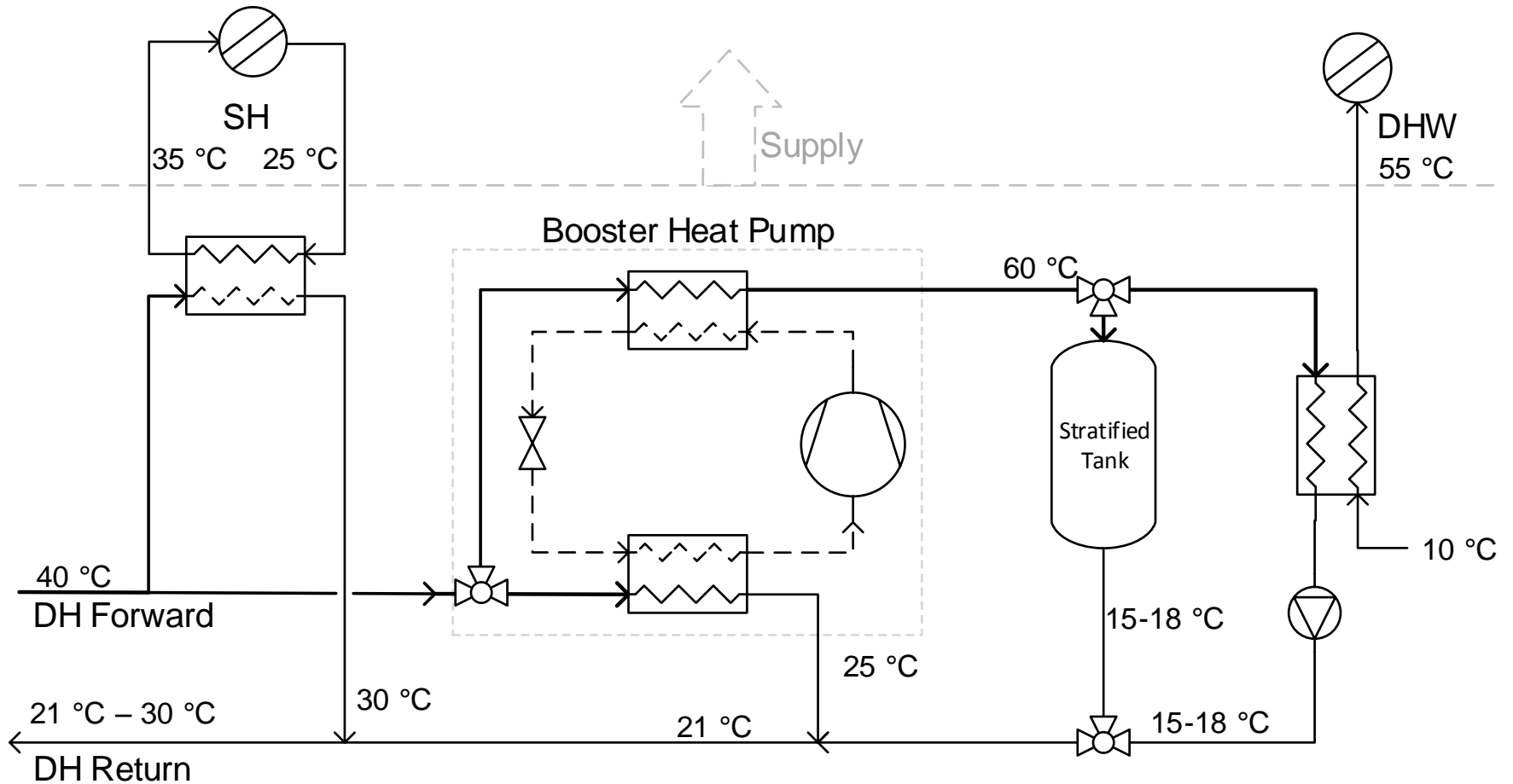




# Agenda

- Introduction
- Motivation for using mixed working fluids
- Booster HP
  - Working fluid screening
  - Economic evaluation
- Ultra low temperature district heating mixtures
  - Off design analysis
  - System performance (incl. central HP with mixtures)
- Conclusions

