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CO₂ Capture through Electro-conductive Adsorbent using Physical Adsorption System for Sustainable Development

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Abstract:

The most critical energy and environmental challenge that our planet is facing today is to minimize the dependence on fossil fuels. Carbon dioxide may be of utmost significance as a solution of this issue through realization of carbon neutral energy cycle. Potentially, this could be achieved through the carbon dioxide capture as the urgent response to ongoing climate change. Activated carbon (AC) adsorption is one the most effective, environment friendly and techno-economic process for the carbon capture. In the current research, an electro-conductive activated carbon was prepared by mixing powdered activated carbon (PAC) with an electro conductive polymer (ECP). Different ratios of 0, 25, 50, 75 and 100 wt. % of ECP with PAC were used for the different analysis of activated carbons in a gas mixture of CO₂/N₂ using a physical adsorption system. Adsorption and desorption analyses, capacities of the process and desorption effects were examined. Electro conductive polymers (ECP) were mixed with AC samples, where breakthrough time was increased up to 400% when mixed with the PAC for CO₂ adsorption. Following adsorption analysis, desorption of activated carbons was conducted with different potentials. It was revealed that mixing could help the PAC sample to overcome the packing issue to increase the breakthrough capacity and the volumes before and after the breakthrough adsorption in the packed bed systems. The desorption rates of the PAC sample were also enhanced, and fast desorption was observed when mixed with ECP. It is envisioned that this method is very much promising carbon capture method for the techno-economic feasibility and sustainable development of the environment.

Key Words: Activated carbon, Carbon capture, Electroconductive polymers, Physical adsorption, sustainable development

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1. Introduction

Due to the more than 39% increase in atmospheric CO₂ the average global temperature has risen to 0.8 °C during the past century. According to an estimate, the equivalent CO₂ concentration in the atmosphere reaching to about 1600 ppm, the green-house gases has emissions would rise from 30-90% over the level of 2000 within next 10 years i.e. by the end of 2030. CO₂ is also deemed to intensify the contamination of CO, apart from its importance as GHG, when both exist in the same gas (Derakhshan-Nejad, Sun et al. 2019). Hence, the apprehensions regarding GHG emissions have triggered massive interest in exploring the domain of CO₂ capture to deal with the environment and sustainability issues (Yang, Lee et al. 2017). Increase in CO₂ causes stress on earth's climactic system and one of the most feasible method recognized up till now to reduce this stress is carbon capture technology (Choi, Piao et al. 2017, Saeed, Farooq et al. 2019).

The commercial technologies used for carbon capture are mainly absorptive and adsorptive processes, as well as processes based on membrane filtration or cryogenic separation (Wang, Yu et al. 2016, Bogusz, Oleszczuk et al. 2017, Budhathoki, Ajayi et al. 2019, Wilberforce, Baroutaji et al. 2019). These established techniques are facing significant challenges in terms of energy consumption and operating costs, which may add substantial costs as well (Thrän, Billig et al. 2014, Kougias, Treu et al. 2017).

The water scrubbing method is currently the most commonly used method for carbon capture (Farooq, Chaudhry et al.). The driving force for water scrubbing is operational track record and ease of use, while its main issue is high operating costs and water consumption (Rajendran, Browne et al. 2019). Pressure swing adsorption (PSA) is an efficient method, but its operational and capital costs are very high (Bauer, Persson et al. 2013). Separation of gases by membrane is a safe and efficient method and its cost are not high, but it has regenerative, scale-up and operational issues (Díaz et al., 2015, (Farooq, Qamar et al. 2016, Zhang, Xin et al. 2019). Membrane-based gas separation have typically low capital cost for the gas permeation processes (Scholz, Melin et al. 2013). Membranes have expensive operation and maintenance cost (Ryckebosch, Drouillon et al. 2011). Membrane based separation tends to be more cost-effective in manufacturing relatively low-purity products. A summary of the techno-economic analysis for producing 97% methane at 99% recovery has been described by Shao et al. (Shao, Dal-Cin et al. 2012). Cryogenic systems are efficient and environment friendly, but these are costly because of the complex set-up to gain the required cryogenic conditions and used only

at very large-scale industrial plants, since cost and safety is a main concern (Farooq, Almoustapha et al. 2018, Song, Liu et al. 2019).

