



Description of the Risø Puff Diffusion Model

Mikkelsen, Torben

Publication date:
1982

Document Version
Publisher's PDF, also known as Version of record

[Link back to DTU Orbit](#)

Citation (APA):
Mikkelsen, T. (1982). *Description of the Risø Puff Diffusion Model*. Risø National Laboratory. Risø-M No. 2361

General rights

Copyright and moral rights for the publications made accessible in the public portal are retained by the authors and/or other copyright owners and it is a condition of accessing publications that users recognise and abide by the legal requirements associated with these rights.

- Users may download and print one copy of any publication from the public portal for the purpose of private study or research.
- You may not further distribute the material or use it for any profit-making activity or commercial gain
- You may freely distribute the URL identifying the publication in the public portal

If you believe that this document breaches copyright please contact us providing details, and we will remove access to the work immediately and investigate your claim.

RISØ-M-2361

DESCRIPTION OF THE RISØ PUFF DIFFUSION MODEL

Torben Mikkelsen

Abstract. The Risø National Laboratory, Roskilde, Denmark, atmospheric puff dispersion model is described. This three-dimensional model simulates the release of Gaussian pollutant puffs and predicts their concentration as they are diffused and advected downwind by a horizontally homogeneous, time-dependent wind. Atmospheric characteristics such as turbulence intensity, potential temperature gradient, buoyant heat flux and maximum mixing depth have been considered.

INIS descriptors: ADVECTION; AIR POLLUTION; BOUNDARY LAYERS; CLUSTER EMISSION MODEL; COMPUTERIZED SIMULATION; DIFFUSION; EARTH ATMOSPHERE; HEAT FLUX; METEOROLOGY; PLUMES; SPATIAL DISTRIBUTION; TEMPERATURE INVERSIONS; TRAJECTORIES; TURBULENCE; WIND

UDC 551.510.4 : 681.3.06

October 1982

Risø National Laboratory, DK 4000 Roskilde, Denmark

ISBN 87-550-0885-2

ISSN 0418-6435

Risø Repro 1982

TABLE OF CONTENTS

1. INTRODUCTION

2. RISØ PUFF MODEL

2.1 General Characteristics

2.2 Wind Field

2.3 Turbulence Intensity and diffusion

2.4 Plume rise

2.5 Reflection

2.6 Limit of mixing depth

3. ACKNOWLEDGMENT

4. REFERENCES

APPENDICES

A. Major sections of the puff model

A. Input data section

B. Initial section

C. Calculation section

D. Output section

E. Error diagnostic section

F. Subroutines

B. Puff model flow chart

C. Puff model contractions

D. Listing of Puff Model computer code

1. INTRODUCTION

The downwind transport and distribution of atmospheric pollutants from a isolated source over land or water has become an important environmental factor in today's society. The need to understand the distribution of smoke, unpleasant or potentially harmful foreign gases and perhaps radioactive debris from a nuclear power plant accident are becoming more and more essential for industrial operations and construction planning. The dispersion of such atmospheric pollutants is commonly modeled by a standard Gaussian plume model which computes one-hour average plume characteristics.

The Meteorology Section of the Risø National Laboratory, Roskilde, Denmark, has recently developed a puff model for prediction and simulation of atmospheric pollutant diffusion.

The model considers individual puffs of pollutants with specific release rates that are advected by a horizontally homogeneous wind over a grid. The wind input may be either the measured wind from a single point, a spatial average or a wind simulation. The model simulates the instantaneous plume characteristics by adding a group of puffs, growing in size, as they advect with the wind. A Gaussian plume model, on the other hand, provides a time averaged concentration pattern based on a single time average wind vector. In the puff model, the plume advects with a time series of actual wind data. Thus, the puff model is able to predict time varying concentration distributions in actual changing wind conditions, making it an appropriate tool for dynamical computations of downwind dispersions of pollutants.

A basic comparison of a puff model simulation and a typical plume is illustrated in Fig. 1. Looking from above, the instantaneous behaviour of a plume being advected from a source by the wind is shown. The outer cone-shaped contours represent the outer limit of the plume boundary and are identical in both Figs. 1 (A) and (B).

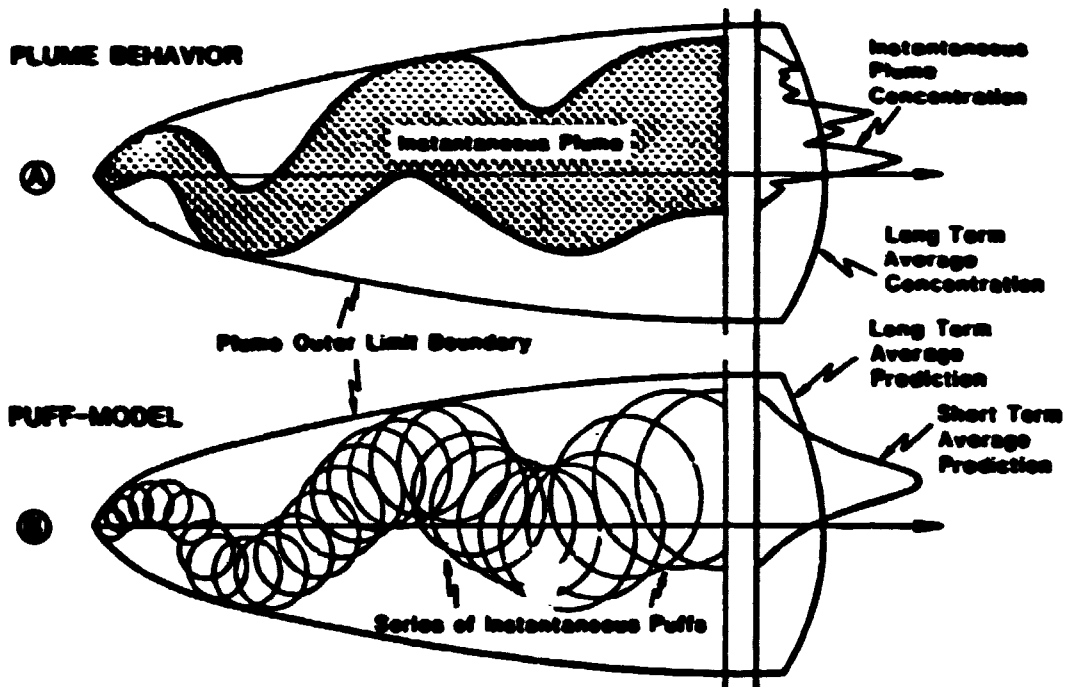


Fig. 1. Instantaneous behaviour of typical plume and a series of puffs from a puff model.

Fig. 1(A) shows an instantaneous depiction of an actual plume. The long-term average plume concentration is shown on the extreme right as a smooth curve with a maximum on the central axis. Also shown is the instantaneous plume concentration considered realistic but is of such a short time scale that it cannot be predicted or easily measured.

The puff model prediction is depicted in Fig. 1(B). The circles show the boundaries of individual puffs of pollutants released from the source. These puffs are advected and diffused downwind by a frequently updated wind. The long term average concentration prediction of the puff model is expected to be identical to the long term concentration of Fig. 1(A). The short term average pollutant prediction, a Gaussian curve shown on the extreme right, is not completely realistic but is a reasonable approximation to the instantaneous plume concentration profile.

2. RISO PUFF MODEL

2.1 General characteristics

The Riso puff model is a three-dimensional computer model used for the prediction and/or simulation of the diffusion and advection of atmospheric pollutants. The puff model technique is to simulate a plume with Gaussian shaped puffs with specified release rates within a specified grid. The initial size of the puffs is normally one meter in diameter although this can be easily adjusted. The amount of material in a puff is the release rate times the elapsed time between puffs. Therefore, a long elapsed time between puff releases results in a higher initial puff pollutant concentration than a short time interval. This should not normally be of concern if an adequate balance is maintained between grid size, advection speed and puff release

The location of the puffs on the grid is determined by computing their movement for a finite time step using a measured wind field. The growth and buoyancy of the puffs are computed from simultaneous specifications of atmospheric turbulence intensity and stability and from buoyant heat flux at the source. An inversion cap through which pollutants cannot pass and the source height where pollutants are released are variable and can easily be adjusted. Grid distances within the model may vary from meters to kilometers and time durations from seconds to hours are possible.

This puff model has the capability of monitoring a maximum of twenty-five sources of puffs and its grid may contain up to 100 puffs. A puff source can be located anywhere on the grid and have a unique release rate, start and stop of release time, and heat production. When the center of a puff moves outside the boundaries of the grid (either horizontally or vertically), that particular puff is dropped from memory. In this way the model does not store irrelevant puff information, thus keeping computer memory requirements to a minimum.

A variable to control the amount of reflection/absorption of the pollutant by the surface is easily adjusted in the puff model. Such a parameter is of great value both in actual dispersion problems and also for gaining understandings of the plume/surface relationship.

The model calculates the concentration at each grid point by summing the contributions from surrounding puffs for each advection step. The grid concentrations can be allowed to accumulate or simply be updated with the latest instantaneous value. A minimum grid concentration of interest can be set to reduce computer run time by dropping concentrations too small to be of interest.

The output of the model contains periodic results of puff locations and concentrations as well as initial input verification. The time interval for the periodic results is adjusted by the input data. This recurrent lineprinter output contains:

- X-Y plane plots showing the position of the sources and of puffs inside the grid,
- X-Z plane plots of puff positions for evaluating plume rise for each vertical level of interest, and
- a table listing of the grid point concentrations for each level.

A computer drawn contour of the magnitudes of the pollutant concentrations is also available.

When considering distance between gridpoints ($\Delta X, Y, Z$), only spatial resolution and computer resources need be considered, calculated concentrations accuracy is not related to the grid-point separation. To ensure that no essential information on individual puffs is "hidden" between grid points, the grid separation should be adjusted dependent upon the size

of the puffs at the downwind distance of interest. Other specific model configuration considerations are described in the following sections. They are also discussed in more detail in the model behaviour chapter.