# Booster HP System

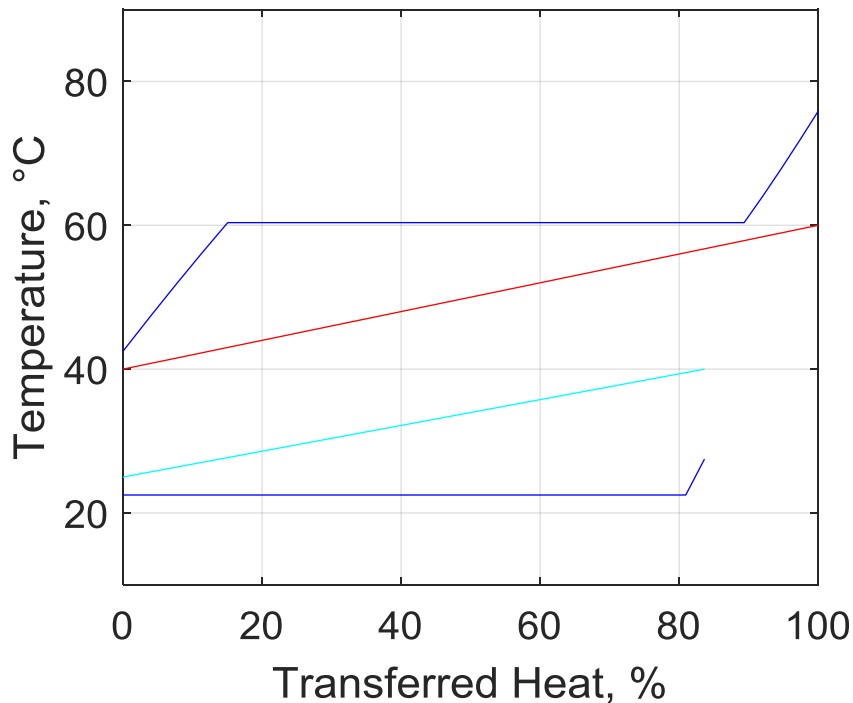


# Motivation

Heat Pump:

Heat Source: 40 °C → 25 °C

Heat Sink: 40 °C → 60 °C



R134a:

COP = 6.11

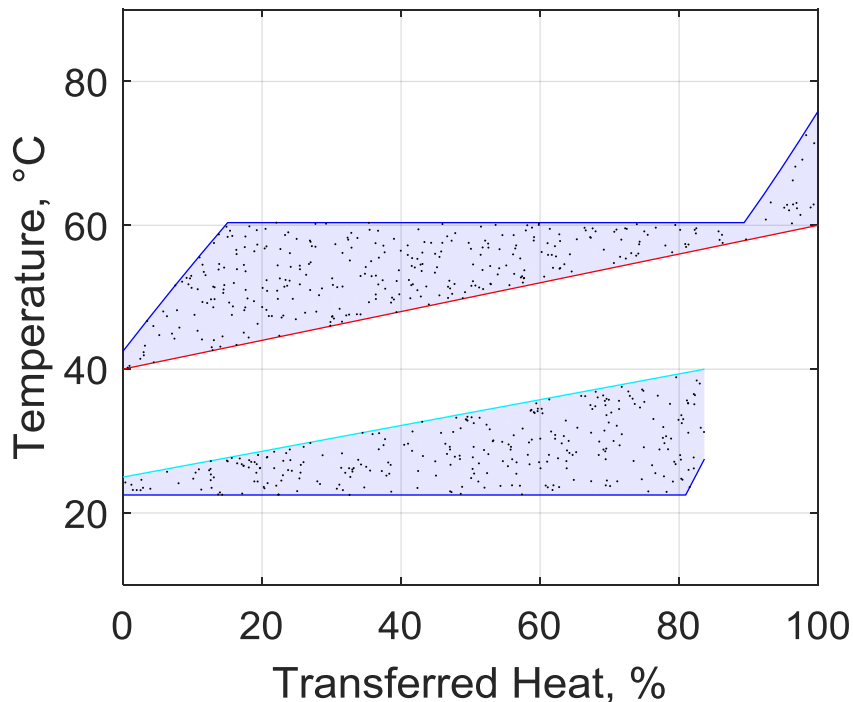
$p_{\text{evap}} = 6.17 \text{ bar}$ ,  $p_{\text{cond}} = 16.97 \text{ bar}$

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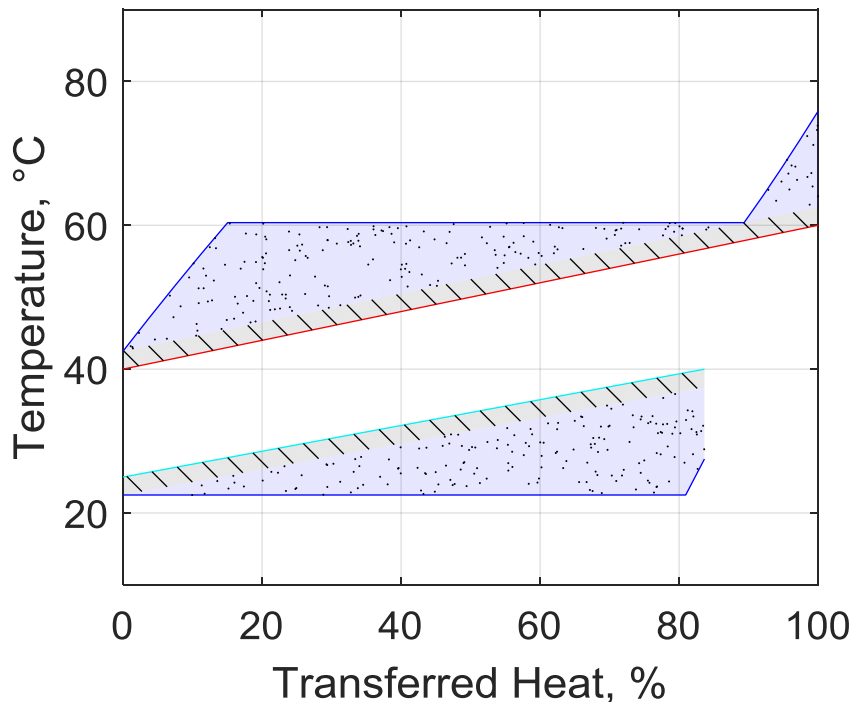
$y_{\text{D,source}}^* = 25 \%$ ,  $y_{\text{D,sink}}^* = 25 \%$

