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On the Influence of Segment Length in PW-tsm Doppler Systems

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Abstract – Two different signal processing techniques can be used for blood velocity measurements with Pulsed Wave (PW) Doppler. These are based on measurement of phase shift and time shift, respectively. The first technique is based on a correlation measurement scheme, which features inherent velocity aliasing. The second technique, which is based on the location of the peak in the cross-correlation function of consecutive received signal segments, is in principle free of this problem. However, as noise are present and finite signal segments are used, only an estimate of the cross-correlation function is available. Thus, as detection of velocities greater than the aliasing velocity will require searching for a peak in a function with several peaks, the method is prone to detection of incorrect peaks. This paper investigates the effect of the length of the signal segments to be cross-correlated on the probability of incorrect detection.

I. INTRODUCTION

Recent advances in blood velocity measurements with pulsed (Doppler) ultrasound have made possible two-dimensional mapping of the velocity of moving blood. In this technique, short tone burst of ultrasound in the 1 - 15 MHz range is transmitted, and using the fact that the received signal is compressed/expanded due to the Doppler effect, the variation in time shift between transmitted and received signals can be measured. This can either be done by interpreting this time variation as a phase shift, or measuring it directly by cross-correlation. These two techniques are called PW-*psm* (phase shift measurement) and PW-*tsm* (time shift measurement), respectively.^[3] In the latter technique, for each range cell, a segment (of length T_w) of one received signal is windowed out, delayed a time equal to the pulse repetition period, T_r , and cross-correlated with the next received signal. This will produce a cross-correlation function which oscillates with the transducer frequency. Assuming that the received signals have identical shape, the cross-correlation function will have a true peak at a time lag, t_0 , which equals the relative time delay between two received signals. From this the velocity in direction of the transducer can be calculated as follows: $v = ct_0/(2T_r)$, where c is the propagation velocity of sound in the medium. An example of the cross-correlation

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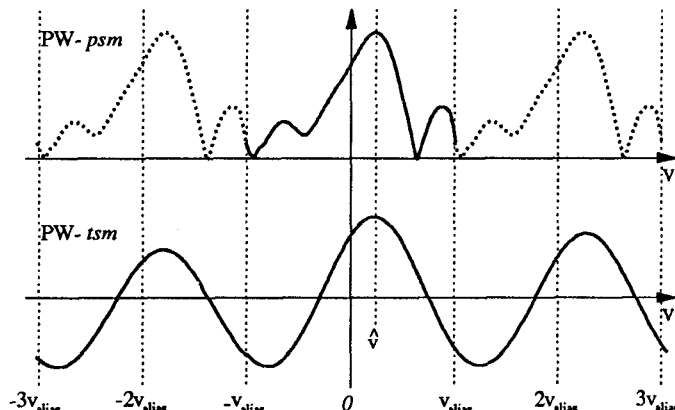


Fig. 1. Example of Doppler spectrum (top) for PW-*psm* and cross-correlation function (bottom) for PW-*tsm*.

function is indicated in Fig. 1, which also shows an example of a Doppler spectrum obtained with a PW-*psm* system. While only velocities within the aliasing velocity range $[-v_{alias}, v_{alias}]$ can be detected with the PW-*psm* system, any velocity can in principle be detected with the PW-*tsm* system. However, as seen from Fig. 1, there is a risk of detecting a sidelobe. The probability of detecting a sidelobe (*i.e.* incorrect detection) decreases with increasing signal to noise ratio and increasing bandwidth of the transmitted pulse.^[1,2] In contrast, the probability is increasing with increasing loss of coherence between consecutive received signals (which is due to beam intensity modulation and velocity variation within the range cell)^[1,3]. Finally, as short signal segments (of length T_w) are used to calculate the cross-correlation function, only an estimate of this function is obtained. However, the longer the signal segments the better the estimate. This is of course consistent with the generalized Heisenberg uncertainty principle, in the sense that a particle's position and velocity can not be found simultaneously with arbitrarily high precision. In essence, a large segment length will yield a large range cell but at better velocity estimate (ignoring the velocity variation inside the range cell).

II. SIMULATION STUDIES

Simulations showing the effect of varying the integration time, T_w , in the cross-correlation function (*i.e.* the size of the range cell) have been performed. These simulations are carried out with the following parameters: rms Bandwidths of transmitted, received and noise signals: 1.2 MHz; Transducer

frequency: $f_0 = 7$ MHz; S/N: 15 dB; $T_r = 66.68$ μ s; Figs. 2 and 3 are based on 2 and 3 transmissions, respectively; $v_{alias} = 0.8$ m/s; The sampling frequency is 100 MHz, and a parabolic fit is used for interpolation.

