



## **A process-oriented life-cycle assessment (LCA) model for environmental and resource-related technologies (EASETECH)**

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3 A process-oriented life-cycle assessment (LCA) model for  
4 environmental and resource related technologies (EASETECH)

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15 *Keywords: Life cycle assessment, environmental assessment, resource recovery, technology modelling, unit-process,*  
16 *material flow analysis, EASETECH, biorefinery*

17

18

19 **Abbreviations**

20 CT = Composite Transformer; FD = Fraction Distributor; FG = Fraction Generator; FH = Fraction Hub; FT = Fraction  
21 Transformer; GW = Global Warming; LCA = Life Cycle Assessment; LCI = Life Cycle Inventory; MD = Material  
22 Distributor; MF = Material Flow; MG = Material Generator; NG = natural gas; RED = Renewable Energy Directive; RF  
23 = Residues Flow; SD = Substance Distributor; SG = Substance Generator; SH = Substance Hub; ST = Substance  
24 Transformer.

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34

35 **Abstract**

36 **Purpose**

37 In life cycle assessment (LCA), environmental technologies are often modelled as “black-box processes”, where inputs  
38 and outputs are typically not linked through physical and/or (bio)chemical relationships. This limits transparency and  
39 usability of environmental modelling of resource systems for which the conversion of materials and chemical substances  
40 in the materials is essential for the environmental performance. We introduce an advanced “process-oriented” modelling  
41 framework allowing quantitative and parameterised physical-chemical relationships between input-material composition,  
42 conversion process units, and subsequent output-products, promoting mass and substance balanced conversion modelling  
43 and environmental assessment.

44

45 **Methods**

46 A dedicated LCA-model, EASETECH, has been used to provide a user-friendly platform for performing advanced LCA  
47 of complex technologies, without the need for additional software/tools. In the modelling framework, the technology is  
48 subdivided into individual unit-processes. In each process, the characterization of the input-feedstock material into  
49 biochemical, physical, chemical, and nutritional properties is taken into consideration in each multi-output production  
50 flows. For each unit-process, the processes governing the mass/energy/substance transition and transformation are  
51 described by mathematical equations (i.e. relationships between inputs and outputs) through the use of parameters. A  
52 range of new operators was developed to establish these relationships that allow for non-linear responses whereby changes  
53 in one flow, can give a non-linear response in other flows. The modelling framework and the involved operators are  
54 explained and applied to a biorefinery case-study.

55

56 **Results and discussion**

57 The model facilitates "tracking" of the feedstock material properties from the input to the final products, by establishing  
58 mass, substance and energy balances for each conversion unit-process. In addition, the process-oriented modelling  
59 framework appropriately represents material/substance transition and transformations. The choice of process parameters  
60 has considerable importance for the overall results. This was illustrated by one-at-a-time changes in parameter values in  
61 two different biorefinery unit-processes (i.e. hydrolysis, and fermentation and distillation). In addition, the relevance of  
62 feedstock characteristics for the performance of the individual unit-processes was proved with fixed parameter sets with  
63 different feedstocks. The biorefinery case-study demonstrated that the LCA model can be applied to technology cases  
64 with different process configurations (e.g. different efficiencies) and different input-feedstock properties, where it  
65 automatically adjusts to these changes in properties.

66

67 **Conclusions**

68 The advanced process-oriented modelling framework offers more flexible modelling of the conversion technology than  
69 previously available, improved options for technology development in view of environmental performance, and  
70 potentially more accurate results. This provides a significantly improved basis for environmental modelling and decision-  
71 making in relation to resource systems.

72

## 73 **1 Introduction**

74 Life cycle assessment (LCA) represents a standardised and systematic methodology for assessing the  
75 environmental performance of technologies and technology systems (ISO 2006 a, b; EC-JRC 2010). In the transition to a  
76 more resource efficient and sustainable society, e.g. represented by circular (bio)economy initiatives (European  
77 Commission 2014; Zabaniotou 2018) and the European sustainability targets (e.g. European Parliament and the Council  
78 of the European Union 2009), appropriate management and utilisation of waste materials and residual resources in society  
79 are critical in order to minimise losses, maximise environmental savings and avoid suboptimal solutions at societal level.  
80 Waste and residual resources represent complex and heterogeneous materials with a wide range of physical and  
81 (bio)chemical properties. Recovery and conversion of such materials into secondary raw materials and new valuable  
82 products rely on the specific characteristics of these materials, and the environmental benefits associated with potential  
83 management solutions are highly affected by the material properties themselves (Bisinella et al. 2017). LCA modelling  
84 of residual resource systems, therefore, should not only account for the resource characteristics but also reflect  
85 relationships between input-material properties and the output-products for a wide range of different conversion  
86 technologies and process configurations. This puts considerable demands on LCA modelling of resource systems to  
87 ensure transparency and flexibility in modelling.

88 A wide range of (non)commercial LCA-models is available for environmental assessment (e.g. SimaPro,  
89 Thinkstep Gabi, TEAM, Umberto NXT LCA; for a more complete list see EPLCA, 2019). While most of these modelling  
90 tools are primarily targeted environmental assessments of products and manufacturing, rather than systems comprising  
91 several technologies involving material flows and conversion of material resources through physical, chemical, and  
92 biological processes, the majority of these tools follow a so-called “black-box” modelling approach where embedded data  
93 inventories represent individual technologies with a fixed list of inputs and outputs. This means that the user is limited to  
94 the technology assumptions “embedded” in the inventories. As differences in modelling assumptions (e.g. technical  
95 assumptions, technology type and the inventories used) lead to differences in LCA results (e.g. Gentil et al. 2010), this is  
96 a crucial aspect that has particular importance in relation to resource systems and when the technologies themselves are  
97 in focus (e.g. Astrup et al. 2018; Henriksen et al. 2018). A few LCA-models are specifically designed to evaluate material  
98 and resource flow systems (e.g. Jain et al. 2015), with EASETECH being a notable example for LCA of environmental  
99 technologies (Clavreul et al. 2014). Using principles from material flow analysis (MFA), EASETECH keeps track of  
100 mass, substance and energy flows throughout a system of processes and technologies represented by a scenario (Clavreul  
101 et al. 2014). However, EASETECH is focused on modelling of linear material and substance flows, but does not allow  
102 accounting of interactions between individual materials and substances nor the transformation of substances themselves.  
103 This interaction is needed in case of technologies involving conversion of substances and materials, and where flows and  
104 transformations are linked to the amount of specific materials entering a process. As such, there is a need for LCA  
105 modelling frameworks allowing constraints, non-linear relationships, and new substances to be created as a result of  
106 biological and chemical reactions, while maintaining the overall mass, substance and energy balance of the model.

107 Black-box models can be defined as a combination of one or more single-operation unit-processes aggregated  
108 into a fixed list of inputs (energy, materials and chemicals) and outputs (products, emissions and residues) with no direct  
109 relationship between inputs, outputs and process operations (EC-JRC 2010). The evolution from product LCA to process  
110 LCA has taken time seeing the process as black-box, thus limiting the analysis of unit-processes within complex systems  
111 (Jacquemin et al. 2012). Recently, this challenge has been highlighted by Maes et al. (2015) who explained how black-

112 box modelling approaches present considerable limitations to application of the EU renewable energy guidelines  
113 (European Parliament and the Council of the European Union 2009) when applied on complex production sites, mainly  
114 because black-box models cannot appropriately represent the individual unit-processes and therefore do not identify the  
115 impacts associated with these unit-processes. For resource conversion technologies such as biorefineries, this means that  
116 no specific links exist between the input-feedstock composition, the subsequent transformation of feedstock properties  
117 occurring within the individual unit-processes, and the final outputs and emissions from the biorefinery. This is in contrast  
118 to real processes in which all these aspects are directly interlinked. As such, the LCA models cannot account for potential  
119 changes in feedstock-composition between case-studies, nor for changes in performance of the involved unit-processes.  
120 Limiting LCA models to fixed technology aggregations and inventory data, thereby significantly limits the applicability  
121 of the LCA model, but also reduces the transparency of the model and requires new inventory datasets to be developed  
122 for each case-study.

123 To overcome the need for implementing inventory datasets according to the specific technological, geographical  
124 and temporal scope of an assessment, several approaches have been applied in literature: a) relatively simple material  
125 flow analysis (MFA) methods for determination of material flow and emission partitioning within technologies and across  
126 a system of technologies (e.g. Mancini et al. 2015; Turner et al. 2016), and b) more advanced process simulation tools  
127 (e.g. ASPEN, ProSim, ProMax, CHEMCAD) to evaluate individual biological, physical, and chemical unit-processes  
128 within a technology (e.g. Tumilar et al. 2016). While these approaches and tools certainly have merits, the definition of  
129 the technology inventories remains separated from the LCA modelling itself. A few studies (e.g. Arora et al. 2016; Brunet  
130 et al. 2012; Gaha et al. 2018) have attempted to combine LCA modelling with the process simulation tools mentioned  
131 above and/or with mathematical programming tools (e.g. MATLAB). While this potentially allows a more detailed  
132 process-oriented approach (as opposed to black-box datasets), these models are typically not integrated with the LCA tool  
133 and need to be run separately, often requiring specific insights in the programming itself (i.e. limited user-friendliness)  
134 (Asprion and Bortz 2018). While such integration is desirable, so far, we are not aware of tools that allow modelling of  
135 unit-processes of complex technologies and concurrently performing a full LCA.