# Motivation

Heat Pump:

Heat Source: 40 °C → 25 °C

Heat Sink: 40 °C → 60 °C



R134a:

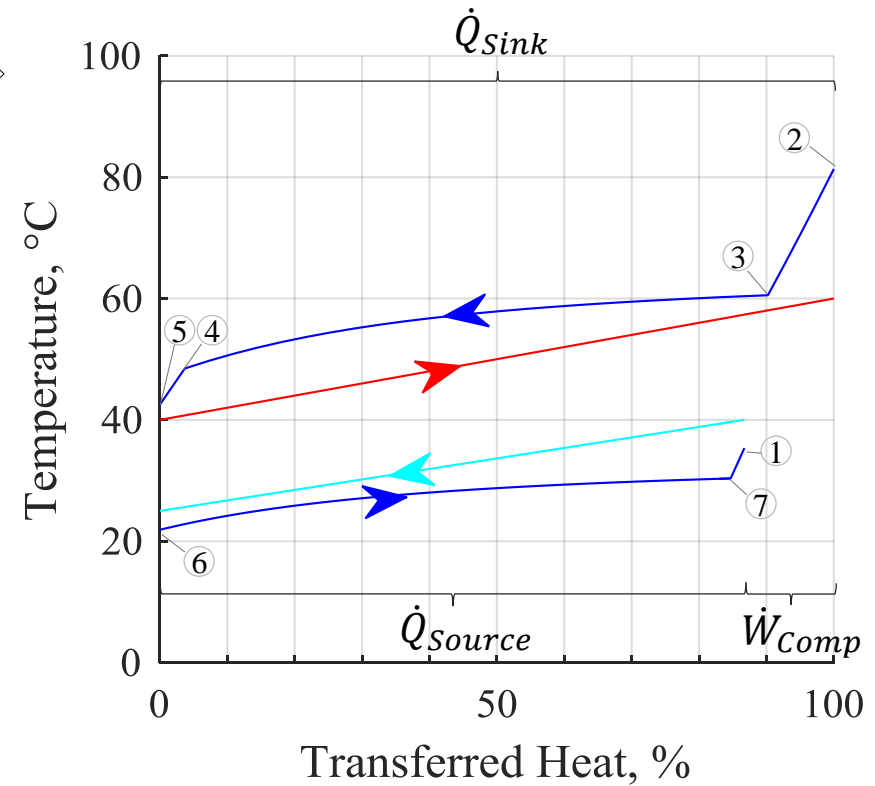
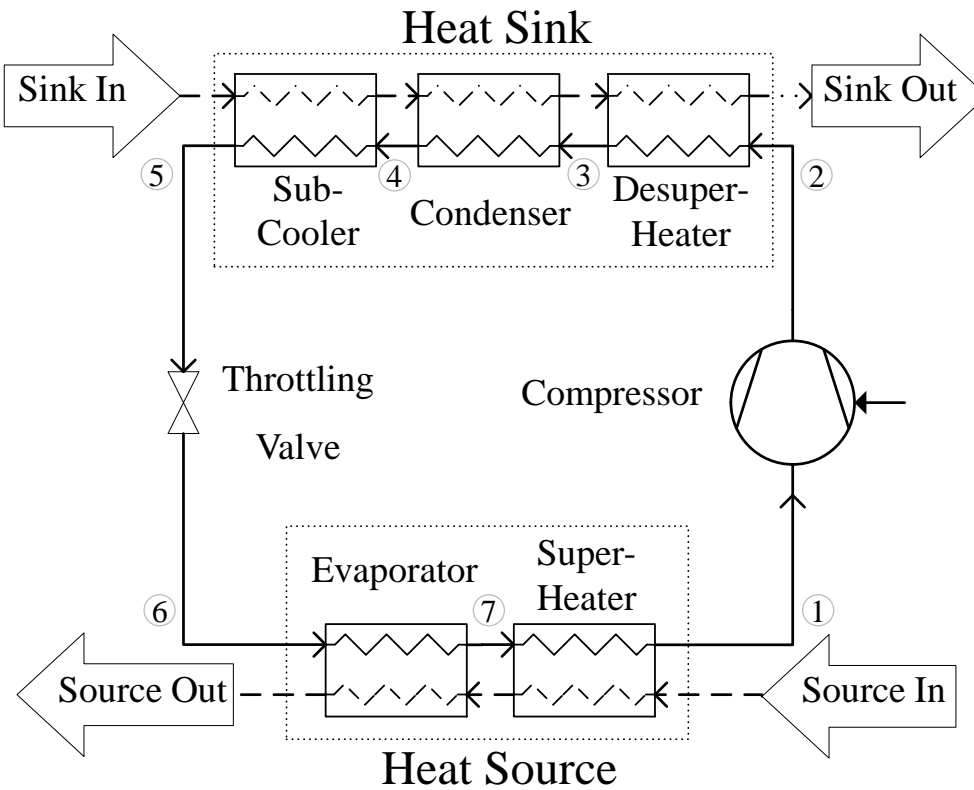
COP = 6.11