Adsorption by activated carbon, on the other hand, provides environment friendly solutions with reference to safety, applicability, and low energy use (Jayawardhana, Mayakaduwa et al. 2017, Rostami, Anbaz et al. 2018). Activated carbons are less costly comparison with silica, zeolite and alumina. The problems associated with activated carbon is the slow regeneration, which leads to high operational cost (Wang, Yao et al. 2016). Also, due to the pressure drop of powdered activated carbons (PAC) in the packed beds, it is recommended that PACs could be added with some other materials/ binders. It could be used with mixing to avoid the pressure drop issue (Bandosz 2006). A conductive material addition is suggested which could be helpful, as conductive polymers are cheaper.

Normally, at industrial level the exhaustive adsorbent is replaced with the fresh adsorbent (Farooq 2018). Presenting a cost-effective system for ACs as analysed by this paper could improve the application of AC to a greater extent. Since the activated carbon is a moderate conductive material, a low volt potential system could be helpful to disturb the adsorption forces between the adsorbate and the gas molecules, which could lead to fast desorption.

In the present study, the adsorption and desorption analysis of CO₂ were conducted using physical adsorption system. Repeated adsorption and desorption cycles with CO₂ were conducted to establish breakthrough times, adsorption/desorption volumes and capacities of electro-conductive activated carbons, where the desorption was carried out with low electric potentials of 10, 20 and 30V and compared without potential system. The results revealed that this system helped for the enhanced adsorption and fast desorption compared to the conventional system and accessible CO₂ adsorption sites could be regenerated with desorption time shorter than the adsorption breakthrough time. Also, the adsorption and desorption cycles can be obtained with a classical two column system, which could lead towards a more efficient process.

2. Material Characteristics

Table 1 summarise the characteristics of activated carbon sample, which were conducted for surface area, elemental, proximate analysis and conductivity. The electro-conductive activated carbon was prepared by mixing the powdered activated carbon (PAC) sample with the electro-

conductive polymer (ECP). The PAC is a steam activated carbon with the high filtration characteristics. It is produced under highly controlled conditions to insure consistent quality. The electro-conductive polymer (ECP) is a permanently electrically conductive thermoplastic based low-density polyethylene (LDPE) blends with different amounts of poly (ethylene-vinyl acetate) (EVA).

Table 1 Characteristics of powdered activated carbon

Property	Activated carbon	
BET Surface area ^a	(m ² /g)	758
Micropore volume ^b	(cm ³ /g)	0.169
Average pore radius ^c	(Å)	12.913
Micropore area ^a	(%)	66.6
Mesoporous area ^a	(%)	33.2
Macro pore area ^a	(%)	0.2
Carbon	(%)	81.38
Hydrogen	(%)	0.2
Nitrogen	(%)	0.11
Oxygen ^d	(%)	0.71
Moisture content	(%)	0.9
Volatile matter	(%)	2.2
Fixed carbon	(%)	80.3
Ash content	(%)	16.7

^aMeasure from adsorption isotherm

^bMeasured by application of t-plot

^cMeasured by the nitrogen adsorption isotherm using BJH method

^dOn difference 100 – [carbon+hydrogen+nitrogen+moisture+ash]

3. Experimental procedure

The activated carbon sample was mixed with electro conductive polymers (ASTM method) to observe the effect of mixing of electro conductive polymers with the activated carbon. The CO₂ adsorption and desorption analyses with the activated carbon samples were conducted in a packed bed of electro-conductive activated carbon as shown in Figure. 1. Glass wool was used

at the bottom to avoid the adsorbent slippage, whereas, the filter paper was used at the top because of smooth passage of the gas in the bed. The gas manifold system comprises of different lines each fitted with volume flowmeters ranging from 1 to 100Nml/min. The system was equipped with a mass-spectrometer with the mass-soft for the continuous gas analyzing. Concentration of the carbon dioxide and nitrogen was analyzed before and after the activated carbon rig.