136 To further advance and facilitate LCA-modelling of more complex and integrated resource management  
137 technologies and systems, LCA-models should allow the establishment of quantitative relationships between input-  
138 feedstock composition, unit-processes, and subsequent outputs of products and emissions. This means “opening-up” the  
139 black-box models and allows the definition of useful relationships between inputs, outputs and process configurations.  
140 While subdivision of complex technologies into unit-processes is supported by current LCA guidelines (EC-JRC, 2010),  
141 such a modelling approach is here termed “process-oriented” LCA modelling. Modelling of residual resource  
142 technologies like biorefineries requires detailed data of the input-material (e.g. water content, energy content), the  
143 transformations of materials or substances during processing, and the transition of mass from one flow to another. To  
144 enable transparent and flexible adjustment of the model to a specific case-study, the involved model parameters should  
145 reflect subdivision in relevant unit-processes (e.g. for a biorefinery: pre-treatment, hydrolysis, fermentation and  
146 distillation, separation and recovery of the solid and liquid fractions). In an integrated technology system with several  
147 flows associated to multiple product-outputs, working with parameterised unit-processes and input-output process  
148 relationships allows to change a specific production-flow and have a non-linear response in other flows such as increasing  
149 or decreasing their production and associated emissions. Currently, no existing publically available LCA model offers

150 such process-oriented modelling approach relevant for resource-centric technologies and systems, although some models  
151 enable interaction with external software to allow users some degree of taking these aspects into account.

152 The aim with this study is to advance LCA modelling of integrated technologies and technology systems  
153 targeting environmental assessment of resource management by implementing advanced “process-oriented” LCA  
154 modelling. The following specific objectives are addressed: i) provide a framework for process-oriented LCA modelling  
155 of multi-output conversion technologies, ii) define the needed operators and implement these in the software EASETECH,  
156 iii) demonstrate the applicability of the modelling framework on a simplified biorefinery case-study, focusing on global  
157 warming impacts in combination with the importance of feedstock characteristics and unit-process parameters (e.g.  
158 conversion efficiency) under specific operating conditions, and finally on this basis iv) evaluate the perspectives and  
159 implications of the proposed advanced process-oriented modelling approach. The outcome of the study represents the  
160 methodological basis for advanced mass, substance and energy balanced LCA modelling to resource technology systems  
161 in EASETECH.

162

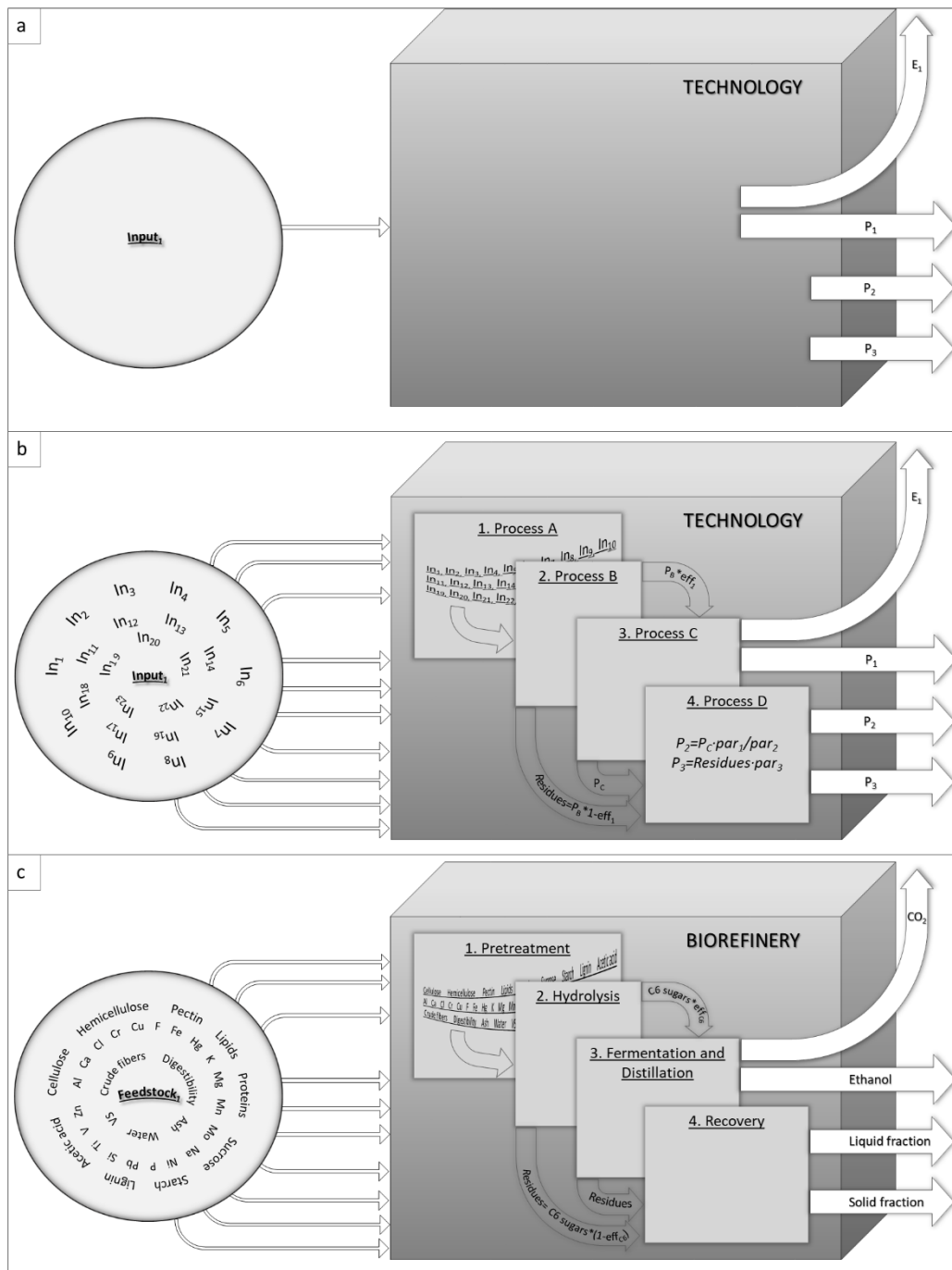
## 163 **2 Material and methods**

### 164 **2.1 Principles of process-oriented LCA modelling**

165 The characterization of the input-feedstock into individual fractions, each with associated biochemical, physical,  
166 chemical, and nutritional properties is the point of departure of a process oriented LCA. Subdividing a material flow  
167 according to properties enables modelling of the conversion (or “fate”) of these properties within a specific process,  
168 technology or an entire system of several technologies, and linking the input-feedstock to the associated outputs generated  
169 by the involved processes. These material properties thereby represent an extension of the substances used within MFA  
170 (Allesch and Brunner 2015; Brunner and Rechberger 2016), e.g. carbon is a chemical element and cellulose is a  
171 compound; both of them are properties of the biomass feedstock: the carbon content takes into consideration the carbon  
172 content of cellulose, representing a part of the total carbon in the biomass. Conversion of the input-feedstock is associated  
173 with either transition or transformation of feedstock properties. Transition occurs when a specific amount of a material or  
174 fraction or substance (and thereby share of material properties), usually expressed in percentages, is transferred from an  
175 input to an output of a process. The transition within a process can be partial (less than 100% of a material flow is  
176 transferred) or total when the entire material flow is transferred. Transformation of the input-feedstock material occurs  
177 when one or more fractions or one or more substances has a change in its composition within a process. Thus, some  
178 fractions/substances may cease to exist, while new ones may be introduced. Also, in this case, the transformation can be  
179 total, when a fraction or substance is entirely used in a transformation, or it can be partial when only a defined quantity  
180 of a selected substance/fraction is involved in the conversion process. Consequently, the original material prior to the  
181 transformation does not exist anymore because a different material is generated departing from it; however maintaining  
182 the overall mass, energy and substance balance of the process. Moreover, mass transition and transformation within a  
183 system are linked to environmental exchanges that subsequently are converted into environmental impacts. For example,  
184 in a process where mass and energy are given by the material conversion of the process itself, considering emission factors  
185 during the characterisation phase (after the inventory), allows emissions to be quantified according to the availability of  
186 the substance/mass/energy involved in different material flows within the considered unit-process. In addition, in the  
187 process-oriented model, the technology is subdivided into individual unit-processes. For each unit-process, the

188 (bio)physical processes governing the mass/energy/substance transition and transformation are identified and described  
 189 by mathematical equations. These equations allow the establishment of relationships and interdependencies between the  
 190 input-feedstock material properties and the (unit)process outputs. Parameters can be applied to allow adjustments of  
 191 material flows and process performance to specific cases. If a parameter is in an equation, it can directly affect its result,  
 192 and thus the conversion process, the substance/mass/energy flow, and the respective emission. Furthermore the proposed  
 193 framework allow for non-linear responses whereby changes in one flow, can give a non-linear response in other flows.

194 Fig. 1 illustrates the generic black-box vs process-oriented technology modelling: in the black-box modelling  
 195 approach (Fig. 1a), the technology is described by an input and several outputs represented by  $Input_1$ , the products  $P_1$ ,  $P_2$ ,  
 196  $P_3$  and the emission  $E_1$ .



227 **Fig. 1** a) Black-box modelling approach applied to a generic technology;  $Input_1$  is the input-process;  $P_1$ ,  $P_2$  and  $P_3$  are  
228 the output-products and  $E_1$  is an example of technology emission.

229 b) Process-oriented approach applied to the same generic technology; same input, final output-products and emission  
230 (i. e.  $Input_1$ ,  $P_1$ ,  $P_2$ ,  $P_3$ ,  $E_1$ ); the input-properties (e.g.  $In_1$ ,  $In_2$ ) are considered. In addition, relationships/interdependencies  
231 are established between the technology unit-processes (i. e. *Process A, B, C, D*) and described with equations containing  
232 parameters (Equation 1:  $P_2 = P_{A2} \cdot par_1 / par_2$  and Equation 2:  $P_3 = P_{B1} \cdot par_3$ , with  $par_1$ ,  $par_2$  and  $par_3$  as parameters).