$p_{\text{evap}} = 6.17 \text{ bar}$ ,  $p_{\text{cond}} = 16.97 \text{ bar}$

$y_{\text{D,source}}^* = 25 \%$ ,  $y_{\text{D,sink}}^* = 25 \%$

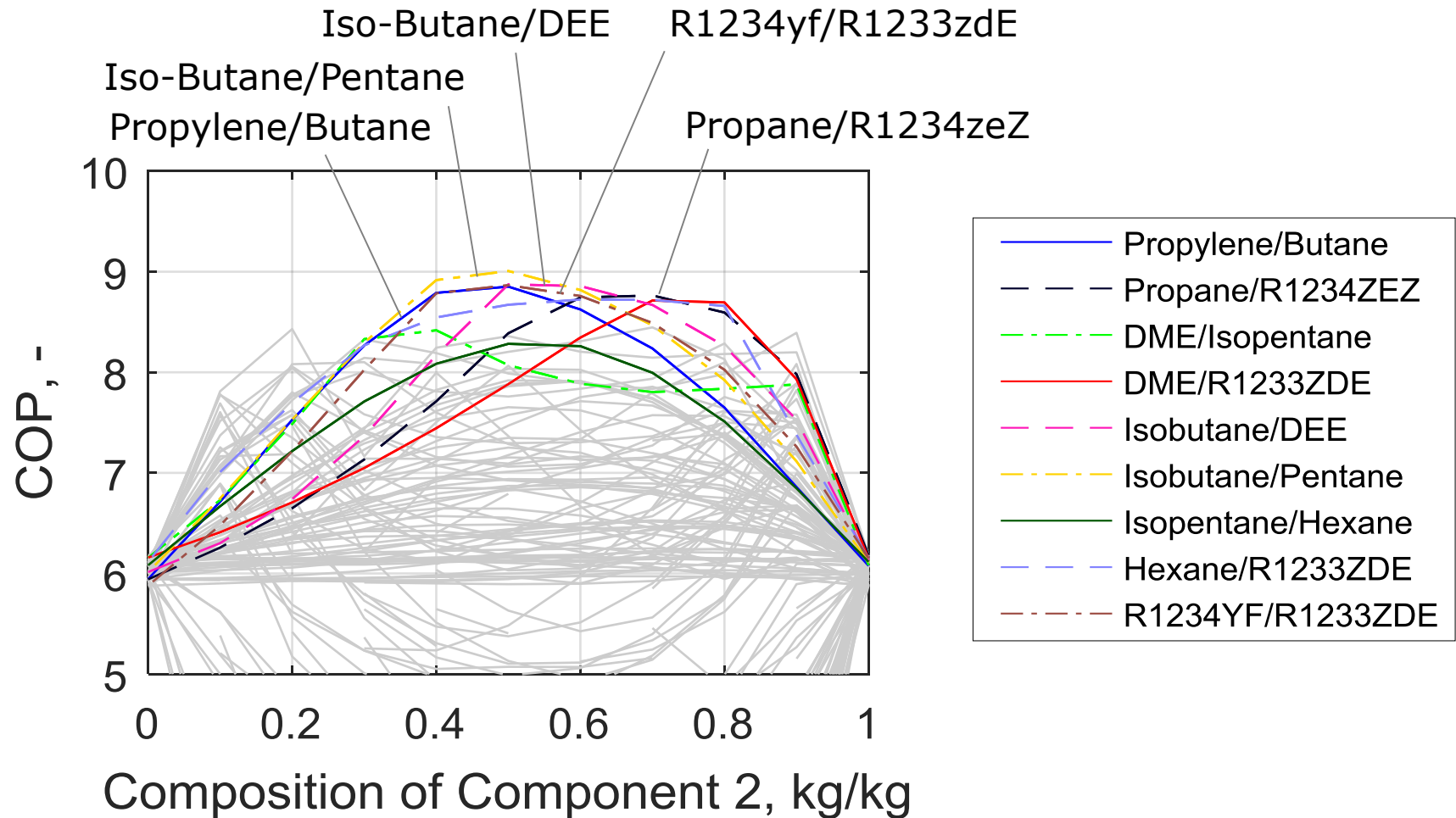
$y_{\text{D,source,Fluid}}^* = \mathbf{19 \%}$ ,  $y_{\text{D,sink,Fluid}}^* = \mathbf{19 \%}$

