RMS contains
measurements of two cameras.

As presented here, the aberration correction is performed cor-
correctly and residual IBA variation, which is apparently driven by
thermal gradients, can be adequately compensated by a thermal
model described in Herceg et al. (2017). These results are contrary
to the fundamental assumption in Maus (2015), where a perfect
OB system and a flawed aberration correction are used to explain
the observed IBA variations.

4 CONCLUSIONS

Periodical variations in relative CHU orientation on the Swarm
satellites are found to be caused by two phenomena: stellar aberra-
tion and thermoelastic effects of the OB. The \( \mu \) ASC attitude data are
not corrected for aberration on-board (although feasible), since the
spacecraft velocity information is not immediately available to the
instrument, and is, therefore, performed during ground data pro-
cessing. After aberration correction, the angle between the CHU
boresights (IBA) is expected to be in the one arc-second range.
However, a small, but significant signal remains in the IBA data,
which is found to be correlated with temperature variations (Herceg
et al. 2017). Therefore, an additional correction is applied on Swarm
\( \mu \) ASC attitude data for compensation of thermoelastic effects. The
results after thermal correction show a decrease in RMS for Swarm
Alpha down to 2.2 arc-seconds, with IBA of thermally corrected
data being virtually constant and clean from any thermally induced
phenomenon.

Contrary to the basic assumption in Maus (2015), where a perfect
OB system and a flawed aberration correction are used to explain
the observed IBA variations, this study proves that aberration cor-
rection is performed correctly and residual IBA variation can be
fully compensated by a simple thermoelastic model using on-board measured temperatures.

REFERENCES