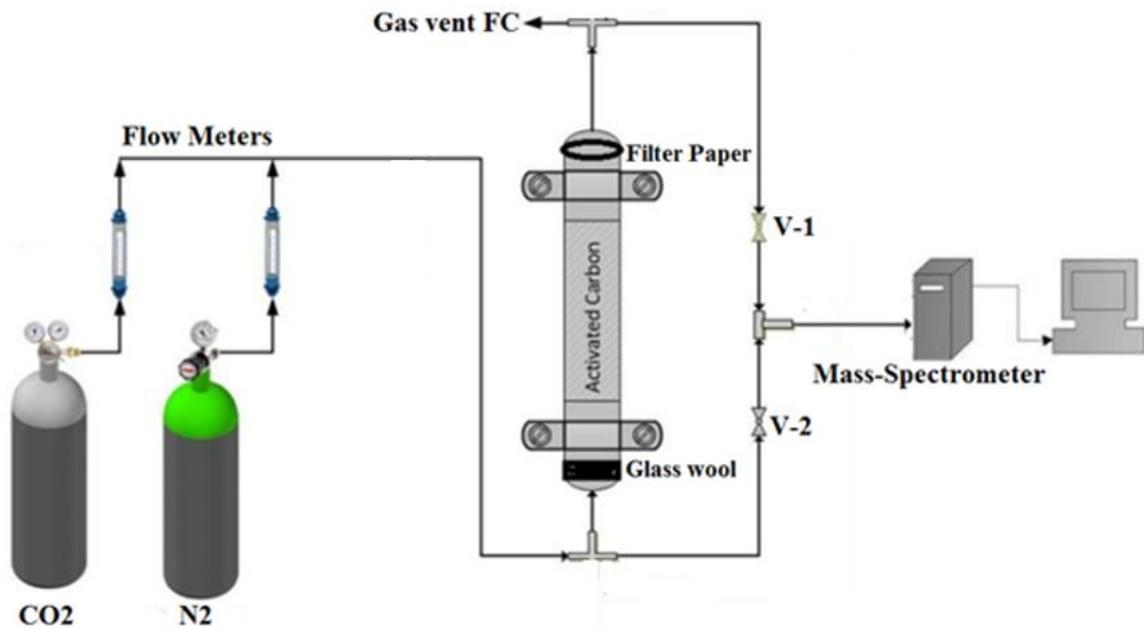


Figure 1. Experimental setup of Physical Adsorption System (Farooq, Bell et al. 2017)

[modified from author's own experimental set-up]

4. Results and Discussions

4.1 Effect of CO₂ Adsorption on PAC sample with mixing ratios of 0, 25, 50, 75 and 100% with ECP

Figure 2 compares the PAC adsorption with different mixing ratios of 0, 25, 50, 75 and 100% with the ECP. Breakthrough capacities of these mixing ratios were calculated, and adsorption behaviour was analysed. It was observed that the breakthrough time for the PAC sample without mixing is about 50 seconds. The adsorption curve raised fast and reached at 20% carbon dioxide after 95 seconds. Afterwards, adsorption was comparatively slow, and 90% concentration was achieved after about 250 seconds, which is about 5 times slower than the initial 50% adsorption. After this, 75% PAC was mixed with 25% ECP and the same adsorption

process was repeated to observe the adsorption and breakthrough behaviour for the mixed sample. It was observed that the breakthrough time of the adsorption is 3.5 times longer than the PAC without mixing. After the breakthrough point, adsorption curve increased smoothly and 50% adsorption was achieved in 147 seconds, i.e. 3.2 times higher compared with the PAC100 sample. Accordingly, the adsorption cycle was carried out by mixing 50% electro conductive polymer with PAC, which shows an increase in the breakthrough time as 5.4 and 1.5 times than PAC100 and PAC75ECP25, respectively. Overall adsorption trend of this mixing ratio sample was observed very much similar to that of PAC75ECP25. The PAC sample was further mixed with a ratio of PAC 25% with 75% ECP, which shows 6% increased breakthrough time compared to the 50% ratio. Adsorption process was then observed for the electro conductive polymers, which shows a breakthrough time of 272 ± 43 seconds, which is 8, 2.7, 1.5 and 1.4 times more than the PAC100, PAC75ECP25, PAC50ECP50 and PAC25ECP75, respectively. This shows that a direct increase in the breakthrough time of the PAC with the addition of ECP, which greatly helped to increase the adsorption rate in the packed bed.