2.2. Wind field

Once a puff is released, it is advected based upon wind data measurements at a single point only, normally the release point. This limits the validity of the model to situations where the wind field and turbulence can be assumed to be horizontally homogeneous throughout the grid. It is therefore important to ensure that the data obtained from such a single point measurement is representative of the wind structure for the whole area of interest.

The wind data are normally obtained in the form of a horizontal velocity time series. A vector sequence is formed by averaging over a convenient interval. These data are read into the model after being segregated into turbulence classes as discussed in the next section.

2.3 Turbulence intensity and diffusion

The growth/diffusion of a puff depends upon the turbulence intensity. To account for this growth, the puff model applies the theory for relative diffusion suggested by Smith and Hay (1961).

The turbulence intensity is defined to be the standard deviation of the wind direction (in radians) squared. These standard deviation values are collected for the same short time periods as the wind speed measurements used to advect the puffs. Therefore, the intensity of the turbulence which governs the relative diffusion of the puffs, can be adjusted along with the advecting wind speed after each time step, if the stability conditions changes.

A very low value of turbulence intensity represents a small standard deviation, normally a stable atmosphere and a weak puff dispersion/diffusion. As the atmosphere becomes more unstable, the turbulence intensity increases along with an increase of the wind direction standard deviations and plume dispersion/diffusion. While these characteristics are representative of turbulence over land, they can be applied to over water cases in a broad sense.

2.4 Plume rise

In the vertical direction, puff-rise can be accounted for by Briggs (1970) plume rise theory. In this case buoyancy is assumed to be conserved (adiabatic motion), and pressure forces, molecular viscosity and local density changes are considered small and are neglected. The rate at which a puff rises as it is advected downwind is a function of the buoyancy flux, wind speed, puff distance travelled and stability of the atmosphere. Plume rise is considered separately for each individual puff.

2.5 Reflection

The interaction of the pollutant with the surface is adjustable and can be easily changed in the input data. Total reflection or absorption or a fraction between the two can be used.

2.6 Limit of mixing depth

The effect of an atmospheric lid (inversion) can be applied in the model to limit the vertical movement of the pollutant. The model does not permit the plume to rise above this cap. When a mixing level is in effect, it acts to totally reflect the pollutant in the same manner as total reflection at the surface. This mixing cap also acts as an inversion limiting the vertical diffusion of a non-buoyant puff.

3. ACKNOWLEDGMENT

Stephan K. Rinard, The Naval Postgraduate School, Monterey, California is grateful acknowledged for, in connection with his master thesis: "An analysis of a puff dispersion model for a coastal region", to significantly improve the previous description of the Risø puff model (Mikkelsen, T. (1979) Simulation of obscuration smoke diffusion, 73 pp).

4. REFERENCES

- Mikkelsen, T. (1979). Simulation of obscuration smoke diffusion. Work done under contract to the Danish Defence Research Establishment/Risø, 73 pp. Available from: Meteorology Section, Physics Department, Risø National Laboratory, DK-4000 Roskilde, Denmark.
- Rinard, S.K. (1982). An analysis of a puff dispersion model for a coastal region. Master's Thesis from Naval Postgraduate School, Monterey, California, 88 pp.

APPENDIX A

Major Sections of the puff model

The Risø puff model code has previously been described Mikkelsen, T. (1979). The code also is well documented with comment statements. With that information and the outline to be provided in this and the following appendices, the computational and input/output procedures will be obvious.

The program and input data are stored on cards for the sake of permanency. For efficient operational execution, the program and input data cards are read on a disk within the computer. The model can then be run at will without reference to the original data cards. Minor changes can easily be made directly on the disk both to the model and/or data before each execution.

The model can be separated into the following main sections:

- a) Input data
- b) Initial
- c) Calculating
- d) Output
- e) Error diagnostics
- f) Subroutines

These will be described separately in the following sections.

A. Input data section

The input data includes the variables shown in Table IV.

Table IV

Input Data Variables for the Puff Dispersion Model

Wind History	Potential Temperature Gradient
Turbulence Intensity	Buoyant Heat Flux
Grid Dimensions	Minimum Concentration of Interest
Mixing Depth	Reflection at Ground Level
Source Locations, Start/Stop Time, Strength, Heat Emission, Number of Seconds between Advection Steps	
Number of Seconds between Printouts/Plots	
Number of Seconds between Puff Releases	

The wind field and stability class for the current time step are read at the start of the calculation section.

The variables listed above are printed as input data check and a permanent record to accompany the actual output. In most cases the print command can be overridden by YES/NO options.

B. Initial section

Based upon the input data from section (A), the initial section specifies and initializes parameters to be used in the calculating section and is passed only once during execution of the model. The grid and some counters are initialized. Constants relating to reflectance, mixing depth and stability as well as those controlling the size of some of the loops within the model are established. Parameters such as number of puff releases per second, number of advection steps per second and number of advection steps per puff release are determined.

C. Calculation section

Using current wind and stability class data read at the start of the calculation section, the model advects the puff centers and calculates the growth rate and plume rise of the puffs. It removes the puffs that have left the grid (horizontally and/or vertically). The predicted concentration is computed at the grid points to include pollutants from all nearby puffs.

D. Output section

For time intervals designated by the input data, printer plots of the X-Y and Y-Z grid are produced. A maximum mixing level is marked on the Y-Z grid if in effect.

These plots include the source location and a trace of the plume from the release time to the maptime. Also printed at this interval is a X-Y table of grid concentrations for each vertical level of interest. These concentrations can be either accumulated or actual concentrations at the plot time.

Added to the puff model is a versatile plotter routine to smooth and contour the grid magnitude concentrations of the above tables.

E. Error Diagnostic section

If the model is directed by the input data beyond the limits of the design of the program, the program is terminated by way of the error diagnostic section. It prints comments relating to the commonly made input errors enabling the user to isolate problems.

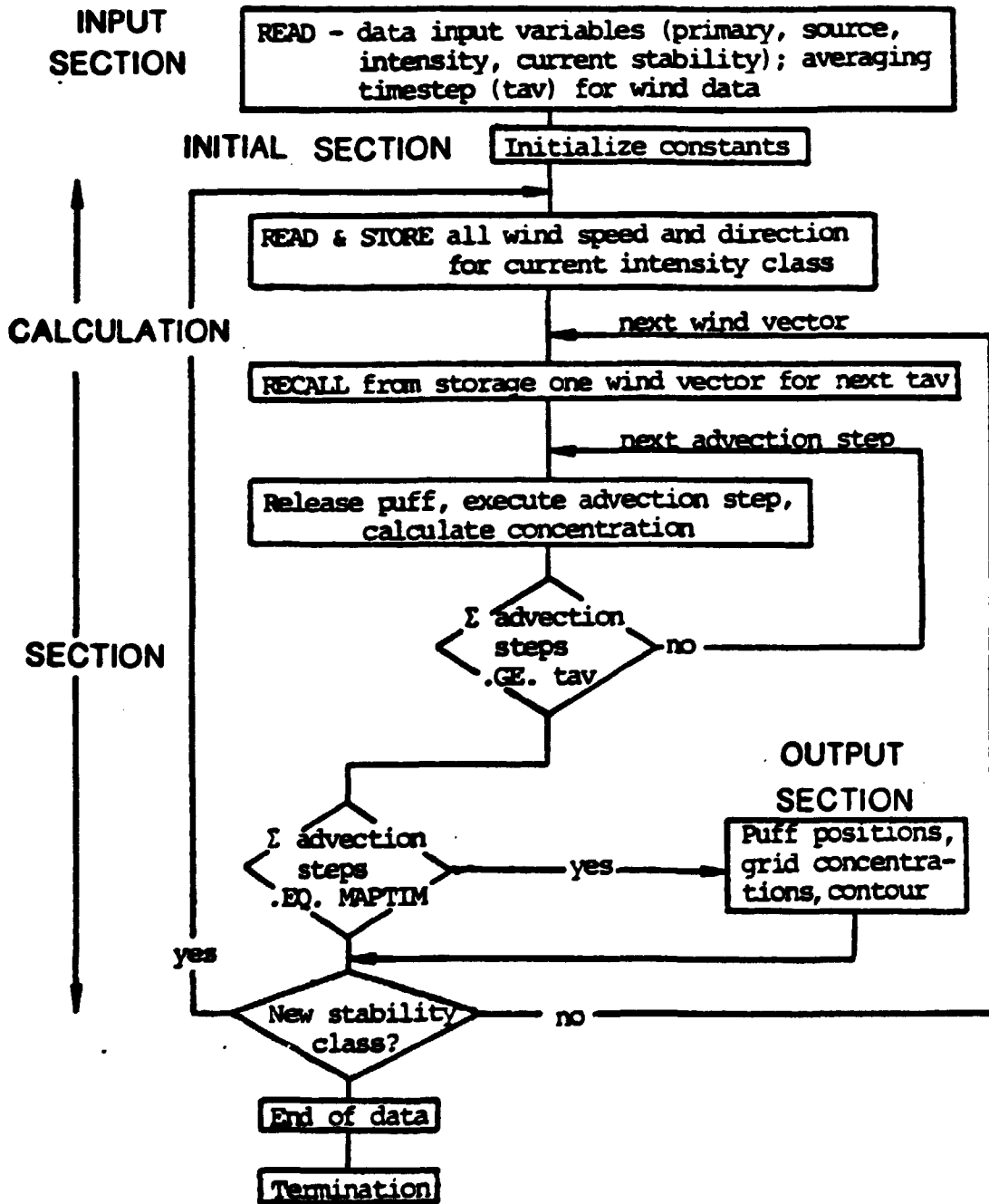
F. Subroutines

The subroutine "Sigris" calculates the puff size in the horizontal and vertical directions. It also estimates plume rise associated with pollutant buoyancy.

The subroutines "Ispace" and "Rspace" are used in the framework of the printer plots.