233 c) Process-oriented approach applied to the case of a second generation biorefinery. The unit-processes considered are:  
234 1. *Pretreatment, Hydrolysis, Fermentation and distillation, Recovery*. The input is  $Feedstock_1$ , having properties (e.g.  
235 Cellulose, Ca). Relationships/Interdependencies are described through equations with parameters; the final whole-  
236 system output-products are: *ethanol, liquid fraction, and solid fraction*.  $CO_2$  represents an example of emission

237 Any relationships and interdependencies between the input-feedstock material and the output-products are not  
238 represented by the model. In addition, the technology is not subdivided into unit-processes and  
239 relationships/interdependencies represented by equations containing parameters are not included. On the contrary, in the  
240 process-oriented modelling approach the technology (Fig. 1b) is described through input-feedstock material properties  
241 (e.g.  $In_1$ ,  $In_2$ ,  $In_3$ ), relevant unit-processes (*Process A, B, C, D*), and relationships between input-feedstock material  
242 properties and process outputs using equations with parameters. In Fig. 1b, the output-product  $P_B$  is partially transferred  
243 to Process C, i.e.  $P_B$  has an associated conversion efficiency ( $eff_1$ ) in the transition from Process B to C.  $(1-eff_1)$  represents  
244 what is left, i.e. residue, of  $P_B$  subsequently transferred to Process D. An example of total transition is represented by the  
245 product  $P_C$ , totally transferred to process D together with the residues of Process B.  $P_2$  and  $P_3$  are two products of Process  
246 D generated through two equations ( $P_2 = P_C \cdot par_1 / par_2$ ;  $P_3 = Residues \cdot par_3$ ). These equations are two examples  
247 of relationships between inputs and outputs within Process D and  $par_1$ ,  $par_2$ , and  $par_3$  are the three associated parameters.  
248 As an example, Fig. 1c illustrates this modelling approach implemented on a second generation biorefinery where the  
249 lignocellulosic input-feedstock is converted into bioethanol, a solid and liquid fraction, and  $CO_2$ . The feedstock is  
250 characterised according to relevant biochemical, chemical, physical, and nutritional properties (e.g. cellulose, proteins,  
251 carbon content, energy content, water content, digestibility, etc.). The overall biorefinery technology is represented by a  
252 range of unit-processes: 1) pre-treatment, 2) hydrolysis, 3) fermentation and distillation, and 4) recovery. In the entire  
253 biorefinery system, both transitions and transformations occur, and the relationships between the input-feedstock  
254 properties and the output-products are identified and described by appropriate equations involving adjustable parameters  
255 (e.g. conversion efficiency of C6 sugars,  $eff_{C6}$ , into ethanol production, thereby facilitating flexible adaption of the model  
256 from one case-study to another). An example of material transformation is given by the hydrolysis, where polysaccharides,  
257 such as cellulose, pectin, hemicellulose, starch, and sucrose, are converted into simple sugars with five and six carbon  
258 atoms (C5 and C6 sugars). While one substance (polysaccharides) thereby is transformed into another substance  
259 (monosaccharides) and thus cease to exist, the overall mass and substance balance of the technology is maintained and  
260 the flows are trackable. In Online Resource (Sections S2 to S6), these biorefinery-unit processes are thoroughly described  
261 including the transformation equations used.

262 The process-oriented modelling approach allows users to establish models with all the necessary unit-processes  
263 involved, to clearly define the feedstock conversion and to include appropriate modelling parameters and assumptions.  
264 This is useful particularly in studies that wish to base the assessment on pre-developed models reproducing specific



265 technologies such as lignocellulosic biorefineries, but intend to apply case-specific process performance data and/or  
 266 update the model to reflect assumptions more relevant for the case-study in question.

267

## 268 2.2 EASETECH modelling features supporting process-oriented modelling

269 To facilitate process-oriented LCA modelling in EASETECH, a range of new “operators” were  
 270 developed following the principles of domain specific language illustrated in Zarrin and Baumeister (2014). The  
 271 new operators allow a domain expert (a person with the relevant technological and systemic expertise) to  
 272 establish the relationships between input and output for the individual unit-processes, described in the previous  
 273 section. In EASETECH, LCA scenarios are characterised by a number of “process modules” that are connected  
 274 with arrows indicating material flows between the processes (see Section 2.3 for further details). Process modules  
 275 may represent individual unit-processes or entire technologies and can be nested, i.e. a number of “unit-process  
 276 modules” may be “packed” into another process module. As such, the scenario building in EASETECH follows  
 277 the overall principles of MFA; for details see (Clavreul et al. 2014) and (Allesch and Brunner 2015). These  
 278 principle are also applied to the unit-processes modelled involving the new operators and subsequently  
 279 implemented into EASETECH. Tab. 1 provides an overview of all new operators, while the remainder of this  
 280 section explains the key features of the operators. Further details describing the individual operators applied for  
 281 the modelling of the biorefinery case study (see also Section 2.3) unit-processes can be found in Online Resource,  
 282 Sections S2.7, S3.1, S4.1, S5.1 and S6.1.

283

284 **Tab. 1** Operators available in EASETECH and their application for the modelling of processes within technologies and systems

OPERATOR	APPLICATION
<i>Material Flow [MF]</i>	MF transfers material from a source element to a target element. It is allowed using more than one MF from the same source element.
<i>Residues Flow [RF]</i>	RF transfers what is left in a source element (residue). It is allowed using only one RF from the same source element
<i>Fraction Distributor [FD]</i>	FD extracts a fraction from a material
<i>Fraction Generator [FG]</i>	FG generates a fraction in a material
<i>Fraction Hub [FH]</i>	FH groups fractions from an input-material
<i>Fraction Transformer [FT]</i>	FT transforms a fraction into another one within a material. As a consequence, the previous fraction does not exist anymore
<i>Material Distributor [MD]</i>	MD extracts a material
<i>Composite Transformer [CT]</i>	CT groups more than one operator. It allows iterating a sequence of transformations and transitions
<i>Primitive Parameter</i>	It generates a parameter (numeric or string)
<i>Data Table Parameter</i>	It generates a table of parameters; it may contain one or more <i>Data Columns</i>
<i>Data Column</i>	It generates columns into a <i>Data Table Parameter</i> ; each column refers to a parameter
<i>Material Generator [MG]</i>	MG generates a material that may contain one or more material fractions
<i>Input</i>	It contains all the initial inputs (starting point)
<i>Output</i>	It contains all the final outputs (ending point)
<i>Substance Distributor [SD]</i>	SD extracts a substance within a fraction

OPERATOR	APPLICATION
<i>Substance Hub [SH]</i>	SH groups substances from fractions
<i>Substance Transformer [ST]</i>	ST transforms a substance into another one; consequently, the previous substance does not exist anymore
<i>Substance Generator [SG]</i>	SG generates a substance

285

286 The following three macro levels are considered in the model: materials, fractions and substances. Materials,  
 287 following the MFA definition, contain both substances and goods. In this case, goods represent fractions, “entities” that  
 288 share common characteristics, i.e. substances. As such, “grass”, “branches”, and “wood” may all represent fractions in a  
 289 material called “garden waste”, while substances represent chemical, nutritional, physical and biochemical properties  
 290 (e.g. cellulose, proteins, lower heating value, methane potential, digestible energy). Some of the substances may be  
 291 correlated, e.g. the energy content of a fraction is a function of the content of cellulose, proteins, etc. Physical, chemical,  
 292 nutritional and biochemical properties are assigned to the substance level, although they are not necessarily substances as  
 293 such (e.g. energy is not a substance, but it is modelled using the same operators as for substances).

294 For the individual process module there is at least one input and one output. There are three possible input types:  
 295 i) an output from another process, ii) a material consisting of several fractions, or iii) a single fraction. The anaerobic  
 296 digestion of organic waste is an example of the first case; it generates biogas and digestate as final outputs: the digestate  
 297 may then be used as input to a subsequent fertilisation process. For the second case, e.g. a material (e.g. garden waste)  
 298 with multiple fractions (e.g. grass, wood), the operator that generates the input-feedstock material is *Material Generator*  
 299 (MG); then, a *Fraction Generation* (FG) is needed for generating each fraction within the input-material. Thus, we are  
 300 generating the material composition. The last case, when the input is a single fraction (e.g. grass), only an FG is applied  
 301 to generate the fraction. Lastly, a *Substance Generator* (SG) is used to specify each input-material property, i.e. chemical,  
 302 biochemical, physical, nutritional. Each of these properties is modelled as substances within a fraction. A range of  
 303 physico-chemical relationships, represented by mathematical equations, are applied when a substance or a fraction is  
 304 “transformed” within a process, e.g. one or more substances are converted into a specific product (e.g. glucose to ethanol)  
 305 that may be the final output of a process or an intermediated product subsequently used in another conversion flow. The  
 306 following operators are used for this purpose: *Substance Transformer* (ST) and *Fraction Transformer* (FT) when the  
 307 transformation is related to a substance and a fraction, respectively. With these operators, a selected substance or fraction  
 308 involved in the conversion process can be specified not to exist anymore while another substance or fraction is generated  
 309 in its place, i.e. transformation from one entity into another. However, a transformation may also represent a modification  
 310 of the substance or fraction content by changing only its amount while still preserving the substance or fraction itself. It  
 311 is possible to change the content of a substance: the substance is the same and its amount is different (e.g. decreasing the  
 312 water content of 50% of the original value).