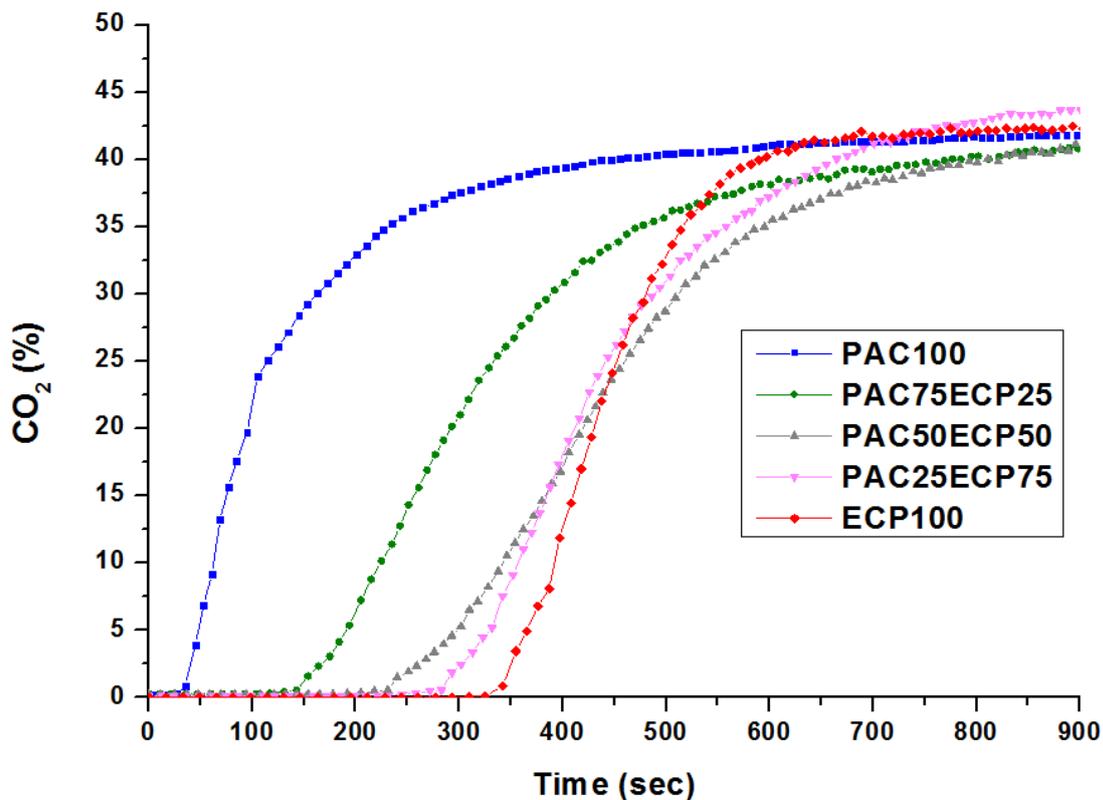


Figure 2 Effect of PAC adsorption at mixing ratios of 0, 25, 50, 75 and 100% with the ECP

4.2 Effect of adsorption breakthrough time of PAC mixing with ECP (wt. %)

Figure 3 compares the effect of adsorption breakthrough time of the PAC with different mixing ratios of the ECP from 0-100% with an increase of 25%. First point was taken from the PAC adsorption breakthrough curve, which gave a value of 40 ± 10 seconds. With the addition of 25% ECP with 75% PAC sample, the adsorption breakthrough time increased to 143 seconds, which is about 3.5% than the PAC 100% sample. The direct relation graph value should give a time of about 100 seconds, whereas, it was observed 43% higher value of adsorption time than the predicted linear relation. Analysis were continued with addition of further 25% of ECP sample in PAC with 50-50% of PAC and ECP, which enhanced the adsorption breakthrough time to 201 seconds. Repetition of the experiments with the same ratios, give very smooth values of 201 ± 17 , which improved the breakthrough 5.4 times than the PAC without mixing sample. The PAC sample was further mixed as PAC25ECP75, which shows consistency of increased breakthrough time of 231 seconds, which is about 8% longer. Further analysis was continued with ECP with 100% concentration which gives the breakthrough time as 272 ± 43 seconds. Since, the adsorption experiments were repeated over the different cycles, which gives good confidence level for the results. It shows very good linear relationship, which means that addition of the ECP with the PAC helps greatly to enhance the breakthrough time of the

powdered sample. The synergistic effect for the total adsorbed volume has been elaborated in the next section with the comparison of different mixing of the PAC with ECP.