# Working Fluid Screening: Thermodynamic Model



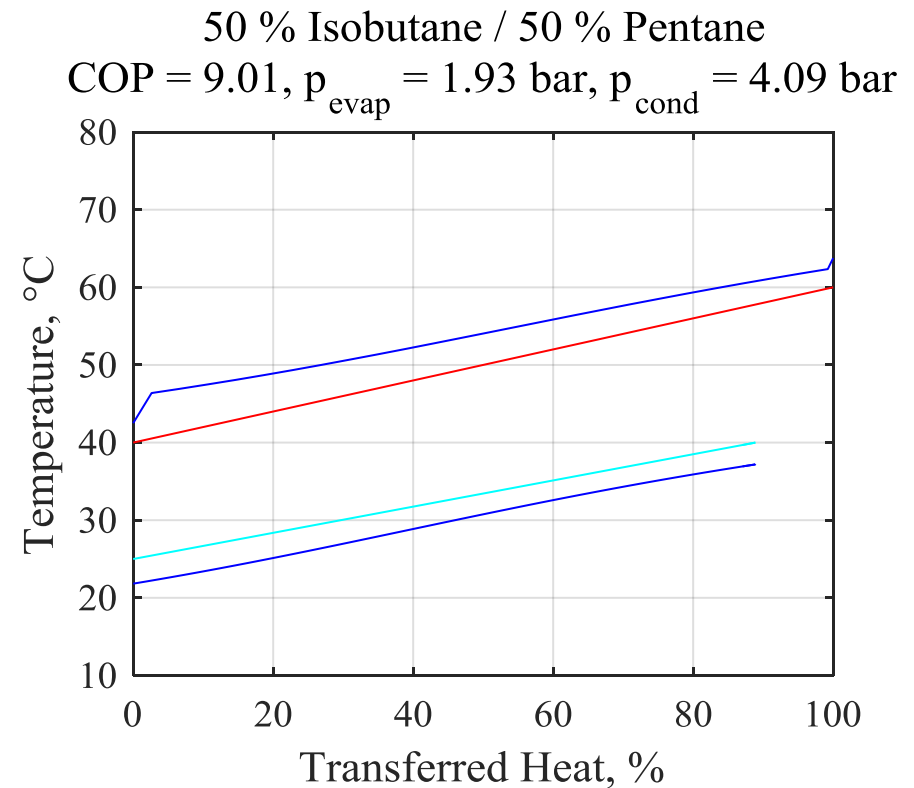
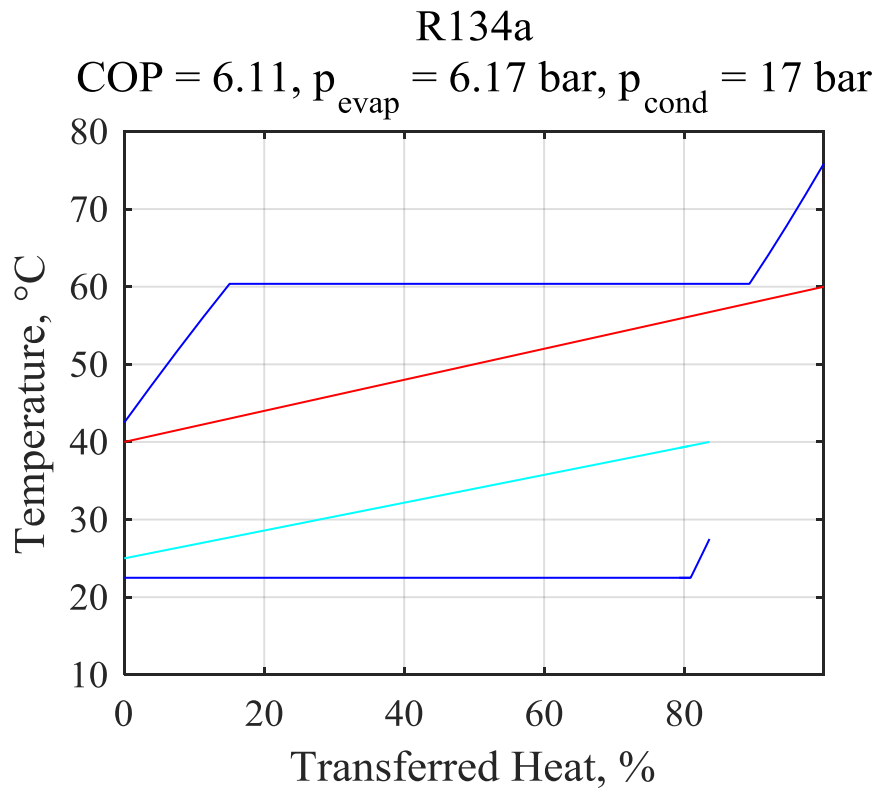
→ Simulation of all possible binary mixtures, considering 14 HCs + 4 HFOs