313 Furthermore, each material/fraction/substance within a system or a technology may be transferred from one  
 314 process to another, i.e. inter-process transition, or within a single process from inputs to outputs, i.e. intra-process  
 315 transition. The inter-process transition represents cases when a process-output is transferred to a subsequent process-  
 316 input, e.g. when sugars produced during hydrolysis are used in fermentation to generate ethanol and CO<sub>2</sub>, thus the  
 317 transition is from hydrolysis to fermentation. The intra-process transition is when specific properties are involved in the  
 318 generation of process-outputs, e.g. when in hydrolysis, cellulose is depolymerised into C6 sugars and this transition occurs

319 from the hydrolysis input to the hydrolysis output. The carbon content of cellulose (here classified as a substance)  
320 contributes to the generation of C6 sugars (classified as substance). To model these two types of transitions one needs to  
321 be able to separate and “extract” a single material/fraction/substance from the remaining materials/fractions/substances.  
322 Extracting means isolating the material/fraction/substance and considering it as a single independent element to be  
323 subsequently used in other conversion flows. Operators that allow this extraction are *Material Distributor* (MD), *Fraction*  
324 *Distributor* (FD) and *Substance Distributor* (SD). Considering the example of garden waste, an FD may be applied in the  
325 example where only grass (a fraction within garden waste) is addressed in a specific (unit)process. Thus, grass may be  
326 extracted from the other fractions composing the garden waste and routed to a different flow for modelling purposes. An  
327 example of using SD is the separation of non-biodegradable matter such as lignin within an organic feedstock. With SD,  
328 the lignin representing a feedstock’s biochemical property may be extracted and routed to a combustion process for energy  
329 utilisation. In cases when more than one fraction or substance are routed to a new flow, these fractions and substances  
330 need to be grouped: a *Fraction Hub* (FH) is used for grouping fractions while a *Substance Hub* (SH) is for substances.  
331 Material Flows (MF) are represented by an arrow and are used for the transition of materials, fractions, and substances  
332 from a source element to a target element. Within a process, conditional statements can be associated with individual  
333 MFs, e.g. water content > 0, to ensure a flow continues as long as the given condition is true. A *Residue Flow* (RF) is  
334 applied to close mass balances, i.e. to “catch” and transfer any remaining mass (residues) after transformation operations.  
335 Also, RF is represented by an arrow and is used for transitions. While it is possible to have more than one MF from a  
336 source element (e.g. an operator), only one RF can be used to close the mass balance. If the residues are transferred to a  
337 target element within the process, no other residue exists.

338 In addition to the above-mentioned methods to transform, divide and group materials, fractions, and substances,  
339 a range of calculations may be done on these entities by a *Composite Transformer* (CT). In a CT calculations may be  
340 grouped and if necessary combined with more operators relevant for the material, fraction or substance “level” in question.  
341 These calculations are performed using mathematical equations with parameters. *Primitive* parameters represent single  
342 values, such as a constant (e.g. conversion efficiency of C6 sugars,  $eff_{C6} = 88\%$ ). *Data Table Parameter* is used when an  
343 element has more than one parameter associated. Each column of the data table represents a parameter, i.e. the values are  
344 elements in the table, and each row is a set of parameters. The data table is identified by a name. In order to build this  
345 table, columns need to be added for each parameter; this can be done with a *Data Column* (DC). For each parameter  
346 (column), the value type is specified (i.e. a number or string). For example, we model cellulose that has as a parameter  
347 mass in kilograms and conversion efficiency into sugars in percentage; since it has two parameters associated, we may  
348 have a Data Table Parameter with three Data Columns, one for cellulose (substance), and a further two for the mass and  
349 the conversion efficiency. A process finishes with one or more outputs having all properties generated during the process  
350 modelling. This involves using one/more *Output(s)* representing all the material properties transferred to it/them through  
351 MFs and/or RFs.

352 An example of a combination of more than one operator described in this section is presented in Fig. 2. This  
353 represents an illustrative example removing 10% of water (substance) from the grass (fraction) in garden waste (material).  
354 A way to accomplish this is first to define and generate the material garden waste through an MG; secondly, the generation  
355 of fractions within it, such as: grass, wood, plants, branches, tree, and soil, stones and foreign objects, through FGs;  
356 thirdly, all these fractions are grouped in an FD, linked to a CT where the substances associated with each fraction are  
357 generated through SGs. Subsequently, the grass is extracted through an FD and the other fractions within the garden waste

358 are sent to the final output through an RF. All the substances within grass are grouped in an SH. Water is extracted through  
 359 an SD and its content is transformed (i.e. -10%) in an ST. In the final output, water with the different content is sent  
 360 through an MF linking ST with the final output. Additionally, the other substances (with the same content) are sent to the  
 361 final output through an RF from SH.

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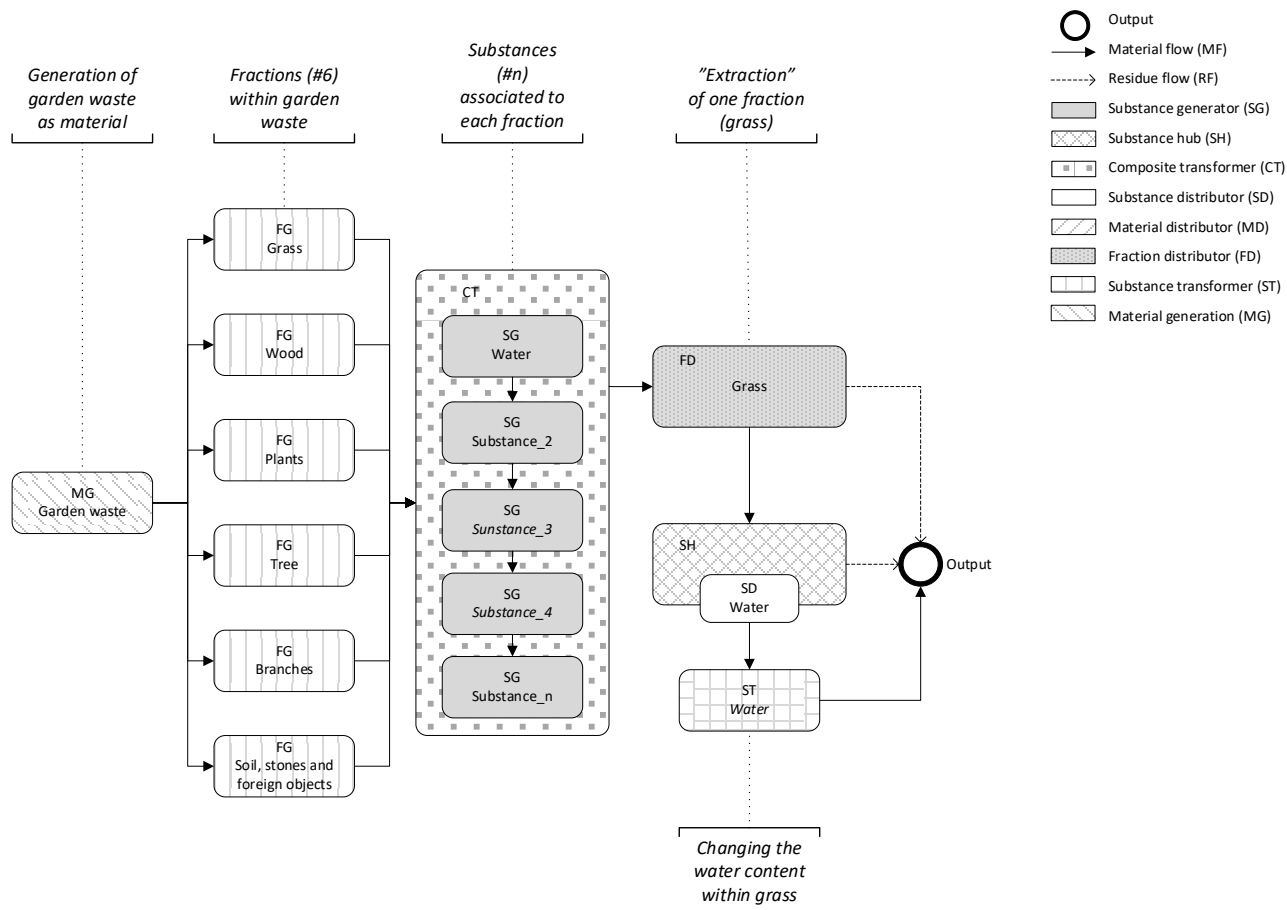
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383 **Fig. 2** Example of an application of operators for decreasing the water content (substance) of the grass (fraction) within garden waste  
 384 (material)

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### 386 2.3 Application of the process-oriented modelling approach to a biorefinery case

#### 387 2.3.1 Description of the technology system

388 The case-study evaluates a second generation biorefinery using the above-mentioned operators within  
 389 EASETECH. The biorefinery is composed of five main unit-processes: *bio-material generation, pre-treatment,*  
 390 *hydrolysis, fermentation* and *distillation, recovery*. In bio-material generation, the input-feedstock is modelled considering  
 391 all its properties (substances), such as biochemical (organic matter content), elemental (inorganic matter content),  
 392 nutritional (i.e. the “feeding value” calculated based on the feedstock nutritional-energy content), and physical (e.g. water,  
 393 ash, etc.), see Online Resource, Section S2 for details. For modelling purposes, bio-material generation is considered as  
 394 a process, although this does not represent the conversion of the feedstock but merely the relevant calculations of  
 395 feedstock properties prior to the input to the pre-treatment process. Some properties (e.g. dry matter, nitrogen, oxygen,