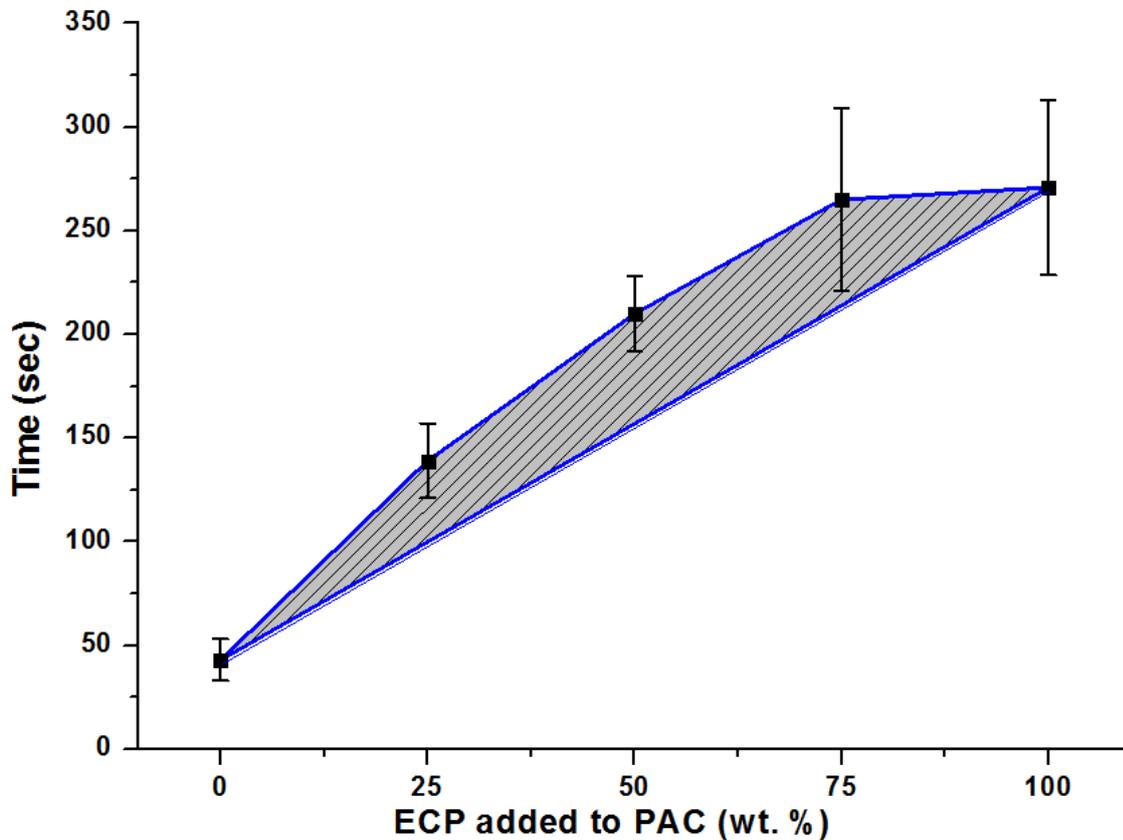


Figure 3 Effect of adsorption breakthrough time of the PAC with ECP

4.3 Comparison of CO₂ adsorption breakthrough time, volume, capacities, volume and synergistic effect of the PAC mixing with ECP

Table 2 compares the breakthrough time (B.T.), capacities, adsorption volumes, theoretical calculated volumes and synergistic effect of volume of the PAC sample mixed with different ratios of the ECP. Breakthrough volumes of adsorption gives very smooth increased values with the mixing of ECP in the PAC sample. The total theoretical breakthrough volume was calculated about 42 mL, whereas, adsorption volume was observed as 49 mL, which gives a 17 vol. % higher value. Subsequently, breakthrough volume for PAC50ECP50 was observed as 78 mL, which is 4 times more than PAC100. The theoretical breakthrough volume for this ratio was calculated as 67 mL, gives about 17% synergistic effect, which is very good outcome with the addition of ECP in the PAC sample. Accordingly, ECP sample was further 25% added in PAC sample, and the breakthrough volume for PAC25ECP75 was observed 83mL, with an increase of 6% than PAC50. The theoretical calculated breakthrough volume was 8mL higher than the total adsorption volume with a synergistic effect of 9.2%. It gives a clear depiction of

smooth incremental values of the rig adsorption capacity and volumes at different ratios. This means that 25% and 50% ratio have a good compatibility of the particle connection, which covers a reasonable space for bonding the particles. The [normalized rate of desorption](#) could be helpful to further explain the behaviour of the mixing of ECP with PAC.

The observed data corresponds to the experimental results, whereas the calculated data related to the actual calculations of ECP and/or AC sample(s) as it is. The total rig adsorption of PAC/ECP sample is 0.1% higher than the ECP. It shows that the mixing of the ECP with the PAC results in good synergistic results compared to as its own. Since, PAC has good surface area and porous structure, which results in low adsorption due to pressure drop in the packed column. The addition of ECP with the PAC helped to regain its actual capacity.

Table 2 Adsorption time, volume, breakthrough capacities and synergistic effect of PAC mixing with ECP

	Parameter		PAC 100	PAC75 ECP25	PAC50 ECP50	PAC25 ECP75	ECP 100
Observed	B.T. Time	(sec)	53.0	143.0	218.0	231.0	271.0
	B.T. Vol.	(ml)	17.5	49.2	77.7	83.0	116.0
	Vol. after B.T.	(ml)	56.5	68.4	92.8	63.4	49.0
	Total Vol.	(ml)	74.0	117.6	170.5	146.4	165.0
Calculated	Theoretical B.T. Vol	(ml)	17.5	42.1	66.8	91.4	116.0
	B.T. Ads.	(wt.%)	0.4	1.0	1.5	1.6	2.3
	Ads. After B.T	(wt.%)	1.1	1.3	1.8	1.2	1.0
	Rig. Ads.	(wt.%)	1.5	2.3	3.3	2.9	3.2
	Synergistic Effect of B.T.	(Vol. %)	0.0	16.8	16.4	-9.2	0.0