# Working Fluid Screening: Results (0 K min. Super Heating)





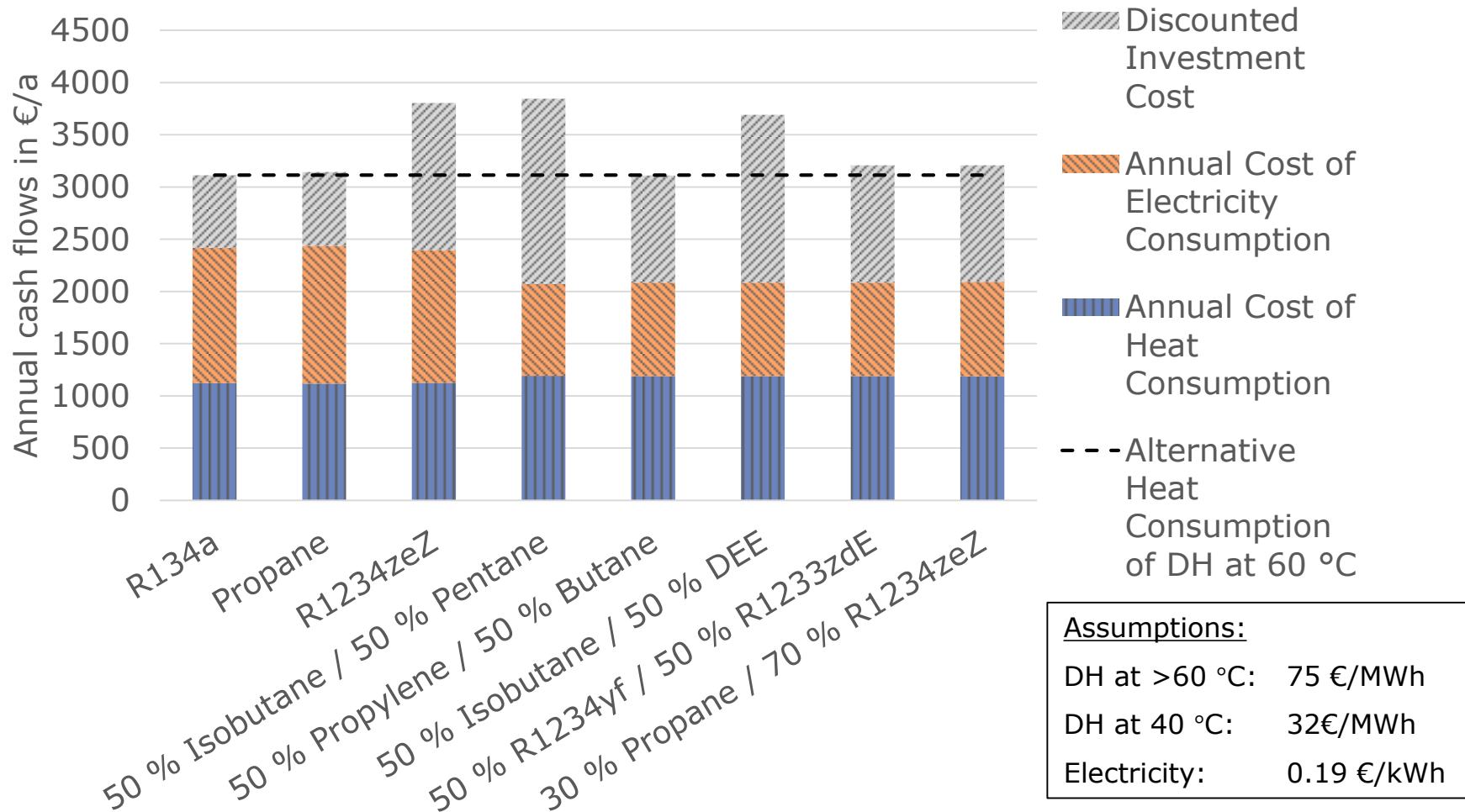
# Working Fluid Screening: Results



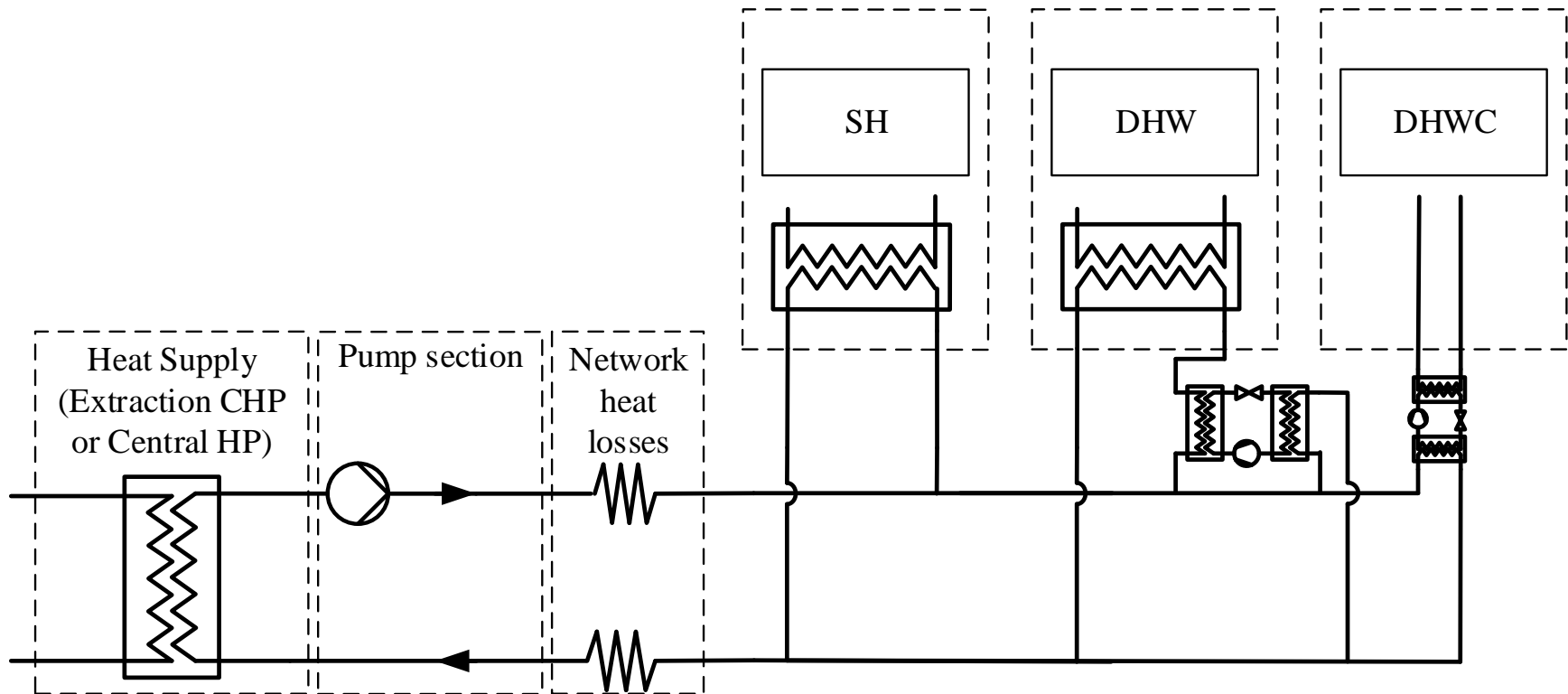
# Booster HP: Investment Cost

Working Fluid	COP	$A_{\text{evap}}$	$A_{\text{cond}}$	$\dot{V}_{\text{comp}}$	$\text{PEC}_{\text{evap}}$	$\text{PEC}_{\text{conc}}$	$\text{PEC}_{\text{comp}}$	$\text{PEC}_{\text{total}}$	$\text{TCI}_{\text{total}}$
	[–]	[m <sup>2</sup> ]	[m <sup>2</sup> ]	[m <sup>3</sup> /h]	[€]	[€]	[€]	[€]	[€]
R134a	6.11	1.52	2.11	9.21	289.01	350.88	1,525.83	2,165.71	8,662.86
Propane	6.01	1.52	2.13	7.56	288.54	353.80	1,564.14	2,206.49	8,825.94
50 % Propylene – 50 % Butane	8.85	5.09	4.28	9.92	668.31	582.06	1,943.18	3,193.55	12,774.20
30 % Propane – 70 % R1234zeZ	8.76	4.41	4.62	12.00	596.30	618.07	2,263.86	3,478.23	13,912.92