The subroutine "Plout" converts the plume concentrations to a logarithmic values, smoothes and then contours them using Risø inhouse contour subroutines. The values are converted to their logarithm values so that the problem of contouring over many orders of magnitude is simplified.2A

APPENDIX B
PUFF MODEL FLOW CHART



APPENDIX C

Puff Model Concentrations

CHEMIN -- Minimum grid concentration of interest
DELX, DELY, DELZ -- Distance in meters between grid points
DOSE -- Allows the concentration matrix to accumulate
DTDZ -- Potential temperature gradient (K/m) (.GE. 0)
HEAT -- Individual source heat emission (KWatt)
ICOLS -- Number of columns in grid (.LE. 10)
INST -- Instantaneous concentration matrix
ITIME -- Start time
JROWS -- Number of rows in grid
KPLANS -- Number of vertical levels in grid (includes surface)
MAPTIM -- Number of seconds between printer plots
NRELSE -- Number of seconds to stop of release
NRMULT -- Number of sources (.LE. 25)
NTADV -- Integer number of seconds between advection steps
REFLEC -- Reflection at ground level (0. none; 1.0 total)
SOURNR -- Number to identify source
SOURST -- Strength for individual source (g/s)
STOPRL -- Individual source stop time (s)
STRTRL -- Individual source start time (s)
TAU -- Integer number of seconds between puff releases
TURN -- Angle of rotation of wind direction
XSOURCE -- X coordinate of source in grid units
YSOURCE -- Y coordinate of source in grid units
ZM -- Limited mixing depth (m)

```

// EXEC PGM=IEBGENER
//SYSPRINT DD DUMMY
//SYSIN DD DUMMY
//SYSUT2 DD UNIT=SYSDA,DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=6400),
// SPACE=(TRK,(1,1)),DSN=&FTO2
//SYSUT1 DD *
WIND DATA SEPT 29 81
810929 1630 #1800#
/D
* 085*04.7* 085*04.8
/

```

APPENDIX D

LISTING OF PUFF MODEL COMPUTER CODE

```

// EXEC FRTXCLGN,NAME=CONRECQC
//FORT.SYSPRINT DD DUMMY
//FORT.SYSIN DD *

```

```

CFILE 1(KIND=DISK,TITLE='PRINDA',FILETYPE=7)
CFILE 2(KIND=DISK,TITLE='VINDDA',FILETYPE=7)
CFILE 3(KIND=DISK,TITLE='STABDA',FILETYPE=7)
CFILE 4(KIND=DISK,TITLE='SOURCEDA',FILETYPE=7)
CFILE 5(KIND=DISK,TITLE='INTSDA',FILETYPE=7)
CFILE PRINT(KIND=PRINTER,FILETYPE=7)
CFILE 6(KIND=PRINTER,FILETYPE=7)

```

```

PUF00010
PUF00020
PUF00030
PUF00040
PUF00050
PUF00060
PUF00070
PUF00160
PUF00170
PUF00180
PU00190
PU00200
UF00210
PUF00220
PUF00230
PUF00240
PUF00250

```

THIS MICRODIFFUSION PROGRAM REPRESENTS THE STATE-OF-
THE-ART CONCERNING THE DEVELOPMENT OF A NUMERIC DIFFUSION
MODEL FOR OBSCURATION SMOKE. (RISO, MET. SEC. SEPT 1978)

THE PROGRAM IS DOCUMENTED BY HEAVY USE OF COMMENT STATEMENTS.

FOR COLLECTING AN OVERALL VIEW OF THE PROGRAM STRUCTURE, AS
WELL AS TO SET UP INPUT DATA FILES, IT IS ADVISED TO
CONSULT THE FLOWCHARTS AND DESCRIPTIONS IN THE CONSECUTIVE
REPORT.

```

PUF00280
PUF00310
PUF00320
PUF00340
PUF00350
PUF00360
PUF00370
PUF00380
UF00390

```

```

COMMON HEATFX(25),I2,DMS,POINT,INTENS(14),STABPA,FBUFLX
1 SPEED, CONST1,DELZ
1 INTEGER TAU,POINT,ANGLE,XSB,XLB,YSB,YLB,ZSB,ZLB,YINT,XINTPF,YLINE
1 ZMG,ZINTPF,WINDAV,TOTTIM,SUMPUF,SOURNR,TPUFFS(25),XINT(100)
INTEGER XSOURC(25),YSOURC(25),STRTRL(25),STOPRL(25)

```

```

LOGICAL LINE,COINCD,NOMXDP,GRRFLX
DIMENSION STRING(105),HORFRM(105),VERFRM(105),IRFRMZ(105),VRFRMZ(1
105),VERPLS(105),VRPLSZ(105),PARENT(105),NBUF(7),SBUF(7)
REAL BL/' /,SN1/' /,SN2/' /,SN3/' /,SN4/' /,SN5/' /,SN6/' /,SN7/' /

```

```

PUF00410
PUF00420
PUF00430
PUF00440

```



```

600 FORMAT(6X,8HDELX  =,F10.2,6X,8HDELY  =,F10.2,6X,8HDELZ  =,F10.2 PUF00960
1) PUF00970
700 FORMAT(6X,8HCHEMIN =,E10.4,6X,8HREFLEC =,F10.5,6X,13HTURN  = PUF00980
1) PUF00990
C 1 SKIPPING LINE PRINTING OF PRIMDATA IF SPECIFIED PUF01000
IF(ABC(5) .EQ. NO ) GO TO 751 PUF01010
DO 750 I = 1,5 PUF01020
750 WRITE(6,1) PUF01030
WRITE(6,35) TITLE PUF01040
WRITE(6,1) PUF01050
WRITE(6,1) PUF01060
WRITE(6,100) PUF01070
WRITE(6,1) PUF01080
WRITE(6,200) ITIME,NRELSE,NSTEPS PUF01090
WRITE(6,1) PUF01100
WRITE(6,300) ICOLS,JROWS,KPLANS PUF01110
WRITE(6,1) PUF01120
WRITE(6,400) NTADV,MAPTIM,TAU PUF01130
WRITE(6,1) PUF01140
WRITE(6,600) DELX,DELY,DELZ PUF01150
WRITE(6,1) PUF01160
WRITE(6,700) CHEMIN,REFLEC,TURN PUF01170
WRITE(6,1) PUF01180
C 751 CONTINUE PUF01190
C C READ SOURCEDATA INPUT FILE PUF01200
C C PUF01210
C PUF01230
800 FORMAT(A1,I2,A1) PUF01240
810 FORMAT(5I5,3F10.5) PUF01250
820 FORMAT(48H CURRENT SOURCEDATA : NUMBER OF ACTIVE SOURCES :,I4) PUF01260
C PUF01270
C READ PUFFDATA,TITLESTRING PUF01280
READ(4,30) PUFFTX PUF01290
WRITE(6,30) PUFFTX PUF01300
C READ NUMBER OF MULTISOURCES:NRMULT PUF01310
READ(4,800) ABC(3),NRMULT,ABC(4) PUF01320
WRITE(6,800) ABC(3),NRMULT,ABC(4)
C INPUT FORMAT TESTING: PUF01330
IF(ABC(3).NE.AA.OR.ABC(4).NE.AA) GO TO 8920 PUF01340
C READ INDIVIDUAL SOURCEDATA: PUF01350
C C PUF01360
C SETTING FRAMEDATA: (M) SMALL-X, (M) FULL-X, ETC. PUF01370
MFY = JROWS PUF01380
MSX = 1 PUF01390
MSY = 1 PUF01400
MFZ = KPLANS PUF01410
PUF01420

```

	MSZ = 1	PUF01430
	XSB=MFX-1	PUF01440
	YLB=MSY-1	PUF01450
	ZLB=MFZ-1	PUF01460
C	BOTTOM OF FRAME : YBB = YSB - .9	PUF01470
	YBB = YSB - .9	PUF01480
	ZSB = MSZ - 1	PUF01490
	ZLB = MFZ - 1	PUF01500
	YLB=MFX-1	PUF01510
	YLL=YLB + 0.1	PUF01520
	DO 850 I = 1,NRMULT	PUF01530
	READ(4,810) SOURNR,XSOURC(I),YSOURC(I),STRTRL(I),	PUF01540
	2STOPRL(I),SOURST(I),HEATFX(I),SOHT(I)	PUF01550
	WRITE(6,810) SOURNR,XSOURC(I),YSOURC(I),STRTRL(I),	
	2STOPRL(I),SOURST(I),HEATFX(I),SOHT(I)	
C	TESTING INDIVIDUAL SOURCEDATA:	PUF01560
	IF(I.NE.SOURNR) GO TO 8910	PUF01570
C	OFF GRID TEST FOR SOURCE COORDINATES:	PUF01580
	IF(XSOURC(I).GT.XLB.OR.XSOURC(I).LT.XSB.OR.YSOURC(I).GT.YLB.OR.YSOURC(I).LT.YSB) GO TO 9000	PUF01590
	850 CONTINUE	PUF01600
C		PUF01620
	WRITE(6,2)	PUF01630
	WRITE(6,1)	PUF01640
	WRITE(6,35) PUFFTX	PUF01650
	WRITE(6,1)	PUF01660
	WRITE(6,820) NRMULT	PUF01670
	WRITE(6,1)	PUF01680
C		PUF01690
C	SETTING UP STRING VARIABLES FOR PLOTTING PURPOSES	PUF01700
	DO 911 N = 1,105	PUF01710
	STRING(N)=BL	PUF01720
	VERFRM(N)=BL	PUF01730
	VERPLS(N) = BL	PUF01740
911	HORFRM(N) = BL	PUF01750
	NY1=MFX*10	PUF01760
	DO 916 I = MSX,NY1	PUF01770
	NY2=I+4	PUF01780
	DO 915 NN = 1,NY2	PUF01790
915	HORFRM(NN)= SN4	PUF01800
	HORFRM(I+5) = SN2	PUF01810
	NY3=I+6	PUF01820
	NY4=I+9	PUF01830
	DO 916 NN = NY3,NY4	PUF01840
916	HORFRM(NN)= SN4	PUF01850
	VERFRM(10*MFX + 3) = SN5	PUF01860
	VERPLS(10*MFX + 3) = SN3	PUF01870
C		PUF01880
		PUF01890