4.4 Effect of CO₂ desorption profiles on PAC with mixing ratios of 0, 25, 50, 75 and 100% with ECP

Figure 4 (a) and (b) compares the effect of desorption and [normalized rate of desorption](#) profile, respectively, for the PAC sample with different mixing ratios of 0, 25, 50, 75 and 100% with ECP, respectively. The 90% desorption of the PAC sample without any mixing of ECP was observed about 4 times longer compared with the 50% desorption. With the mixing of electro conductive polymer in the powdered sample helped to quick desorption, where by the addition of 25% ECP with 75% PAC reduced the 90% desorption to about half of the non-mixed PAC sample. After the observation of efficient behaviour of quick desorption mixing ratio was increased as 50-50% to observe the desorption behaviour, which shows 7% reduction at 50% desorption. However, with the 50-50% mixing ratio, 90% [normalized rate of desorption](#) of mixed sample was observed 4.3 times fast than the PAC75ECP25. Further mixing of sample was observed as PAC25ECP75, which shows 21% quick desorption at the rate of 50% desorption compared with the previous mixing of 50-50%. At the 90% [normalized rate of desorption](#) for this mixed sample, 40% efficient desorption was observed when compared with the PAC50ECP50 sample. Finally, the samples were compared with the ECP, which gives a very good direct linear relationship, and it was observed as almost 2.1 and 1.9 times fast desorption for 50 and 90% [normalized rate of desorption](#), respectively. Since, in the current section the [normalized rate of desorption](#) of the different mixing ratios of ECP with PAC sample were analysed, it may be important to observe the behaviour of the [normalized rate of desorption profiles](#) of these mixing ratios with different low potentials.