From Fig. 2 it is seen that the imprecision (coefficient of variation)^[3] is relatively unaffected by integration time, apart from minor effects for $T_w = 4/f_0$. An incorrect detection (*i.e.* detection of a sidelobe) is defined as occurring when a detected velocity is outside the range $[-v_{alias} + v_a, v_{alias} + v_a]$ where v_a is the actual velocity (x -axis). The risk of an incorrect detection is increasing with velocity, as the received signals to be cross-correlated becomes less alike, which will increase the relative value of the sidelobes shown in Fig. 1.

Applying a stationary echo-canceller (SEC) to the received HF signals has some interesting effects. First of all, at small velocities, consecutive received signals due to the flow are nearly identical. Thus, they cancel out, leaving only noise for the estimation. This results in a very high imprecision and incorrect detections. Second, at higher velocities two different effects are present:

When the time shift is near $(2n+1)/(2f_0)$, where $n = 0, 1 \dots$ the coherent signals are subtracted out of phase. However, when the time shift is around n/f_0 , the coherent signals are subtracted in phase, giving a degradation of the signal to noise ratio.^[2] This effect is only slightly visible in Fig. 3 ($v = 1.6$ m/s) due to the relatively high signal to noise ratio.

The second effect is due to interference in the cross-correlation function. When the SEC is used, three received signals are needed. If these are considered to be identical, but each time shifted a fixed amount, *i.e.* $g_2(t) = g_1(t-t_0) = g_0(t-2t_0)$, then the cross-correlation function

$$C(\tau) = \int [g_1(t) - g_0(t)] [g_2(t + \tau) - g_1(t + \tau)] dt, \quad (1)$$

will consist of three individual functions, where one of these

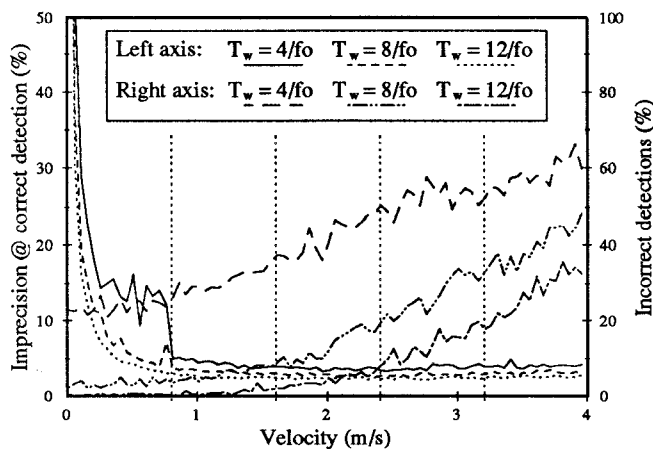


Fig. 2 Imprecision and probability of incorrect detection.

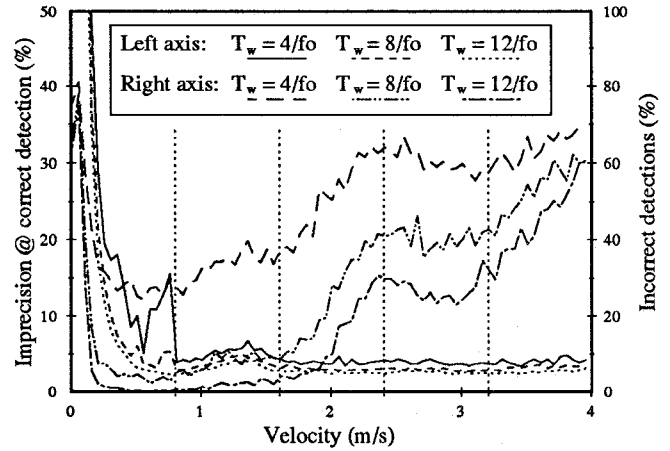


Fig. 3 Imprecision and probability of incorrect detection, when a stationary echo-canceller is used.

is the auto-correlation function of $g_1(t)$. For special values of t_0 (*e.g.* $t_0 = 3/(2f_0)$), this function will interfere with the sidelobes of the main cross-correlation function, thereby increasing the risk of detecting a sidelobe. This is clearly seen in Fig. 3, for $v = 2.4$ m/s.

CONCLUSIONS

It has been shown that increasing the segment length (T_w) of the signals to be cross-correlated diminish the risk of detecting an incorrect peak at the expense of degraded depth resolution. The probability has been graphed, and the effect of using a stationary echo-canceller has been demonstrated. Based on these observations, a scheme could be designated, where the approximate location of the peak is found with a large segment length, and then the precise location can be found by recalculating the cross-correlation function with a small segment length.

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