396 hydrogen, carbon, sulphur, energy content, methane potential, etc.) are stoichiometrically calculated based on the  
397 biochemical and physical contents of the feedstock; as such these properties are correlated to other properties (Online  
398 Resource, Eq. S1 to S15). In the bio-material generation, mathematical equations then recalculate some of the properties  
399 of the selected feedstock, with the advantage of correlating them (e.g. C with LHV, N with proteins,  
400 cellulose/hemicellulose/proteins/etc. with nutritional value and LHV). All the mathematical equations used in the bio-  
401 material composition are explained in Online Resource from Sections S2.1 to S2.6. In pre-treatment (Online Resource,  
402 Section S2), energy in the form of heat is used to pre-treat the feedstock. The structure of the lignocelluloses is broken  
403 down to separate the lignin from the cellulose and hemicellulose and allow an efficient conversion into fermentable  
404 sugars. Pre-treatment may also result in some losses (e.g. when eventual mass is lost the conversion efficiency to the pre-  
405 treatment output-composition is lower than 100%) not routed further to the hydrolysis process. In hydrolysis (Online  
406 Resource, Section S4), cellulose, starch, hemicellulose, pectin, and sucrose are hydrolysed into C5 and C6 sugars. The  
407 non-hydrolysed biochemical properties represent the hydrolysis residues. In fermentation and distillation (Online  
408 Resource, Section S5), the C5 and C6 sugars are converted to bioethanol, CO<sub>2</sub>, and liquid molasses. The unconverted  
409 sugars are transferred to yet another output and passed on to a recovery process (Online Resource, Section S6), which in  
410 addition to the fermentation residues receives the mixed solid and liquid residues from hydrolysis (hydrolysis residues);  
411 here, all residues are separated to maximise further utilisation.

412           Regarding the further utilisation of these output-products, the liquid fraction was assumed to be converted into  
413 biogas, while the solid fraction was assumed to be incinerated with energy recovery. For both fractions, natural gas was  
414 assumed to be substituted for simplicity. In order to focus on the technology system modelling, we deliberately neglected  
415 the possible impacts from diverting the feedstock from its current use(s) and eventual land use changes. This should be  
416 kept in mind when interpreting the results to avoid inconsistent and unfair comparisons with other studies. We briefly  
417 stress the importance of these aspects in Section 4.3.

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### 420 **2.3.2 Assessment scope, functional unit, and system boundary**

421           The primary goal with the LCA was to demonstrate the applicability of process-oriented modelling in  
422 EASETECH and illustrate potential learnings that can be achieved on this basis. In this perspective, the assessment focus  
423 was placed on a single biorefinery scenario without the range of scenario alternatives and sensitivity/uncertainty  
424 evaluations otherwise part of an LCA (see Negro et al. 2017; Serra et al. 2017; Wang et al. 2016). As such, the case-study  
425 followed the principles of the relevant ISO standards (ISO 2006 a, b), while not strictly complying with these. Two  
426 perspectives were evaluated with the case-study: i) the importance of unit-process performance and choice of process  
427 parameters for the overall results, and ii) the importance of feedstock characteristics for the performance of the individual  
428 unit-processes at fixed parameter sets. For the first perspective, three types of input-feedstock were considered: wheat  
429 straw, beet top, and wild grass, while the second perspective was proved based on *Miscanthus*, brewer's grains, and  
430 willow. The first set of biomasses was selected based on their different composition to test the biorefinery model and the  
431 expected different results. Tab. 2 presents key characteristics and properties. The second set of biomasses was selected  
432 according to their cellulose, hemicellulose and lignin content. These three organic molecules have high importance for  
433 the carbon pool available in the biorefinery; *Miscanthus* has the highest cellulose content, brewer's grain has the highest  
434 hemicellulose content, and willow has the highest lignin one.

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**Tab. 2** Characteristics and properties of wheat straw (feedstock 1), wild grass (feedstock 2) and beet top (feedstock 3), used as feedstock for the biorefinery case-study

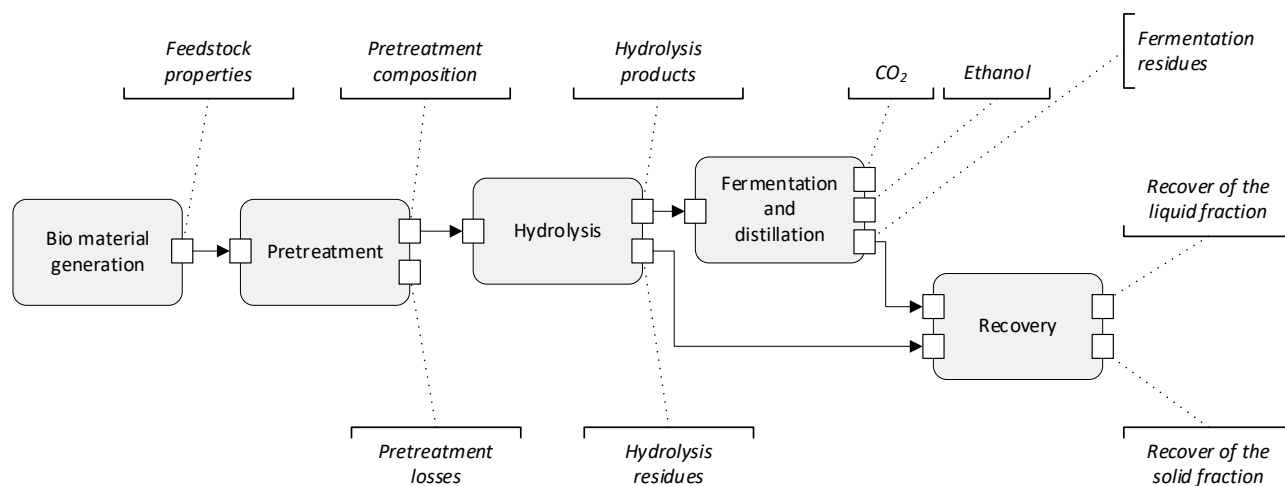
<i>Bio_material_generation</i> – PARAMETERS						
Subgroup	<b>BIOCHEMICAL PROPERTIES</b>	<b>Description</b>	<b>Feedstock 1</b>	<b>Feedstock 2</b>	<b>Feedstock 3</b>	<b>Unit</b>
1	<i>Acetic acid*</i>	CH <sub>3</sub> COOH	0.0	0.0	0.0	%DM
2	<i>Cellulose</i>	Cellulose parameter	34.7	29.1	11.2	%DM
3	<i>Hemicellulose</i>	Hemicellulose parameter	22.4	24.2	16.2	%DM
4	<i>Lignin</i>	Lignin parameter	17.7	3.0	8.2	%DM
5	<i>Lipids</i>	Lipids parameter	2.3	0.5	2.4	%DM
6	<i>Pectin</i>	Pectin parameter	0.0	0.0	8.2	%DM
7	<i>Proteins</i>	Proteins parameter	3.5	5.2	16.9	%DM
8	<i>Starch</i>	Starch parameter	0.0	0.0	3.6	%DM
9	<i>Sucrose</i>	Sucrose parameter	0.0	0.0	11.9	%DM
10	<i>OtherVS</i>	Unspecified VS parameter	14.07	33.86	4.9	%DM
Subgroup 2	<b>ELEMENTAL PROPERTIES</b>					
11	<i>Al</i>	Aluminium	0.0168	0.0000	0.0000	%DM
12	<i>Ca</i>	Calcium	0.2435	0.5500	1.3000	%DM
13	<i>Cl</i>	Chlorine	0.3876	0.8000	1.6000	%DM
14	<i>Cr</i>	Chromium	0.0003	0.0000	0.0000	%DM
15	<i>Cu</i>	Copper	0.0004	0.0007	0.0013	%DM
16	<i>F</i>	Fluorine	0.0011	0.0000	0.0000	%DM
17	<i>Fe</i>	Iron	0.0134	0.0220	0.0000	%DM
18	<i>Hg</i>	Mercury	0.0000	0.0000	0.0000	%DM
19	<i>K</i>	Potassium	0.9870	0.3300	4.8000	%DM
20	<i>Mg</i>	Magnesium	0.0439	0.1800	0.4100	%DM
21	<i>Mn</i>	Manganese	0.0020	0.0070	0.0090	%DM
22	<i>Mo</i>	Molybdenum	0.0001	0.0000	0.0000	%DM
23	<i>Na</i>	Sodium	0.0100	0.1500	0.9700	%DM
24	<i>Ni</i>	Nickel	0.0001	0.0000	0.0000	%DM
25	<i>P</i>	Phosphorus	0.0490	0.4000	0.1750	%DM
26	<i>Pb</i>	Lead	0.0003	0.0000	0.0000	%DM
27	<i>S</i>	Sulphur	0.0000	0.2100	0.2000	%DM
28	<i>Si</i>	Silicon	0.9300	0.0000	0.0000	%DM
29	<i>Ti</i>	Titanium	0.0005	0.0000	0.0000	%DM
30	<i>V</i>	Vanadium	0.0001	0.0000	0.0000	%DM
31	<i>Zn</i>	Zinc	0.0034	0.0000	0.0045	%DM
Subgroup 3	<b>FEEDSTOCK</b>					
32	Fraction name	Fraction	Wheat straw	Wild grass	Beet top	String
Subgroup 4	<b>FEEDSTOCK AMOUNT</b>					
33	<i>Quantity</i>	Input amount	1000	1000	1000	kg <sub>ww</sub>
Subgroup 5	<b>NUTRITIONAL PROPERTIES</b>					
34	<i>Crude_Fibers_input</i>	Crude fibres parameter	45.3	78	82	%DM
35	<i>Digestibility_input</i>	Substrate digestibility	44	24.9	12	%DM
Subgroup 6	<b>PHYSICAL PROPERTIES</b>					
37	<i>Ash</i>	Ash parameter	5.4	4.1	16.5	%DM
38	<i>VS</i>	Volatile solid parameter	94.7	95.9	83.5	%DM
39	<i>Water</i>	Water parameter	12.2	78.8	76.7	% <sub>ww</sub>

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\* Acetic acid may be present in some biomasses as degradation product

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440 The functional unit represented “the valorisation within a biorefinery of one tonne (wet weight) of input-feedstock  
 441 into three main output-products: bioethanol, solid, and a liquid fraction”. While results were calculated for all the impact  
 442 categories included in the IPCC 2013 method (IPCC, 20013; 100-year time horizon was assumed), only results for global  
 443 warming were discussed for the purpose of illustrating the functionality and applicability of the process-oriented  
 444 modelling approach. Fig.3 illustrates a generic representation of the biorefinery process-oriented model.