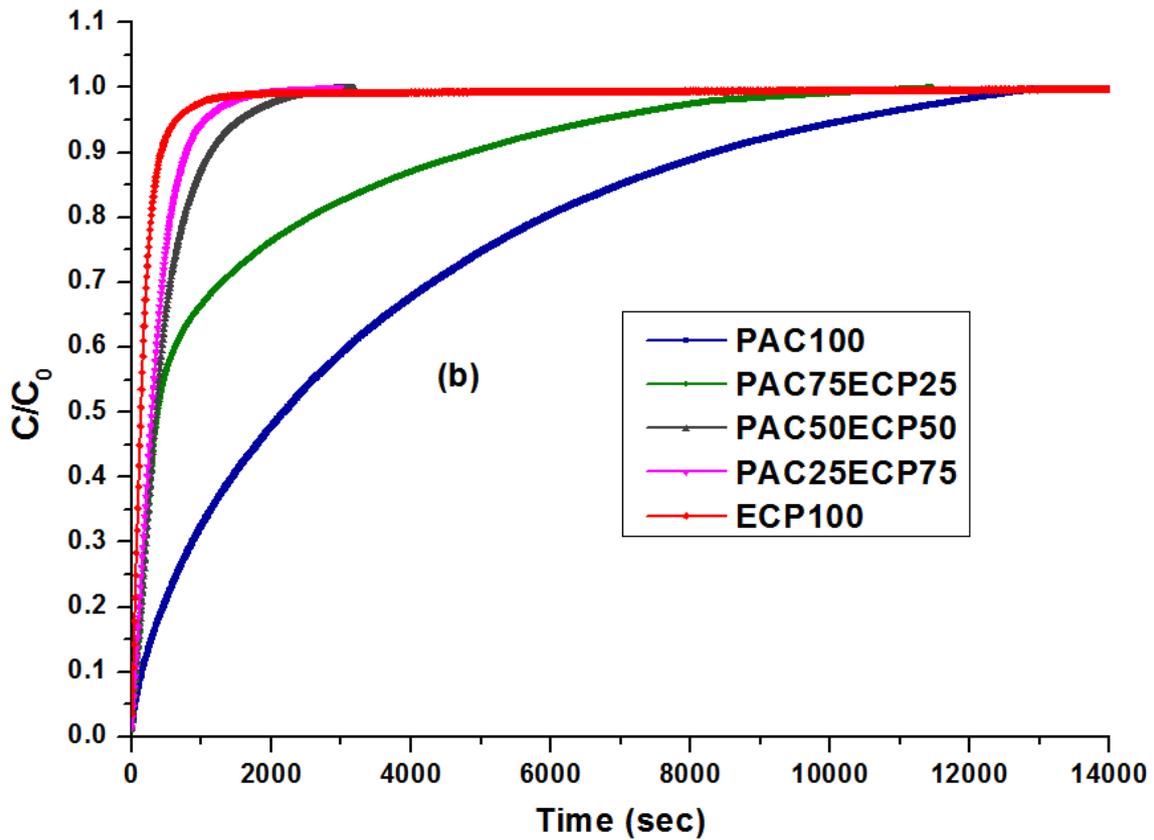
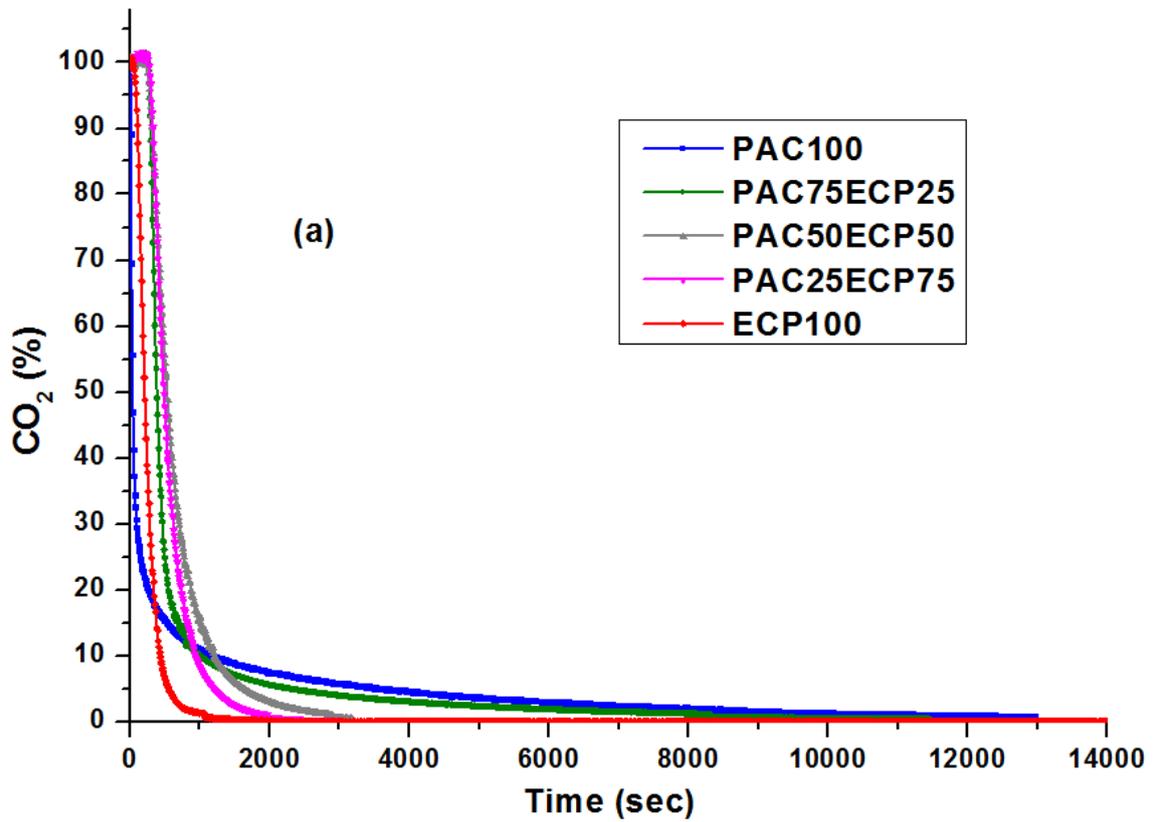


Figure 4 Mixing of PAC at ratios of 0, 25, 50, 75 and 100% with ECP (a) Effect of desorption (b) Profiles of normalized rate of desorption

4.5 Effect of 90% desorption reduction of 0 and 30v potential for PAC sample at mixing ratios of 0, 25, 50, 75 and 100% with ECP

Figure 5 and Table 3 compares the effect of reduction of 90% desorption of 0 and 30V potential of PAC with mixing ratios of 0, 25, 50, 75 and 100% with ECP. The 90% desorption of the PAC sample occurred at about 8,277 seconds without mixing. This time was reduced to 4,425 seconds with the 30V potential value, which is about 47% reduction in the desorption time. When the PAC sample was mixed with 25% ECP, a decrease of about 38% reduction was observed. This value found with similar linear behaviour, which was observed 25% for the 50-50% mixing ratio of PAC with ECP. With an increase in the ECP ratio to 75% in overall weightage of the sample, the reduction in desorption was observed as 15%. Whereas, without any mixing, ECP100 sample had the lowest value of 4.4 %. This behaviour of PAC shows a very smooth linear change in the sample with the ECP addition. However, there was no reasonable synergy observed.