C	OUTPRINTING CURRENT SOURCE POSITION(S) IN GRID PICTURE	PUF01920
C		PUF01930
C	SKIP PLOT OF SOURCE POSITIONS IF SPECIFIED IN 'RIMDA	PUF01940
	IF(ABC(6) .EQ. 'NO ') GO TO 999	PUF01950
C		PUF01970
	IF(ICOLS.GT. 10) GO TO 995	PUF01980
	860 FORMAT(1H ,49X,33H CURRENT SOURCE DATA AS SPECIFIED,/50X,27H IN SOURCE	PUF01990
	DATA INPUT FILE: //)	PUF02000
	865 FORMAT(1H0,50X,'SOURCES ARE REPRESENTED BY: ',/55X,'SOURCE NUMBER',	PUF02010
	1/55X,'START TIME (SEC)',/55X,'STOP TIME (SEC)',/55X,	
	2,'SOURCE STRENGTH',/55X,'BUOYANT HEAT FLUX.'//)	
	870 FORMAT(2H0 ,16H Y COORDINATE OF,25X,32H X COORDINATE OF THE GRID P	PUF02050
	POINTS/2X,16H THE GRID POINTS,18,9110/)	PUF02060
	871 FORMAT(2H0 ,16H Y COORDINATE OF,25X,32H Z COORDINATE OF THE GRID P	PUF02070
	POINTS/2X,16H THE GRID POINTS,18,9110/)	PUF02080
C		PUF02090
	WRITE(6,860)	PUF02100
	WRITE(6,865)	PUF02110
	WRITE(6,870) (I,I=XSB,XLB)	PUF02120
C	WRITING DATA INTO GRIDPOINTS:	PUF02130
	910 FORMAT(1H+,111,5X,2H +,105A1)	PUF02140
	912 FORMAT(1H+,19X,105A1)	PUF02150
	913 FORMAT(1H ,17X,1H ,105A1/1H ,17X,1H ,105A1)	PUF02160
	914 FORMAT(1H+ ,17X,1H ,105A1)	PUF02170
C		PUF02190
	WRITE(6,1)	PUF02200
	WRITE(6,912) HORFRM	PUF02210
	WRITE(6,913) VERFRM,VERFRM	PUF02220
	MAX = JROWS - 1	PUF02230
	NY5 = MAX + 1	PUF02240
	DO 950 NY6 = 1, NY5	PUF02250
	I = NY6 - 1	PUF02260
	MAXMI = MAX - I	PUF02270
	WRITE(6,910) MAXMI, VERPLS	PUF02280
	DO 920 J = 1, NRMULT	PUF02290
	IF(MAX-I .NE. YSOURC(J)) GO TO 920	PUF02300
	CALL ISPACE(XSOURC(J),J)	PUF02310
920	CONTINUE	PUF02320
	WRITE(6,913) VERFRM,VERFRM	PUF02330
C		PUF02340
	DO 932 J = 1, NRMULT	PUF02350
	IF(MAX-I .NE. YSOURC(J)) GO TO 932	PUF02360
	WRITE(6,914) VERFRM	PUF02370
	CALL ISPACE(XSOURC(J),STRTRL(J))	PUF02380
932	CONTINUE	PUF02390
	WRITE(6,913) VERFRM,VERFRM	PUF02400
		PUF02410

C	DO 934 J = 1,NRMULT	PUF02420
	IF(MAX-I .NE. YSOURC(J)) GO TO 934	PUF02430
	WRITE(6,914) VERFRM	PUF02440
	CALL ISPACE(XSOURC(J),STOPRL(J))	PUF02450
934	CONTINUE	PUF02460
	WRITE(6,913) VERFRM,VERFRM	PUF02470
C	DO 940 J=1,NRMULT	PUF02480
	IF(MAX-I .NE. YSOURC(J)) GO TO 940	PUF02490
	WRITE(6,914) VERFRM	PUF02500
	CALL RSPACE(XSOURC(J),SOURST(J))	PUF02510
940	CONTINUE	PUF02520
	WRITE(6,913) VERFRM,VERFRM	PUF02530
C	DO 930 J=1,NRMULT	PUF02540
	IF(MAX-I .NE. YSOURC(J)) GO TO 930	PUF02550
	WRITE(6,914) VERFRM	PUF02560
	CALL RSPACE(XSOURC(J),HEATFX(J))	PUF02570
930	CONTINUE	PUF02580
	WRITE(6,913) VERFRM,VERFRM	PUF02590
	WRITE(6,913) VERFRM,VERFRM	PUF02600
C	950 CONTINUE	PUF02610
	WRITE(6,1)	PUF02620
	WRITE(6,912) HORFRM	PUF02630
C	GO TO 999	PUF02640
990	FORMAT(53H SOURCE DATA PLOT SUPPRESSED BECAUSE*ICOLS*EXCEEDS 10)	PUF02660
995	WRITE(6,990)	PUF02670
999	CONTINUE	PUF02680
C	DEFINE STABILITY AND INTENSITY CLASSES	PUF02700
C	INPUT FROM INTENSITY - DATA: INTSDA	PUF02710
C	960 FORMAT(14 F5.4)	PUF02720
	965 FORMAT(1H0, 46H IN THE CURRENT RUN, THE STABILITY-CLASSES ARE,/41H	PUF02730
	1 CONNECTED TO INTENSITY DATA AS FOLLOWS:)	PUF02740
	970 FORMAT(1H ,21H STABILITY CLASS NO. :,13,1315)	PUF02750
	975 FORMAT(1H ,21H INTENSITY DATA :, 14F5.4)	PUF02760
C	READ INTSDA, TITLE-STRING:	PUF02780
	READ(5,30) INSTX	PUF02790
	WRITE(6,30) INSTX	PUF02800
C	READ INTSDA, NO. OF INTENSITY-CLASSES: NRINCL	PUF02810
	READ(5,800) ABC(3),NRINCL,ABC(4)	PUF02820
	WRITE(6,802) NRINCL	PUF02830
C	INPUT FORMAT TESTING:	PUF02840
		PUF02850
		PUF02870
		PUF02880
		PUF02890

C	NUMBER OF PUFF RELEASES PER SEC: TAUINVERS.	PUF03860
	TAUINV = 1.0/ FLOAT(TAU)	PUF03870
C		PUF03880
C	NUMBER OF ADVECTION STEPS PER SEC.: ADSTPS.	PUF03890
C	ADSTPS = 1.0/ FLOAT(NTADV)	PUF03900
C	BASIC DOSE PER PUFF:(GRAM/SEC.)*TAU = GRAM/PJFF.	PUF03910
	BADOPP = 1*TAU	PUF03920
C		PUF03930
C	NUMBER OF BASIC ADVECTION STEPS (INTEGER NUMBER) PER PUFF RELEASE:	PUF03940
	NADPRP = TAU/NTADV	PUF03950
C		PUF03960
C	NUMBER OF BASIC ADVECTION STEPS (INTEGER NUMBER) PER WINDFIELDSP.	PUF03970
	NADPRW= WINDAV/NTADV	PUF03980
C		PUF03990
C		PUF04000
C	TOTAL RUNTIME COUNTER: TOTTIM.	PUF04010
	TOTTIM =0	PUF04020
C		PUF04030
C		PUF04040
C	COUNTER FOR REMOVED PUFFS: LEAVE	PUF04050
	LEAVE = 0	PUF04060
C	STABILITY PARAMETER FOR PLUMERISE:	PUF04070
	STABPA = G/T*(DTHETE/DZ)	PUF04080
	STABPA = .033*DTDZ	PUF04090
C	CONSTANT IN CONNECTION WITH PLUMERISE FORMULA =OR USE IN	PUF04100
	SUBROUTINE SIGRIS: CONST1.	PUF04110
	CONST1 = 0.6667 * 1.6**1.5	PUF04120
C		PUF04130
C	IF MIXING DEPTH IS NOT SPECIFIED,SET NOMXDP = .TRUE.	PUF04140
	IF(ZM .EQ. 0.) NOMXDP = .TRUE.	PUF04160
C		PUF04170
C	IF REFLECTANCE AT GROUND LEVEL IS SPECIFIED,SET GRRFLX = .TRUE.	
	IF(REFLEC .GT. 0.) GRRFLX = .TRUE.	PUF04190
C	MIXING DEPTH IN GRID-UNITS: ZMG	
	ZMG = ZM/DELZ	PUF04210
C	TESTING THAT MIXING DEPTH IS INSIDE GRID:	UF04220
	IF(ZMG .GT. (KPLANS -1)) GO TO 8870	PUF04230
C		PUF04240
C	END OF INITIAL SECTION	PUF04250
C		PUF04260
C		PUF04270
C	*****	PUF04280
C	*****CALCULATION SECTION*****	PUF04290
C	*****	PUF04300
C		PUF04310
C	READING STABILITY CLASS AND WINDDATA FROM INPUTFILE:	PUF04320
	1135 READ (2,1130) (TYPE(I),DATA(I) , I = 1,14)	PUF04330