457 **Fig. 3** Generic representation of the biorefinery process-oriented model in EASETECH with the intermediate and final outputs

459 To ensure simplicity, a “zero burden” approach was followed and no upstream burdens associated with the input-  
 460 feedstock biomass nor any indirect effects associated with the diversion from alternative uses of the biomass  
 461 (counterfactual scenarios) were included. System expansion was applied to credit the system for avoided impacts  
 462 associated with substituting and displacing conventional market products with the biorefinery output-products. Ethanol  
 463 was assumed to be used in vehicles, substituting gasoline; molasses, the liquid fraction from the biorefinery, was used in  
 464 a biogas plant substituting the production and combustion of natural gas; solid biofuel, the solid fraction from the  
 465 biorefinery, was used in an incineration plant that substituted the production and combustion of natural gas. The emission  
 466 factor assumed for gasoline was  $0.097 \text{ kgCO}_2\text{-eq}\cdot\text{MJ}^{-1}$  and the emission factor for natural gas was  $0.067 \text{ kgCO}_2\text{-eq}\cdot\text{MJ}^{-1}$   
 467 from EASETECH database (Clavreul et al. 2014). The residual digestate after biogas production was assumed to displace  
 468 conventional NPK fertilizers, according to the content of N, P, and K. The substitution efficiency was assumed to be 40%  
 469 for N according to current Danish legislation (Danish Ministry of Food, Agriculture and Fisheries 2018) and 100% for P  
 470 and K. Air and water emissions arising from digestate and mineral fertilisers (avoided) spreading on-land were based on  
 471 the work of Yoshida et al. (2016); particularly, the emission factors used to describe  $\text{N}_2\text{O}$  emissions from digestate and  
 472 substituted mineral fertilizers were 2.78% and  $(2.32*0.40)\%$  respectively. The system boundaries included refinery  
 473 operations, harvest of biomass, transportation (digestate and solid fraction) as well as final utilisation and management of  
 474 all biorefinery outputs.

### 476 3 Results

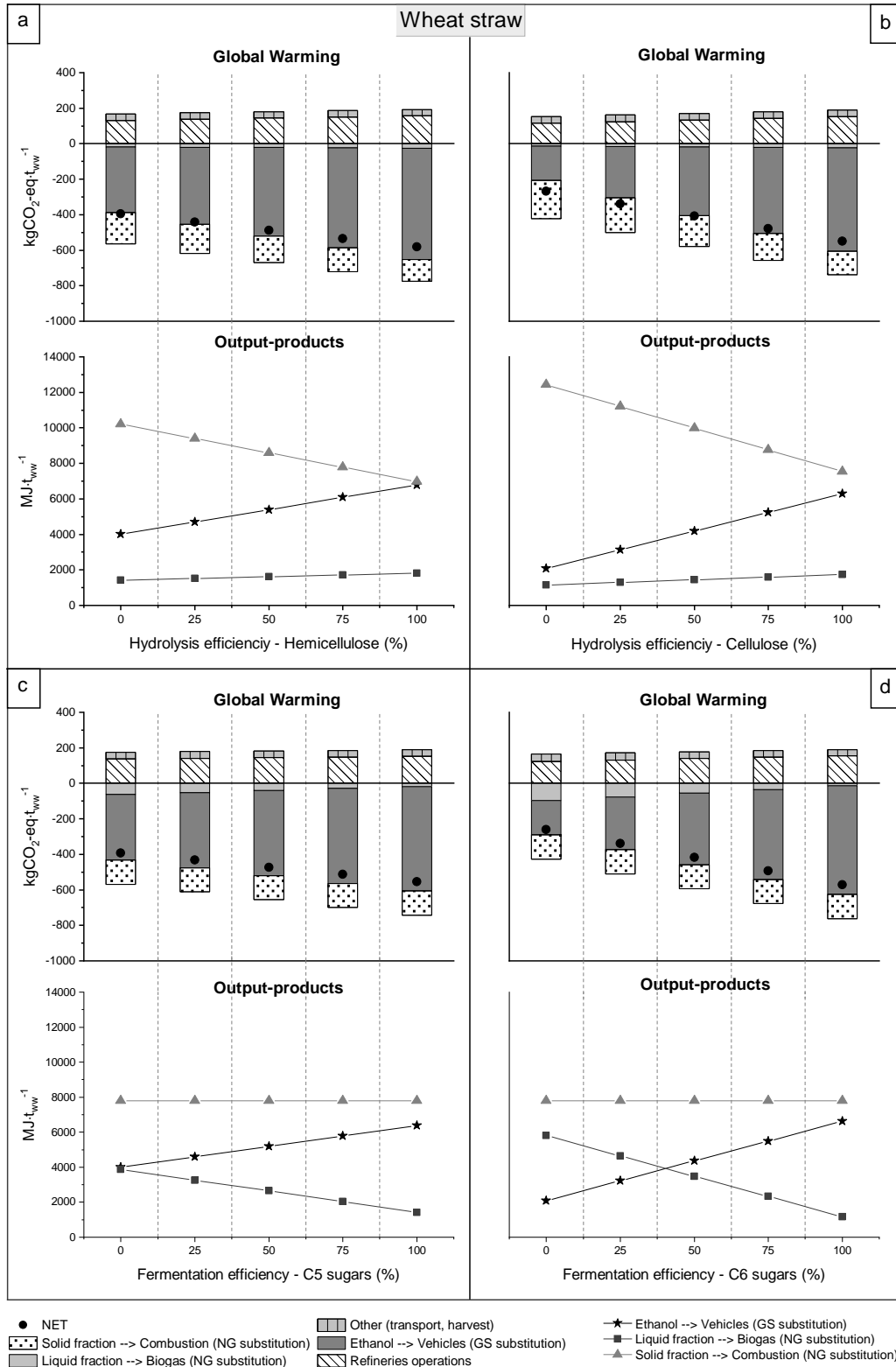
#### 477 3.1 Importance of unit-process operational efficiencies

478 Fig. 4 presents the results of global warming (GW) in kg CO<sub>2</sub>-eq t<sup>-1</sup><sub>ww</sub> for a biorefinery using wheat straw as  
479 feedstock. The biorefinery outputs are given in MJ·t<sup>-1</sup><sub>ww</sub> as a function of the efficiencies of the hydrolysis (Fig. 4a and 4b)  
480 and the fermentation (Fig. 4c and 4d) unit-processes. Through the selection of parameters (e.g. yield, efficiencies, etc.),  
481 the model responds to variations in the performance of the individual unit-processes and allows users to adapt a specific  
482 biorefinery configuration. Here, the environmental impacts of the entire technology systems were calculated by one-at-a-  
483 time changes in parameter values, from a low conversion efficiency (25%) to a complete conversion (100%). For example,  
484 for fermentation of C5 sugars, only the fermentation efficiency was changed with all other parameters unchanged; the  
485 parameter values (0%, 25%, 50%, 75% and 100%) were selected for illustrative purposes

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**Fig. 4** An overview of the process-oriented LCA model response, in terms of global warming, GW, ( $\text{kgCO}_2\text{-eq}\cdot\text{kg}_{\text{ww}}^{-1}$ ) and mass/energy balance ( $\text{MJ}\cdot\text{t}_{\text{ww}}^{-1}$ ), to (one-at-the-time) unit-process performance variations (i.e. 0%, 25%; 50%; 75%; 100%): 3a) hemicellulose conversion efficiency in hydrolysis, 3b) cellulose conversion efficiency in hydrolysis, 3c) C5 sugars conversion efficiency in fermentation, 3d) C6 sugars conversion efficiency in fermentation. The feedstock considered is wheat straw. NG: natural gas; GS: gasoline

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557 As the results demonstrate, process parameters play an important role: the user can modify the mass and energy  
558 balances (here represented by the process-outputs) with a direct effect on the associated environmental impacts (here  
559 represented by GW). In this example, increased efficiency of cellulose hydrolysis leads to better GW performance (Fig.  
560 3b); this is reflected by the increased production of liquid fuel (ethanol) and the decreased production of solid fraction  
561 (sometimes called solid biofuel) resulting in the decreased substitution of natural gas combustion. In addition, increasing  
562 the fermentation efficiency of C6 sugars leads to better GW performance (Fig. 4d); also in this case, fuel production was  
563 increased, but now the liquid fraction (sometimes called molasses) decreased, thereby resulting in lower biogas production  
564 and lower substitution of natural gas combustion. In Fig. 4, for a cellulose hydrolysis efficiency of 0% the associated GW  
565 performance was  $-269 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ ; for an efficiency of 25%, the associated GW performance was  $-339 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ ;  
566 for an efficiency of 50%, the associated GW performance equalled  $-409 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ , for 75% it was  $-479 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$   
567 and for 100% it was  $-549 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ . Such direct proportionality between the energy/mass balances  
568 and the GW impacts may not necessarily have a direct effect on full scenario results as also framework conditions may  
569 be important, e.g. type of substituted energy, system boundaries, and process configurations. Furthermore the linear results  
570 are due to the equations applied in the case example, the model could just as well have been used for cases with  
571 exponential changes, or more scattered results if conditions for flow properties were applied in the model. These aspects  
572 can, however, be captured by the process-oriented LCA model either by adjusting parameters, changing the mathematical  
573 relationships involving the functions introduced earlier, or choice of background process data and interactions with the  
574 background system. For further details of the biorefinery modelling results involving variations in parameter efficiencies  
575 and associated GW impacts, please see Online Resource, Section S7, Tab. S7.1, S7.2 and S7.3.