Table 3 Effect of 90% desorption time of PAC mixing with ECP at 0, 10, 20 and 30V potential

Sample	Des. time at 0V	Des. time at 10V	Des. time at 20V	Des. time at 30V
	(sec)	(sec)	(sec)	(sec)
PAC100	8277	5029	4788	4425
PAC75ECP25	4834	4181	3860	3173
PAC50ECP50	1113	967	965	833
PAC25ECP75	788	672	672	673
ECP100	496	496	496	470

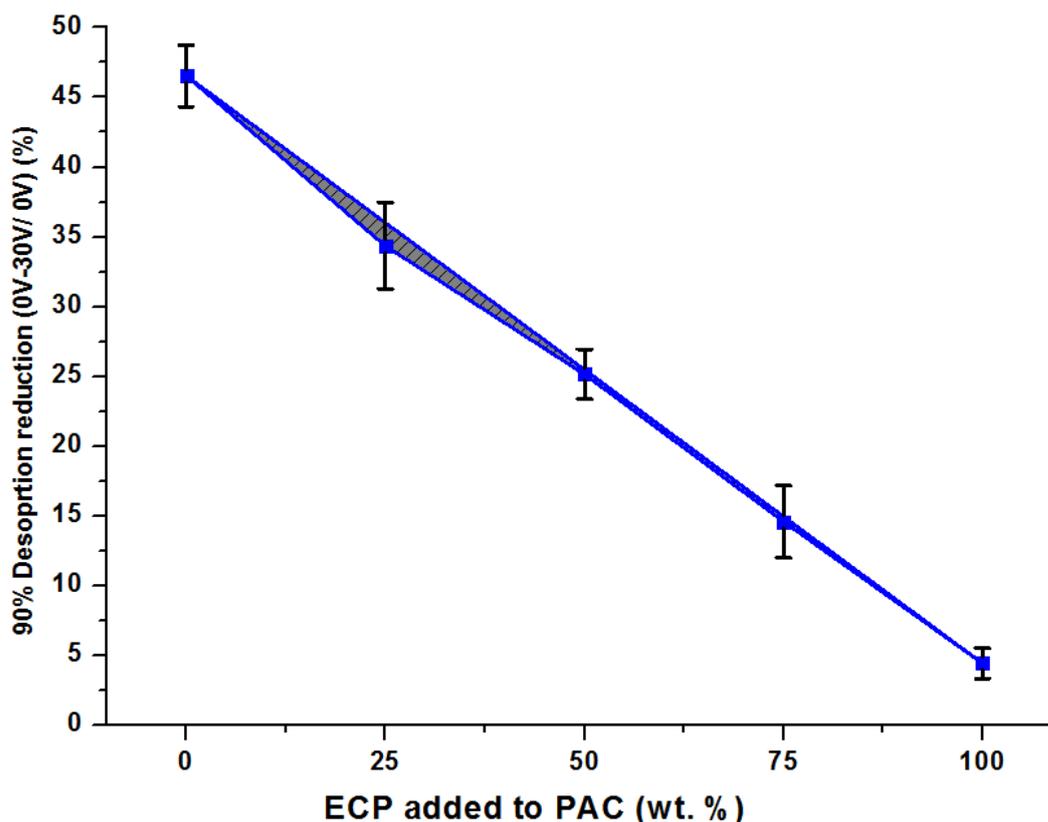


Figure 5 Effect of 90% desorption reduction of PAC mixing with ECP from 0 to 30V potential

5. Conclusions

It was concluded that the powdered activated carbon sample could be more effective for the adsorption and regeneration using physical adsorption system when used by adding with electro-conductive polymer. The electro-conductive polymers (ECP) used at different mixing ratios with the PAC shows very efficient results with increased breakthrough times compared with the non-mixed sample. Mixing ratio of ECP at 25%, 50% and 75% boosted the breakthrough times with 170%, 311% and 336% for the PAC sample. The synergistic effect was observed as 17% and 16% higher with 25% and 50% for the PAC sample, respectively. It is therefore concluded that adsorption and desorption of CO₂ using physical adsorption system through electro-conductive activated carbon is a new way of adsorption and regeneration of adsorbent as compared to the system without potential. It is cost effective, safe and environment friendly. It can be used for quicker desorption of powdered activated carbon without using a pressure or temperature intensive techniques of regeneration, since regeneration can be done without the addition of any extra energy into the system.

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