	BACKSPACE 2	
	IF (TYPE(1).EQ.ANFO) READ(2,1131)(NBUF(I),SBUF(I),I=1,7)	
	IF (TYPE(1).EQ.ANFO) WRITE(6,1131)(NBUF(I),SBUF(I),I=1,7)	
	IF (TYPE(1).EQ.SLASH) READ(2,1130)	
1131	FORMAT(7(1X,14,1X,F4,1))	
C	LOOP THRU WINDDATA AT SPECIFIED TIMESTEPS	
	I = 1	
	IF (TYPE(1).NE.SLASH) GO TO 1150	
	NRSTAB = NRSTAB + 1	
C		
C	COUNTING NUMBER OF WINDDATA SPECIFICATIONS: IWDASP	
	IWDASP = 0	
C	READING STABILITY CATEGORY FROM WINDDATA:	
	CLASS = DATA(1)	
	IF (CLASS.EQ. A) POINT = 1	
	IF (CLASS.EQ. B) POINT = 2	
	IF (CLASS.EQ. C) POINT = 3	
	IF (CLASS.EQ. D) POINT = 4	
	IF (CLASS.EQ. E) POINT = 5	
	IF (CLASS.EQ. PUNK) GO TO 8930	
	IF (CLASS.EQ. BLANK) GO TO 8940	
1140	FORMAT(53H PROGRAM STOPPED ORDINARILY FM WINDDATA SPECIFICATION)	
	WRITE(6,1)	
	WRITE(6,1141) NRSTAB,POINT	
	WRITE(6,1)	
1141	FORMAT(4H THE,13,38H. STABILITY SPECIFICATION CLASS IS NO.,11)	
	GO TO 1135	
C		
C	INPUT STRUCTURE TEST:	
1150	IF (TYPE(1).NE.ANFO .OR. TYPE(I+1).NE.ASTER) GO TO 1160	
C		
	IWDASP = IWDASP + 1	
C	CURRENT WINDDATA:	
	J1=(I+1)/2	
	ANGLE=NBUF(J1)	
	SPEED=SBUF(J1)	
	GO TO 1175	
1160	IF (TYPE(1).NE.BLANK .OR. TYPE(I+1).NE.BLANK) GO TO 8950	
C	READ NEW DATA IN LINE 1135	
	GO TO 1135	
C	INDATA PART OF PROGRAM TERMINATED.	
1175	CONTINUE	
C		
C	CURRENT WINDDATA PRESENT.	
C		
C	OUTPRINTING CURRENT WINDDATA:	
C	WRITE(6,1161) IWDASP ,ANGLE, SPEED	
C		

PUF04350
 PUF04360
 PUF04370
 PUF04380
 PUF04390
 PUF04400
 PUF04410
 PUF04420
 PUF04430
 PUF04440
 PUF04450
 PUF04460
 PUF04470
 PUF04480
 PUF04490
 PUF04500

 PUF04530
 PUF04540
 PUF04550
 PUF04560
 PUF04570
 PUF04580
 PUF04590
 PUF04600
 PUF04610
 PUF04620
 PUF04630
 PUF04640
 PUF04650
 PUF04660
 PUF04670
 PUF04680
 PUF04690
 PUF04700
 PUF04710
 PUF04720
 PUF04730
 PUF04740
 PUF04750
 PUF04760
 PUF04770
 PUF04780

C		PUF04790
C	CALCULATING WIND VELOCITY IN GRID UNITS: VGX, VGY	PUF04800
	VGX = SPEED*(COS(ANGLE*3.142/180)) / DELX	PUF04810
	VGY = SPEED*(SIN(ANGLE*3.142/180)) / DELY	PUF04820
C		PUF04830
C	RENAMING WIND AVERAGING TIME: WINDAV AS TAV:	PUF04840
	TAV = WINDAV	PUF04850
	1161 FORMAT(4H THE, I4, 49H WINDDATASET IN THE CURRENT STAB.CLASS IS: ANG	PUF04860
	1LE=, I4, 8H , SPEED=, F4.1)	PUF04870
C		PUF04880
C	LOOP THRU BASIC ADVECTION STEPS WITH CURRENT WIND FIELD	PUF04900
C		
C	DO 5000 NN=1, NADPRW	PUF04920
C		
C	JUMPING OVER "ZERO-SETTING" OF CONCENTRATION MATRIX : CHI , IF	PUF04940
C	"DOSE MODE" IS SPECIFIED IN PRIMDA.	PUF04950
C	IF(ABC(8).EQ. DOSE) GO TO 1256	PUF04960
C		PUF04970
	DO 1255 IG=1, ICOLS	PUF04980
	DO 1255 JG=1, JROWS	PUF04990
	DO 1255 KG=1, KPLANS	PUF05000
1255	CHI(IG, JG, KG) = 0.0	PUF05010
C		PUF05020
C	1256 CONTINUE	PUF05030
C		PUF05040
C	TIMECOUNTER: TOTTIM (SEC.)	PUF05050
C	TOTTIM = TOTTIM + NADV	PUF05060
C	SKIPPING RELEASE-SECTION IF SPECIFIED	
C	IF(TOTTIM .GT. NRELSE) GO TO 1250	PUF05080
C	TESTING IF RELEASE CONDITIONS ARE FULFILLED	PUF05090
C	IF(MOD(TOTTIM, TAU) .NE. 0) GO TO 1250	PUF05100
C		PUF05110
C	LOOP THRU MULTIPLE SOURCES	PUF05130
C	DO 1250 I2 = 1, NRMULT	PUF05140
C		PUF05150
C	INDIVIDUAL RELEASE CONTROL AS SPECIFIED IN SOURCE DATA:	PUF05170
C		PUF05180
C	IF((TOTTIM.LT.STRTRL(I2)) .OR. (TOTTIM.GT.STOPRL(I2))) GO TO 1250	PUF05190
C	TOTAL NUMBER RELEASED FROM SOURCE(I2): TPUFFS(I2):	PUF05200
C	TPUFFS(I2) = TPUFFS(I2) + 1	PUF05210
C		PUF05220
C	SHIFTING PUFF TABLE ONE POSITION TO THE RIGHT AND THEREBY	PUF05230
C	GIVING SPACE FOR ONE NEW PUFF:	PUF05240
C		PUF05250
	J=1	PUF05260
1204	DO 1205 K=1, 7	PUF05270
1205	SHIFT(J+1, K) = PTABEL(I2, J, K)	PUF05280
	J = J + 1	PUF05290

```

IF(J,GE,100) GO TO 8900
IF(PTABEL(I2,J,1) .NE. 0) GO TO 1204
DO 1210 L = 2,J
1209 DO 1210 K = 1,7
1210 PTABEL(I2,L,K) = SHIFT(L,K)
C
C      INSERTING NEW PUFF DATA IN PUFF TABLE AT J = 1
PTABEL(I2,1,1) = TPUFFS(I2)
C      DOSE RELEASED WITH EACH PUFF: SPECIFIED SOURCE STRENGTH*SEC.
C      BETWEEN RELEASES
PTABEL(I2,1,2) = SOURST(I2) * TAU
C
C      LOADING IN INITIAL SOURCE POSITIONS
PTABEL(I2,1,3) = XSOURC(I2)
PTABEL(I2,1,4) = YSOURC(I2)
C
C      TO AVOID NUMERICAL PROBLEMS IN ESTIMATING PLUME RISE,
C      SET SOHT(I2) (SOURCE HEIGHT) .GE. 1 METER.
PTABEL(I2,1,5) = SOHT(I2)/DELZ
C      INITIAL SIZE OF PUFFS:
C      SIGMAXY SET TO 1 METER:
PTABEL(I2,1,6) = 1
C      SIGMAZ SET TO 1 METER:
PTABEL(I2,1,7) = 1
C      END OF PUFF RELEASE SECTION.
1250 CONTINUE
C
C      ADVECTION OF ALL PUFF CENTERS
C
C      ADVANCE OF PUFF CENTERS IN GRID UNITS (HORIZONTALLY)
DGX = VGX* NTADV
DGY = VGY* NTADV
C      TOTALLY TRAVELED DISTANCE BY THE PUFFS IN METERS
C      DURING CURRENT BASIC ADVECTION STEP: DMS
DMS = SQRT((DGX*DELX)**2 + (DGY*DELY)**2)
C
C      ADVECTION SECTION FOR ALL EXISTING PUFFS:
C      LOOP THRU ALL SOURCES, COUNTING REMOVED PUFFS: LEAVE
DO 1300 I2 = 1, NRMULT
J = 1
C      SKIPPING SOURCE I2, IF THE LAST BORN PUFF HAS LEFT GRID
IF(PTABEL(I2,1,1) .EQ. 0) GO TO 1300
1260 PTBL3 = PTABEL(I2,J,3) + DGX
PTBL4 = PTABEL(I2,J,4) + DGY
C
C      CALLING SUBROUTINE "SIGRIS", THEREBY ADDING DEVIATION INCREMENT
C      AND PLUME RISE INCREMENT TO PUFF TABLE:

```

```

PUF05300
PUF05310
PUF05320
PUF05330
PUF05340
PUF05350
PUF05380
PUF05390
PUF05410
PUF05420
PUF05430
PUF05440
PUF05450
PUF05460
PUF05500
PUF05510
PUF05520
PUF05530
PUF05540
PUF05550
PUF05560
PUF05570
PUF05580
PUF05630
PUF05650
PUF05660
PUF05680
PUF05690
PUF05700
PUF05720
PUF05730
PUF05740
PUF05750
PUF05770
PUF05780
PUF05790
PUF05800
PUF05840
PUF05850
PUF05860