576 Overall, similar results and trends were obtained for the two other feedstock types, beet top and wild grass, i.e.  
577 higher efficiencies provided larger environmental savings (see Online Resource, Section S8, Fig. S8.1 and S8.2 for the  
578 results). Differences in biochemical and physical properties between wheat straw, beet top and wild grass were reflected  
579 in the results by different “levels”. With a cellulose hydrolysis efficiency of 0%, the associated GW performance for beet  
580 top was  $-55 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$  and for wild grass  $-37 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ ; for an efficiency of 25%, the associated GW  
581 performance for beet top was  $-61 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$  and for wild grass  $-51 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ ; for an efficiency of 50%, the  
582 associated GW potential was respectively  $-67$  and  $-65 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ , while for 75% it was  $-73$  and  $-79 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$   
583 <sup>1</sup>, and  $-79$  and  $-93 \text{ kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$  in the case of 100%. While a similar trend in results can be expected, the model  
584 demonstrates the relative importance of the hydrolysis and fermentation steps for the three different feedstocks and  
585 thereby transparently explains the difference in results between the cases. This demonstrates that the model can be applied  
586 to technology cases with different process configurations (illustrated here by different efficiencies of unit-processes and  
587 subsequent changes in material and substance flows) and can accommodate different input-feedstock properties in a  
588 flexible manner.

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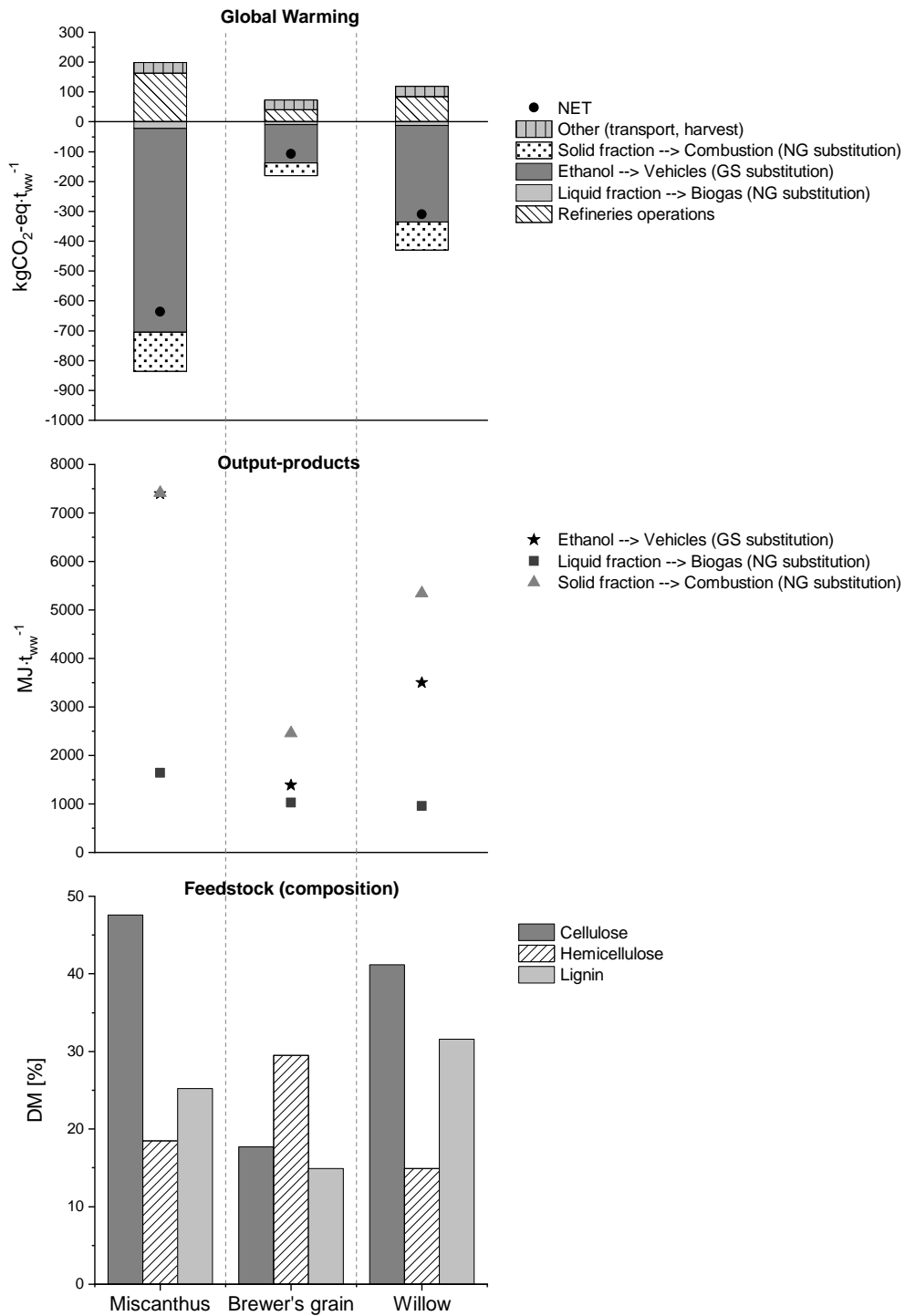
### 590 **3.2 Importance of input-feedstock characteristics**

591 The feedstock characteristics play an important role for the biorefinery performance, both with respect to GW  
592 ( $\text{kg CO}_2\text{-eq}\cdot\text{t}_{\text{ww}}^{-1}$ ) and output-products (e.g.  $\text{MJ}\cdot\text{t}_{\text{ww}}^{-1}$ ) as illustrated in Fig. 5.

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**Fig. 5** Process-oriented LCA model response, in terms of global warming, GW, ( $\text{kgCO}_2\text{-eq.kg}_{\text{ww}}^{-1}$ ) and mass/energy balance ( $\text{MJ.t}_{\text{ww}}^{-1}$ ), to three different feedstocks (i.e., *Miscanthus*, brewer's grain and willow) having different shares of cellulose, hemicellulose and lignin. NG: natural gas; GS: gasoline. For these three biomasses the values of the parameters used are: in hydrolysis, a cellulose and a hemicellulose conversion efficiency of 95% and 75% respectively, and in fermentation and distillation the conversion efficiency of 88% for both C5 and C6 sugars

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635           Among the three biomasses addressed here, *Miscanthus* has the highest cellulose content (CE = 47.6 %<sub>DM</sub>),  
636 brewer's grain has the highest hemicellulose content (HC = 29.5 %<sub>DM</sub>), and willow the highest lignin content (LG = 31.6  
637 %<sub>DM</sub>). In Online resources, Section S9, Tab S9.1 presents key characteristics and properties of these three biomasses. The  
638 cellulose, hemicellulose, and lignin contents for these three biomasses are shown in Fig. 5. The conversion efficiencies  
639 considered were: 95% and 75% for cellulose and hemicellulose respectively during hydrolysis, and for both C5 and C6  
640 sugars it was 88% during fermentation and distillation.

641           Considering the three main products of the biorefinery (ethanol, solid and liquid fraction), cellulose and  
642 hemicellulose affect mostly the production of ethanol and the liquid fraction as these molecules can be hydrolysed into  
643 chains of monosaccharides (e.g. glucose) used in the fermentation to produce ethanol and CO<sub>2</sub>. Lignin represents the  
644 carbon pool that in a biorefinery leads to the formation of the solid fraction output unless pretreatment is applied, together  
645 with non-hydrolysed material. With this in mind, based on the composition of the three feedstocks, *Miscanthus* generated  
646 more ethanol (7400 MJ·t<sub>ww</sub><sup>-1</sup>), followed by willow (3500 MJ·t<sub>ww</sub><sup>-1</sup>) and brewer's grain (1400 MJ·t<sub>ww</sub><sup>-1</sup>). Considering the  
647 solid fraction, although willow has the highest lignin content *Miscanthus* provided the largest solid fraction (7200 MJ·t<sub>ww</sub><sup>-1</sup>  
648 <sup>1</sup>), due to the larger amounts of unconverted sugars (dry basis). The liquid fraction is influenced mainly by the  
649 fermentation and distillation process. For this reason, *Miscanthus* provided the highest liquid output (1600 MJ·t<sub>ww</sub><sup>-1</sup>)  
650 followed by brewer's grain (1000 MJ·t<sub>ww</sub><sup>-1</sup>) and willow (960 MJ·t<sub>ww</sub><sup>-1</sup>). In this illustrative example, the conversion of all  
651 three biomasses provided net GW savings as no upstream activities (e.g. production) and indirect effects (e.g. land-use  
652 changes) were included. The largest savings were obtained from *Miscanthus* due to its higher dry matter content. These  
653 results were in accordance with Parajuli et al. (2017), who showed that the high dry matter and energy yield of the input-  
654 feedstock material can contribute to a better environmental performance. In addition, the relevance of conversion  
655 efficiencies of feedstock properties (e.g. carbohydrates) in the biorefinery processes was highlighted in Parajuli et al.  
656 (2017), in agreement with this study.