# Booster HP: Heat Generation Cost

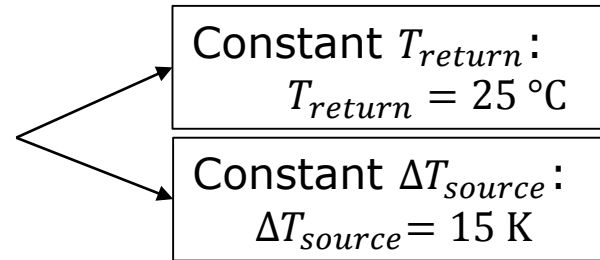


# DH System: Layout



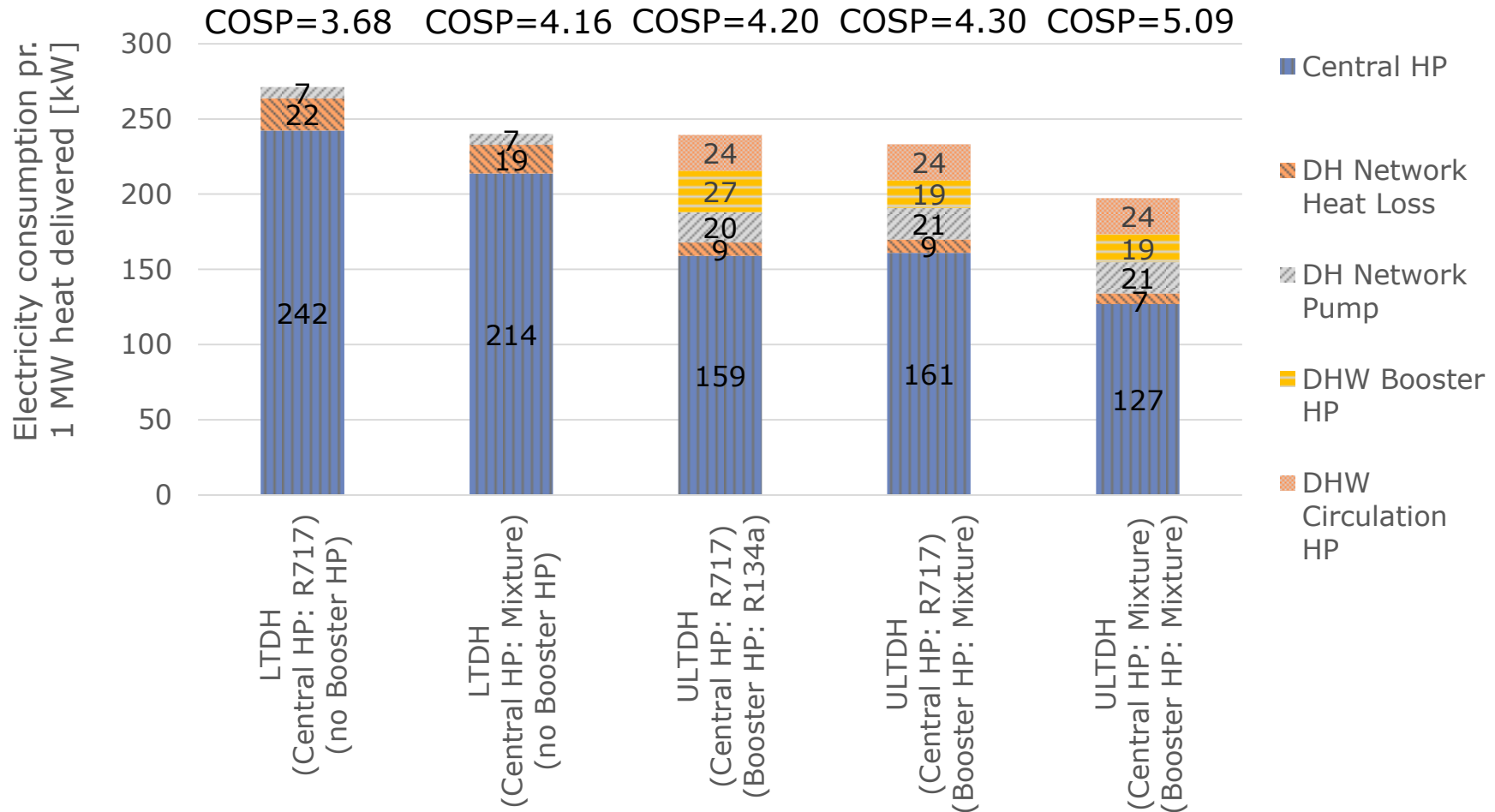
# DH System: Off Design Analysis

Varying forward temperature:  
 $T_{forward} = (35 \dots 40 \dots 45 \dots 50) \text{ } ^\circ\text{C}$



	$T_{forward} = T_{sink,in}$									
	35 °C		40 °C	45 °C		50 °C				
	$T_{return} = T_{source,out}$									
	20 °C	25 °C	25 °C	30 °C	25 °C	35 °C	25 °C			
Medium	COSP [-]									
R134a	- 7 %	- 13 %	<b>4.18</b>	$\pm 0 \%$	$\pm 0 \%$					
R290			<b>4.17</b>						- 2 %	- 3 %
R1234zeZ			<b>4.18</b>							
50 % IsoButane – 50 % Pentane			<b>4.30</b>							
50 % Propylene – 50 % Butane			<b>4.29</b>							
50 % IsoButane – 50 % DEE			<b>4.29</b>						- 3 %	- 4 %
50 % R1234yf – 50 % R1233zdE			<b>4.29</b>							
30 % Propane – 70 % R1234zeZ			<b>4.29</b>							

# DH System: System Performance



# Conclusions

- Thermodynamic performance of Booster HP:
  - R134a: COP = 6.11
  - 50 % Isobutane / 50 % Pentane: COP = 9.01 (+47 %)
- Economic performance of best mixtures similar to best pure fluid
  - Economic performance strongly dependent on boundary conditions
- Off Design of mixtures similar to pure fluids
- Temperature difference between forward and return should be maintained during off design
- Thermodynamic performance of DH System:

Working Fluid of HPs	Pure Fluid	Mixture	
LTDH	COSP=3.68	COSP=4.16	(+13 %)
ULTDH	COSP=4.20	COSP=5.09	(+21 %)
	(+14 %)	(+22 %)	