```

C	PTABEL(I2,J,5): Z-POSITION IN GRIDUNITS	PUF05870
C	PTABEL(I2,J,6): SIGMAXY IN METERS	PUF05880
C	PTABEL(I2,J,7): SIGMAZ IN METERS	PUF05890
C	CALL SIGRIS(PTABEL(I2,J,5),PTABEL(I2,J,6),PTABEL(I2,J,7))	PUF05900
C	INTRODUCING AN UPPER LIMIT FOR BUOYANCY CONVECTION: ZM	PUF05910
C	IF(.NOT.NOMXDP.AND.PTABEL(I2,J,5).GT.ZMG) PTABEL(I2,J,5) = ZMG	PUF05920
C	Z - POSITIONS IN GRIDUNITS: PTBL5	PUF05940
C	PTBL5 = PTABEL(I2,J,5)	PUF05950
C	TESTING AND REMOVING PUFFS WHICH HAVE LEFT THE GRID:	PUF05980
C	IF(PTBL3.GT.XSB.AND.PTBL3.LT.XLB.AND.PTBL4.GT.YBB.AND.PTBL4.LE.YL	PUF05990
C	1L.AND.PTBL5.LT.ZLB) GO TO 1290	PUF06000
C	REMOVE SECTION	PUF06010
C	LEAVE = LEAVE + 1	PUF06020
C	IF(PTABEL(I2,J+1,1).EQ.0) GO TO 1265	PUF06030
C	REMOVING PUFF BORN AT SOURCE I2 WHICH IS NOT THE LONGEST LIVING:	PUF06040
C	LEFT JUSTIFICATION OF OLDER PUFFS:	PUF06050
C	JJ = J + 1	PUF06060
C	1269 DO 1270 K = 1,7	PUF06070
C	1270 SHIFT(JJ,K) = PTABEL(I2,JJ,K)	PUF06080
C	JJ = JJ + 1	PUF06090
C	IF(PTABEL(I2,JJ,1).NE.0) GO TO 1269	PUF06100
C	SHIFT(JJ,1) = 0	PUF06110
C	JMAX = JJ	PUF06120
C	COPY SHIFT BACK INTO PTABEL:	PUF06130
C	NY7 = JMAX - 1	PUF06140
C	DO 1275 JJ = J, NY7	PUF06150
C	DO 1275 K = 1, 7	PUF06160
C	1275 PTABEL(I2,JJ,K) = SHIFT(JJ+1,K)	PUF06170
C	RETURNING TO INCREMENTAL PART WITHOUT INCREASE IN J:	PUF06180
C	GO TO 1260	PUF06200
C	REMOVING LONGEST LIVING PUFF FROM SOURCE(I2):	PUF06210
C	1265 PTABEL(I2,J,1) = 0	PUF06220
C	CONTINUING WITH NEXT SOURCE	PUF06230
C	GO TO 1300	PUF06240
C	REPLACING NEW PUFF POSITION IN PUFF TABLE	PUF06250
C	1290 PTABEL(I2,J,3) = PTBL3	PUF06260
C	PTABEL(I2,J,4) = PTBL4	PUF06270
C	CALCULATING GRID CONCENTRATION IN EACH BASIC ADVECTION STEP	PUF06280
C		PUF06290
C		PUF06300
C		PUF06330
C		PUF06340
C		PUF06350
C		PUF06380
C		PUF06390
C		PUF06420

```

C      RENAMING ESSENTIAL PARAMETERS:
C      DOSE IN CURRENT PUFF:
C      QI = PTABEL(12,J,2)
C      SIGMA VALUES IN METERS:
C      SIGMXY = PTABEL(12,J,6)
C      SIGMZ = PTABEL(12,J,7)
C
C      CALCULATING MAXIMUM CONCENTRATION IN EACH PUFF CENTER
C      (PUFF-CHEM-CENTER) IN DIMENSION: GRAM/M**3 :
C      CONSTANT : (2*PHI)**(3/2)
C      CONST = 15.7496
C
C      PCHCEN = QI/(CONST*SIGMZ*SIGMXY**2)
C
C      SKIPPING SUMMATION SECTION IF CONCENTRATION IS TOO LOW
C      IF(PCHCEN.LT.CHEMIN) GO TO 1500
C
C      CALCULATING MAXIMUM RADIUS OF INTEREST FOR EACH PUFF:
C      MAXIMUM PUFF RADIUS IN METERS:
C      PFRMXY = SIGMXY * SQRT(-2.*ALOG(CHEMIN/PCHCEN))
C      PFRMZ = PFRMXY*SIGMZ/SIGMXY
C
C      X-DIRECTION:
C      PUFRGX = PFRMXY/DELX
C      Y-DIRECTION:
C      PUFRGY = PFRMXY/DELY
C      Z-DIRECTION:
C      PUFRGZ = PFRMZ/DELZ
C
C      DETERMINING START AND STOP GRID POINTS FOR ACCUMULATION OF
C      THE PUFFS IN QUESTION:
C
C      ISTRTX = PTBL3 - PUFRGX + 1
C      ISTOPX = PTBL3 + PUFRGX
C      ISTRTY = PTBL4 - PUFRGY + 1
C      ISTOPY = PTBL4 + PUFRGY
C      ISTRTZ = PTBL5 - PUFRGZ + 1
C      ISTOPZ = PTBL5 + PUFRGZ
C
C      CONTROL FOR EXCEEDING GRID DIMENSIONS
C
C      IF(ISTRTX.LT.XSB) ISTRTX=XSB
C      IF(ISTOPX.GT.XLB) ISTOPX=XLB
C      IF(ISTRTY.LT.YSB) ISTRTY=YSB
C      IF(ISTOPY.GT.YLB) ISTOPY=YLB
C      IF(ISTRTZ.LT.ZSB) ISTRTZ=ZSB
C      IF(ISTOPZ.GT.ZLB) ISTOPZ=ZLB

```

```

PUF06430
PUF06440
PUF06450
PUF06460
PUF06470
PUF06480
PUF06490
PUF06510
PUF06520
PUF06530
PUF06540
PUF06550
PUF06560
PUF06570
PUF06590
PUF06600
PUF06610
PUF06620
PUF06630
PUF06640
PUF06650
PUF06660
PUF06670
PUF06680
PUF06690
PUF06700
PUF06710
PUF06720
PUF06730
PUF06740
PUF06750
PUF06760
PUF06770
PUF06780
PUF06790
PUF06800
PUF06810
PUF06820
PUF06830
PUF06840
PUF06850
PUF06860
PUF06870
PUF06880
PUF06890
PUF06900
PUF06910

```



```

C      UPPER LIMIT IN CASE OF SPECIFIED MIXING DEPTH:ZM
      IF(.NOT.NOMXDP .AND. ISTOPZ .GT. ZMG ) ISTOPZ = ZMG
      IF(ISTRIZ .GT. ISTOPZ) GO TO 1500
C      CALCULATE CONTRIBUTIONS TO SURROUNDING GRIDPOINTS
C      PRELIMINAR CALCULATIONS:
C      SIGMAS IN GRIDUNITS:
      SIGGX = SIGMX/DELX
      SIGGY = SIGMY/DELY
      SIGGZ = SIGMZ /DELZ
C      CALCULATING DENOMINATOR UNDER EXP-SIGN:
      SIGGX2 = (SIGGX**2)*(-2)
      SIGGY2 = (SIGGY**2)*(-2)
      SIGGZ2 = (SIGGZ**2)*(-2)
C      LOOPING THRU ALL GRIDPOINTS OF INTEREST:
      DO 1500 KG = ISTRIZ,ISTOPZ
      ZG2NEG = (KG-PTBL5)**2
      PCHI1 = PCHCEN * EXP(ZG2NEG/SIGGZ2)
      IF(GRRFLX) PCHI1 = PCHI1 + PCHCEN*REFLEC*EXP((KG+PTBL5)**2/SIGGZ2)
      IF(NOMXDP) GO TO 1295
      IF((PTBL5+PUFRGZ) .LT. ZMG) GO TO 1295
      ZG2MX = (KG+PTBL5-2*ZMG)**2
      PCHI1 = PCHI1 + PCHCEN*EXP(ZG2MX/SIGGZ2)
1295 DO 1500 IG = ISTRIX,ISTOPX
      XG2 = (IG-PTBL3)**2
      DO 1500 JG = ISTRY,ISTOPY
      YG2 = (JG-PTBL4)**2
C      INDIVIDUAL PUFFS CONTRIBUTION : PCHI,GRAM/M**3
C      PCHI = PCHI1 * EXP(XG2/SIGGX2 + YG2/SIGGY2)
C      IF(PCHI .LT. CHEMIN) GO TO 1500
C      ACCUMULATING IN GRIDPOINTS:
      CHI(IG+1,JG+1,KG+1) = CHI(IG+1,JG+1,KG+1) + PCHI
C      1500 CONTINUE
C      END OF CONCENTRATION CALCULATIONS
C
      ADVANCE IN PUFF TABLE (J) DURING BASIC ADVECTION STEP
      J = J + 1

```

```

PUF06940
PUF06950
PUF06960
PUF06970
PUF06990
PUF07000
PUF07010
PUF07020
PUF07030
PUF07040
PUF07050
PUF07060
PUF07070
PUF07080
PUF07090
PUF07100
PUF07110
PUF07130
PUF07140
PUF07150
PUF07160
PUF07170
PUF07180
PUF07190
PUF07200
PUF07210
PUF07220
PUF07230
PUF07240
PUF07250
PUF07260
PUF07270
PUF07280
PUF07290
PUF07300
PUF07310
PUF07320
PUF07330
PUF07340
PUF07350
PUF07360
PUF07370
PUF07380
PUF07410
PUF07440
PUF07450
PUF07460