657           While the influence of feedstock choice on the LCA results have been evaluated previously in the literature (e.g.  
658 Bernstad Saraiva A 2017; Tonini et al. 2016 b), the above process-oriented assessment approach demonstrates the added  
659 insight of the importance of individual unit-processes (and potentially also parameter choices as illustrated in the previous  
660 section). Particularly, the inter- and intra-process transition, the material transformation due to the process specificities  
661 and the feedstock specificities (e.g. the importance of feedstock properties and their availability to be degraded or  
662 converted into different products), and their consequences in terms of environmental impacts.

663

## 664 **4 Discussion**

### 665 **4.1 Novel insights from process-oriented modelling**

666           The process-oriented approach focuses on the evaluation of process relationships through subdivisions of technologies  
667 into unit-processes and appropriate linking of process material inputs with transformation and process-outputs. In  
668 previous literature (e.g. Tonini et al. 2016 a, b), these aspects have been demonstrated as critical for the LCA results and  
669 interpretation, in particular in relation to integrated technologies such as biorefineries where the feedstock characteristics  
670 and the biorefinery outputs are interdependent and further affect the downstream substitutions (e.g. energy, feed,  
671 materials). One of the most notable advantages of the process-oriented modelling approach is the possibility of

672 implementing new (unit)processes by using operators in a single modelling tool such as EASETECH, rather than requiring  
673 a combination of several tools as illustrated by previous literature (e.g. in Tonini et al. 2016 a, b, and Vadenbo et al. 2018,  
674 where a combination of Matlab, Gams, and SimaPro was applied).

675 Mathematical equations describing the input-output relationships are integrated within the model itself and  
676 default parameter values can be further adjusted by the users. The subdivision into unit-processes is important for  
677 identification, quantification and evaluation of intermediate process-outputs within the system. Further, the process  
678 parameters and associated mathematical relationships themselves may be selected to appropriately represent operational  
679 parameters that can be recognised by users and more easily adjusted to accommodate specific case-studies and industry  
680 data. Quantification of the intermediate products linking individual unit-processes allows evaluation of the environmental  
681 performance of these unit-processes, which may further allow identification of technology hotspots at a much more  
682 detailed level than traditional “black-box” modelling approaches, both in terms of production and emissions. This is fully  
683 in line with existing recommendations, e.g. by ILCD guidelines (EC-JRC 2010) and strongly highlighted in Jacquemin et  
684 al. (2012).

685 The process-oriented modelling approach enables more control of the material, energy and substance flows  
686 within the analysed technologies. This is particularly important in relation to integrated technologies such as biorefineries  
687 or many waste technologies for which intermediate products affect the subsequent processing; an aspect that black-box  
688 approaches cannot capture (Maes et al. 2015). Modelling a biorefinery technology within EASETECH following the  
689 process-oriented approach offers an “active” material flow system represented by the established input-output  
690 relationships and parameters. This material flow system is linked to environmental emissions and output-product  
691 substitutions associated with the LCA scenarios; thereby a direct link between input-feedstock composition, process  
692 operation and environmental performance is established. For example, higher hydrolysis and fermentation efficiencies  
693 incur larger ethanol production with lower solid and liquid residue quantities, thereby increasing gasoline substitution and  
694 lowering natural gas substitution. Although purposely kept simple in this illustrative case-study, interactions between the  
695 foreground and background systems can be easily modelled with appropriate selection of parameters. The conversion of  
696 biochemical properties of the feedstock into the biorefinery products depends on the type of feedstock and its degradability  
697 under the specific operating conditions of the technology. All such aspects can be addressed and evaluated by the proposed  
698 process-oriented modelling approach.

699

## 700 **4.2 Implications for LCA**

701 Subdividing the technology into relevant unit-processes and establishing appropriate input-output relationships  
702 including operating parameter variations allow a direct response of the LCA model with respect to potential environmental  
703 impacts. While subdivision into smaller units has been suggested in previous literature, this has mainly been discussed  
704 from the perspective of Maes et al. (2015) rather than with the intention of Götze et al. (2014) and Papadokonstantakis et  
705 al. (2016) as suggested here for the process-oriented approach. Only few studies have discussed the potential of  
706 establishing operational relationships and more “technology relevant” parameters (e.g. Portha et al. 2010; Kikuchi et al.  
707 2014). As previously indicated, the ability to “track” intermediates and conversion of individual input-material fractions  
708 is essential for LCA modelling of multi-output technologies (e.g. Astrup et al. 2018), although relatively few LCA studies  
709 take this aspect seriously. With a black-box approach, where unit-processes may be combined even if they are physically  
710 separated, relevant disaggregation of the environmental impacts associated with individual outputs may not be possible

711 (e.g. Jacquemin et al. 2012). As the process-oriented modelling approach attempts to disaggregate technology and process  
712 elements into individual units reflecting the actual process flow and conversion steps, the process-oriented approach can  
713 facilitate easier compliance with the recommendations provided by current ISO standards and ILCD guidelines with  
714 respect to multi-functionality. In the case of LCA modelling of material and resource technology systems, we suggest that  
715 the process-oriented approach is a needed development from black-box approaches and that these cannot be considered  
716 state-of-the-art for such systems. We envision that further development of process-oriented inventories may offer a route  
717 to avoid the current challenges of multi-functionality associated with complex multi-output technologies.

718 LCA studies are also sometimes used to assess the environmental performance of technologies prior to  
719 commercialisation and full-scale implementation, e.g. prospective assessment of emerging technologies (Arvidsson et al.  
720 2017). From a black-box modelling perspective, such assessments pose specific challenges with respect to data  
721 uncertainties, process configurations, potential performance improvements, etc. as these aspects are typically aggregated  
722 within the technology inventory thereby limiting transparency. Process-oriented modelling, on the other hand, allows  
723 disaggregation and establishment of appropriate data relationships. Thereby the uncertainties and importance of individual  
724 process parameters may be evaluated directly and linked to the environmental performance of the technology in question.  
725 This makes process-oriented modelling particularly relevant for LCA assisted technology developments and upscaling  
726 activities, as the assessment results allow identification of process hotspots that may otherwise remain un-evaluated. We  
727 envision that these aspects are particularly important in relation to integrated and multi-output technologies as part of  
728 circular (bio)economy initiatives.

729

### 730 **4.3 Further research and perspectives**

731 As developed and implemented in this study, the process-oriented modelling approach represents a first attempt  
732 to demonstrate applicability and potential. Future research is intended to focus on improving the existing model and  
733 extending the process-oriented modelling approach to a wide range of material-centric technologies, e.g. anaerobic  
734 digestion, thermal pyrolysis and gasification, thermal combustion, and biomaterial production facilities. This requires  
735 identification and appropriate implementation of relevant process relationships between input-resources and materials  
736 (e.g. chemicals, energy, etc.) and process-outputs and emissions. While EASETECH offers a unique basis for this as the  
737 modelling is already based on material flows, implementation of new process-oriented technology models nevertheless  
738 requires considerable effort (see Online Resource as an example for a biorefinery). However, once a process-oriented  
739 model is established, subsequent adjustments can be achieved simply by changing the appropriate parameters (assuming  
740 the fundamental process configuration remains appropriate). As mentioned earlier (section 2.3.1), to focus on the  
741 technology modelling, we deliberately excluded the upstream impacts associated with diverting the feedstock from its  
742 current use(s) or with land use changes. Such impacts have been earlier estimated in the order of 19-88 kg CO<sub>2</sub>-eq ·t<sub>ww</sub><sup>-1</sup>  
743 for wild grass and wheat straw, 191-360 kg CO<sub>2</sub>-eq ·t<sub>ww</sub><sup>-1</sup> for perennial energy crops as willow and *Miscanthus*, and 265-  
744 287 kg CO<sub>2</sub>-eq ·t<sub>ww</sub><sup>-1</sup> for agro-industrial residues as beet top and brewer's grain (Tonini et al 2016 a, b). These figures  
745 should be added to the results quantified in this study to obtain a full picture of the Climate Change impact of the studied  
746 scenarios.

747

## 748 **5 Conclusion**

749           The study developed a process-oriented environmental life cycle assessment modelling framework, implemented  
750 this in EASETECH and applied this on a biorefinery case-study for illustrative purposes. The process-oriented modelling  
751 framework provides an improved representation of complex technologies allowing definition and evaluation of process  
752 relationships between inputs and outputs. This is particularly important for integrated technologies comprising individual  
753 unit-processes, e.g. biomass conversion and management of residual resources. Traditional black-box modelling  
754 approaches, represented by most existing LCA models, do not offer similar possibilities for detailed evaluation of  
755 processes and technologies nor allow the same level of transparency with respect to inventory definition. The process-  
756 oriented modelling framework provided by this study allows consistent balancing of material, fraction, and substance  
757 flows within the technology system and, through mathematical expressions, at the same time establishment of the process  
758 relationships that affect these flows through transition and transformation within each single unit-process. Based on the  
759 biorefinery case-study, the advantages of the modelling approach were demonstrated: input-feedstocks and key process  
760 operational parameters can be adjusted easily in order to evaluate process performance and the importance of feedstock  
761 properties. This facilitate quantification of individual/intermediate (bio)product flows within unit-processes; this has not  
762 been possible previously. The potential implications of process-oriented modelling are considerable, e.g. in relation to  
763 novel insights associated with uncertainty evaluation, technology upscaling and process optimisation.

764

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768

#### 769 **Conflict of interest**

770           The authors declare that they have no conflict of interest.

771

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