```


C	MAX = JROWS - 1 OUTER LOOP THRU INTEGER Y-VALUES: NY8=MAX+1 DO 1350 NY9=1,NY8 I2=NY9-1 MAXI2 = MAX - I2 WRITE(6,1327) MAXI2 , VERPLS	PUF07960
C	PLOTTING SOURCE POSITIONS KI = 0 DO 1330 J = 1,NRMULT IF(MAX-I2 .NE. YSOURC(J)) GO TO 1330 NUMBER OF SOURCES IN MAINLINE: KI KI = KI + 1 CALL ISPACE(XSOURC(J),J) SOURCE POSITIONS IN EACH MAINLINE: XINT(KI) XINT(KI) = 10*XSOURC(J)	PUF08000 PUF08010 PUF08020 PUF08030 PUF08040 PUF08050 PUF08060 PUF08070 PUF08080 PUF08090
C	1330 CONTINUE	PUF08110 PUF08120 PUF08130 PUF08140
C	LOOPING 9 LINES DOWN TO NEXT MAINLINE: DO 1345 NY10=1,10 IDECI=NY10-1 YLINE = 10*(MAX - I2) - IDECI + 10 IF(IDECI .GE. 1) WRITE(6,1326) VERFRM	PUF08160 PUF08170 PUF08180 PUF08190 PUF08200 PUF08210 PUF08220 PUF08230 PUF08240 PUF08250 PUF08260 PUF08270 PUF08280 PUF08290 PUF08300 PUF08310 PUF08320 PUF08330 PUF08340 PUF08350 PUF08360 PUF08370 PUF08380 PUF08400
C	SCANNING THRU WHOLE PUFF TABLE DO 1340 II = 1,NRMULT J = 0 1335 J = J + 1 IF(PTABEL(II,J,1) .EQ. 0) GO TO 1340 TRUNCATING Y-VALUE OF PUFF TO INTEGER: YINT = PTABEL(II,J,4)*10 + 10.5	PUF08160 PUF08170 PUF08180 PUF08190 PUF08200 PUF08210 PUF08220 PUF08230 PUF08240 PUF08250 PUF08260 PUF08270 PUF08280 PUF08290 PUF08300 PUF08310 PUF08320 PUF08330 PUF08340 PUF08350 PUF08360 PUF08370 PUF08380 PUF08400
C	PRINTING "*" IN GRIDFRAME IF X-POSITION OF PUFF NOT COINCIDE WITH ONE OF THE SOURCE POSITIONS IF((YINT .NE. YLINE) .OR. (IDECI .NE. 0)) GO TO 1338 COINCD = .FALSE. INTEGER VALUE OF PUFFS X-POSITION: XINTPF XINTPF = PTABEL(II,J,3) * 10 + .5 DO 1336 KK = 1,KI 1336 IF(XINTPF .EQ. XINT(KK)) COINCD = .TRUE. IF(COINCD) GO TO 1335 STRING(XINTPF + 1) = SN1 GO TO 1335	PUF08160 PUF08170 PUF08180 PUF08190 PUF08200 PUF08210 PUF08220 PUF08230 PUF08240 PUF08250 PUF08260 PUF08270 PUF08280 PUF08290 PUF08300 PUF08310 PUF08320 PUF08330 PUF08340 PUF08350 PUF08360 PUF08370 PUF08380 PUF08400
C	1338 IF(YINT .NE. YLINE) GO TO 1335 PRINTING PUFF POSITIONS BETWEEN Y-GRID LINES: XINTPF = PTABEL(II,J,3) * 10 + .5	PUF08420

	STRING(XINTPF + 1) = SN1	PUF08430
	GO TO 1335	PUF08440
C	1340 CONTINUE	PUF08450
C	END OF PUFF TABLE LOOP.	PUF08470
C		PUF08480
C		PUF08490
	WRITE(6,1325) STRING	PUF08500
	DO 1342 NST = 1,105	PUF08510
C	1342 STRING(NST) = BL	PUF08520
C	1345 CONTINUE	PUF08530
C		PUF08540
C	RESET "SOURCE IN LINE COUNTER" XINT(KK)	PUF08550
	DO 1349 KK=1,10	PUF08570
C	1349 XINT(KK) = -1	PUF08580
C	1350 CONTINUE	PUF08590
C	END OF PUFF POSITION PLOT.	PUF08600
	WRITE(6,1)	PUF08610
	WRITE(6,912) HORFRM	PUF08620
C	1400 CONTINUE	PUF08630
C		PUF08640
C		PUF08650
C		PUF08660
C		PUF08670
C	PLOTTING PUFFS IN "Y-Z FRAME"; FOR COMMENTS REFER TO THE EQUI-	PUF08690
C	VALENT "Y-X FRAME" PLOTTING DESCRIBED ABOVE.	PUF08700
	WRITE(6,1)	PUF08710
	WRITE(6,1)	PUF08720
	WRITE(6,1)	PUF08730
881	FORMAT(11H, 20X, 15, 10H, SOURCE(S))	PUF08740
	WRITE(6,871) (12,12=ZSB,ZLB)	PUF08750
	WRITE(6,1)	PUF08760
C	HRFRM2 : STRING CONTAINING HORIZONTAL GRID FRAME	PUF08770
	DO 1410 N = 1,105	PUF08780
	VRFRM2(N) = BL	PUF08790
	VRPLS2(N) = BL	PUF08800
	PARENT(N) = BL	PUF08810
1410	HRFRM2(N) = BL	PUF08820
	NY11=HFZ+10	PUF08830
	DO 1418 IHFZ = MSZ,NY11,10	PUF08840
	NY12=IHFZ+4	
	DO 1411 MN = IHFZ,NY12	
1411	HRFRM2(MN) = SN4	PUF08860
	HRFRM2(IHFZ+5) = SN2	PUF08870
	NY13=IHFZ+6	
	NY14=IHFZ+9	
1416	DO 1416 MM=NY13,NY14	
	HRFRM2(MM) = SN4	PUF08890

1418	CONTINUE		
	WRITE(6,912) HRFMZ		PUF08900
	PARENT(10*ZMG + 1) = SN6		PUF08910
	VRFRMZ(10*MFZ + 3) = SN5		PUF08920
	VRPLSZ(10*MFZ + 3) = SN3		PUF08930
	WRITE(6,1326) VRFRMZ		PUF08940
	WRITE(6,1326) VRFRMZ		PUF08950
	MAX = JROWS - 1		PUF08960
	DO 1445 NY15=1, JROWS		PUF08970
	I2=NY15-1		
	MAXM12 = MAX - I2		PUF08980
	WRITE(6,1327) MAXM12, VRPLSZ		PUF08990
	K1=0		PUF09000
	DO 1430 J=1, NRMULT		PUF09010
	IF(MAX-I2 .NE. YSOURC(J)) GO TO 1430		PUF09020
	K1 = K1 + 1		PUF09030
C	1430 CONTINUE		PUF09040
	WRITING NUMBER OF SOURCES IN EACH Y-GRIDLINE: VN SOURCE(S)		PUF09050
	IF(K1 .GT. 0) WRITE(6,881) K1		PUF09060
	DO 1445 NY16=1, 10		
	IDEC1=NY16-1		
	YLINE = 10*(MAX-I2) - IDEC1 + 10		PUF09080
C	IF(IDEC1 .GE. 1) WRITE(6,1326) VRFRMZ		PUF09090
	ILLUSTRATING MIXING DEPTH IN Y-Z FRAME:		
	IF(ZMG .GT. 0) WRITE(6,1328) PARENT		PUF09110
	DO 1440 II = 1, NRMULT		PUF09120
	J=0		PUF09130
	J = J + 1		PUF09140
	IF(PTABEL(II, J, 1) .EQ. 0) GO TO 1440		PUF09150
	YINT = PTABEL(II, J, 4) * 10 + 10.5		PUF09160
	IF(YINT .NE. YLINE) GO TO 1435		PUF09170
C			PUF09180
	ZINTPF = PTABEL(II, J, 5) * 10 + .5		PUF09190
	STRING(ZINTPF + 1) = SN1		PUF09200
	GO TO 1435		PUF09210
C			PUF09220
C	1440 CONTINUE		PUF09230
C			PUF09240
	WRITE(6,1325) STRING		PUF09250
	DO 1442 NST = 1, 105		PUF09260
	1442 STRING(NST) = BL		PUF09270
C			PUF09280
C	1445 CONTINUE		PUF09290
C			PUF09300
	WRITE(6,1)		PUF09310
	WRITE(6,912) HRFMZ		PUF09320
C			PUF09330
C	SECTION FOR OUTPRINTING GRID CONCENTRATIONS		PUF09350

C		PUF09360
C	SKIPPING CONCENTRATION PRINTING IF SPECIFIED IN PRIMDA. (F(ABC(9).EQ. NO) GO TO 1600	
C	1510 FORMAT(1H0,49X,37H PRINT OF CURRENT GRID CONCENTRATIONS,/50X 1,16,29H SEC. AFTER START OF RELEASE.)	PUF09380
C	1520 FORMAT(1H0,49X,32H GRIDCONCENTRATION IN THE PLANE:,/51X,3HZ =F6.2 1,25H METER ABOVE THE SURFACE.)	PUF09390
C	1525 FORMAT(111,8X,10E10.2)	PUF09410
C	WRITE(6,1301)	PUF09420
C	WRITE(6,1510) ITOTIM	PUF09430
C	WRITE(6,1)	PUF09440
C	WRITE(6,1)	PUF09450
C	WRITE(6,1)	PUF09460
C	LOOP THRU ALL Z LEVELS	PUF09470
C	DO 1550 KC=1,KPLANS	PUF09480
C	DEM KMI = DELZ*(KC-1)	PUF09490
C	WRITE(6,1520) DEMKMI	PUF09500
C	WRITE(6,1)	PUF09510
C	WRITE(6,870) (IC,IC = XSB,XLB)	PUF09520
C	PRINTING EACH LINE IN CONCENTRATION TABLE:	PUF09530
C	DO 1560 JC = 1,JROWS	PUF09540
C	JJC = JRCWS - JC	PUF09550
C	JC1 = JJC + 1	PUF09560
C	WRITE(6,1525) JJC, (CHI(IC,JC1,KC) , IC = MSX,MFX)	PUF09570
C	DO 1551 IC=MSX,MFX	PUF09580
C	1551 CPLOT(IC,JC1)=CHI(IC,JC1,KC)	PUF09590
C	1552 FORMAT(5X,10E10.2)	PUF09600
C	1560 CONTINUE	PUF09610
C		PUF09620
C		PUF09630
C		PUF09640
C		PUF09650
C		PUF09670
C		PUF09680
C	KC IS THE NO. OF LEVELS PRINTED...HERE CONTROLS WHICH LEVELS ARE CONTOURED.	
C	IF (KC.EQ.1) CALL DRAWICPLOT,10,17)	
C	1550 CONTINUE	PUF09690
C	WRITE(6,1)	PUF09710
C	WRITE(6,1)	PUF09720
C	GO TO 1600	PUF09730
C	1590 FORMAT(95H PUFF POSITION PLOT AND GRID CONCENTRATION PRINTING AR 1E SUPPRESSED BECAUSE "ICOLS" EXCEED 10.)	PUF09750
C	1595 WRITE(6,1590)	PUF09760
C	1600 CONTINUE	PUF09770
C	END OF GRID CONCENTRATION PRINTING SECTION	PUF09780
C		PUF09790
C		PUF09800
C		PUF09830
C		PUF09840
C		PUF09870

C	END OF OUTPRINT SECTION.	PUF09880
C		PUF09910
C	5000 CONTINUE	PUF09920
C	END OF ADVECTION STEPS DURING CURRENT WIND FIELD SPECIFICATION	PUF09930
C		PUF09940
C	END OF CALCULATION PART.	PUF09960
	I = I+2	PUF09970
C	IF(I.GE.14) GO TO 1135	PUF09980
	RETURN FETCHING NEW ANGLE,SPEED:	PUF09990
	GO TO 1150	PUF10000
C		PUF10020
C	OUTPUT DIAGNOSTICS :	PUF10030
C	1000 FORMAT(37H X AND/OR Y COORDINATES OF SOURCE NR: ,I5,I2H IS OFF GRID	PUF10040
	1)	PUF10050
	1005 FORMAT(72H FORMAT ERROR IN SECOND WINDDA CARD:MISSING OR WRONG PL	PUF10060
	1 ACED #-CHARACTER))	PUF10070
	1010 FORMAT(55H BAD SPECIFICATION OF PUFF RELEASE AND ADVECTION STEP,	PUF10080
	15H TAU=,I5,6X,7H NTADV=,I5)	PUF10090
	1015 FORMAT(60H BAD SPECIFICATION OF WINDAVERAGING TIME AND ADVECTION S	PUF10100
	1TEP: ,8H WINDAV=,I4,7X,7H NTADV=,I5)	PUF10110
	1025 FORMAT(64H ERROR IN WINDATA-SPECIFICATION OF: *SPEED,*ANGLE, AFT	PUF10120
	1ER THE: ,I6,24H STABILITY SPECIFICATION)	PUF10130
	1030 FORMAT(86H MISSING STABILITY CLASS SPECIFICATION,THE LAST SPECIFI	PUF10140
	1ED STABILITY CLASS NUMBER WAS,I6)	PUF10150
	1035 FORMAT(72H FORMAT ERROR IN SECOND PUFFDA-CARD: MISSING OR WRONG PL	PUF10160
	1 ACED #-CHARACTER))	PUF10170
	1040 FORMAT(16H MISMATCH IN THE ,I5,22H. SOURCE SPECIFICATION)	PUF10180
	1045 FORMAT(12H SOURCE NR: ,I5,72H HAS MORE THN 100 CONTRIBUTING PUFFS	PUF10190
	1 IN THE GRID.TAU MUST BE INCREASED.)	PUF10200
	1050 FORMAT(72H FORMAT IN SECOND INTSDA-CARD: MISSING DR WRONG PL	PUF10210
	1 ACED #-CHARACTER))	PUF10220
	1055 FORMAT(41H ZM MUST BE AN INTEGER MULTIPLUM OF DELZ))	PUF10230
	1060 FORMAT(47H MIXING LAYER DEPTH EXCEEDS Z DIMENSION OF GRID)	PUF10250
C		PUF10260
C		PUF10270
C	8870 WRITE(6,1060)	PUF10290
	GO TO 9999	PUF10300
	8880 WRITE(6,1055)	PUF10310
	GO TO 9999	PUF10320
	8890 WRITE(6,1050)	PUF10330
	GO TO 9999	PUF10340
	8900 WRITE(6,1045) I	PUF10350
	GO TO 9999	PUF10360
	8910 WRITE(6,1040) I	PUF10370
	GO TO 9999	PUF10380
	8920 WRITE(6,1035)	PUF10390
	GO TO 9999	PUF10400


```

C      FI : BUOYANT FLUX FROM SOURCE I
C      AFTER BRIGGS:
C      F = 8.9 < M**4/SEC**3 > * Q < MWATT >
C      HEATFX(I2) UNITS ARE KW
C      FI = 8.9 * 0.001 * HEATFX(I2)
C
C      IF(STABPA.LE.0.0) GO TO 2501
C      MAXIMUM PLUME LIFT IN STABLE ATMOSPHERE:HSMAX.
C      HSMAXG = 2.9*(FI/(UNN*STABPA))**(1./3) / DELZ
2501  CONTINUE
C
C      CALCULATING PLUME HEIGHT AFTER FILFILLED ADVECTION STEP
C      HGRID(N+1) : HGNP1
C      HGNP1 = HGN + CONST1*SQRT(FI/HGN)/((DELZ *UNN)**1.5)*DMS
C      IF(STABPA.LE.0.0) GO TO 2510
C      IF(HGNP1.GT.HSMAXG) GO TO 2520
2510  HGN = HGNP1
2520  CONTINUE
      RETURN
      END
C
C      SUBROUTINE ISPACE(ITENFT,INR)
C
C      THE SUBROUTINE "ISPACE" MAKES VARIABLE TABULATING POSSIBLE
C      IN CONNECTION WITH FRAMEPLOTS.
C
C      ITENFT: NUMBER OF TEN SPACES,THE FIGURE IN QUESTION HAS TO
C              BE MOVED RIGHTMOST.
C
C      INR   : INTEGER NUMBER TO BE PRINTED.
C
10   FORMAT(1H+,19X,16)
20   FORMAT(1H+,29X,16)
30   FORMAT(1H+,39X,16)
40   FORMAT(1H+,49X,16)
50   FORMAT(1H+,59X,16)
60   FORMAT(1H+,69X,16)
70   FORMAT(1H+,79X,16)
80   FORMAT(1H+,89X,16)
90   FORMAT(1H+,99X,16)
100  FORMAT(1H+,109X,16)
C
C      IF(ITENFT.NE.0) GO TO 1
C      WRITE(6,10) INR

```

```

PUF110930
PUF110940
PUF110950
PUF110960
PUF110970
PUF110980
PUF111010
PUF111020
PUF111030
PUF111040
PUF111050
PUF111060
PUF111070
PUF111080
PUF111090
PUF111100
PUF111110
PUF111120
PUF111130
PUF111140
PUF111150
PUF111160
PUF111170
PUF111180
PUF111190
PUF111200
PUF111210
PUF111230
PUF111240
PUF111250
PUF111260
PUF111270
PUF111280
PUF111290
PUF111300
PUF111310
PUF111320
PUF111330
PUF111340
PUF111350
PUF111360
PUF111370
PUF111380
PUF111390
PUF111400
PUF111410
PUF111420

```

```

RETURN
1 IF (ITENFT.NE.1) GO TO 2
WRITE(6,20) INR
RETURN
2 IF (ITENFT.NE.2) GO TO 3
WRITE(6,30) INR
RETURN
3 IF (ITENFT.NE.3) GO TO 4
WRITE(6,40) INR
RETURN
4 IF (ITENFT.NE.4) GO TO 5
WRITE(6,50) INR
RETURN
5 IF (ITENFT.NE.5) GO TO 6
WRITE(6,60) INR
RETURN
6 IF (ITENFT.NE.6) GO TO 7
WRITE(6,70) INR
RETURN
7 IF (ITENFT.NE.7) GO TO 8
WRITE(6,80) INR
RETURN
8 IF (ITENFT.NE.8) GO TO 9
WRITE(6,90) INR
RETURN
9 IF (ITENFT.NE.9) GO TO 1000
WRITE(6,100) INR
1000 RETURN
END

```

C
C
C
C
C
C

SUBROUTINE DRAW (A,M,N)

THIS SUBROUTINE CONVERTS THE GRID CONCENTRATIONS TO LOG VALUES
THEN SMOOTHES AND CONTOURES THE PUFF ARRAY...

DIMENSION A(M,N)

A IS THE ARRAY TO BE SMOOTHED AND CONTOURED
M,N IS THE DIMENSION OF ARRAY A

```

DO 1553 JC=1,N
JJC=N-JC
JCI=JJC+1
DO 1554 IC=1,M
IF (A(IC,JCI).LT. .1E-12) A(IC,JCI)=0.0
A(IC,JCI)=A(IC,JCI)*1.E13

```

PUF11430
PUF11440
PUF11450
PUF11460
PUF11470
PUF11480
PUF11490
PUF11500
PUF11510
PUF11520
PUF11530
PUF11540
PUF11550
PUF11560
PUF11570
PUF11580
PUF11590
PUF11600
PUF11610
PUF11620
PUF11630
PUF11640
PUF11650
PUF11660
PUF11670
PUF11680
PUF11690
PUF11700
PUF11710
PUF11720

PUF11740


```

50 FORMAT(1H+,59X,F6.1)
60 FORMAT(1H+,69X,F6.1)
70 FORMAT(1H+,79X,F6.1)
80 FORMAT(1H+,89X,F6.1)
90 FORMAT(1H+,99X,F6.1)
100 FORMAT(1H+,109X,F6.1)

```

C

```

IF(ITENFT.NE.0) GO TO 1
WRITE(6,10) RNR
RETURN
1 IF(ITENFT.NE.1) GO TO 2
WRITE(6,20) RNR
RETURN
2 IF(ITENFT.NE.2) GO TO 3
WRITE(6,30) RNR
RETURN
3 IF(ITENFT.NE.3) GO TO 4
WRITE(6,40) RNR
RETURN
4 IF(ITENFT.NE.4) GO TO 5
WRITE(6,50) RNR
RETURN
5 IF(ITENFT.NE.5) GO TO 6
WRITE(6,60) RNR
RETURN
6 IF(ITENFT.NE.6) GO TO 7
WRITE(6,70) RNR
RETURN
7 IF(ITENFT.NE.7) GO TO 8
WRITE(6,80) RNR
RETURN
8 IF(ITENFT.NE.8) GO TO 9
WRITE(6,90) RNR
RETURN
9 IF(ITENFT.NE.9) GO TO 1000
WRITE(6,10) RNR
1000 RETURN
END

```

```

PUF111670
PUF111880
PUF111890
PUF111900
PUF111910
PUF111920
PUF111930
PUF111940
PUF111950
PUF111960
PUF111970
PUF111980
PUF111990
PUF120000
PUF120010
PUF120020
PUF120030
PUF120040
PUF120050
PUF120060
PUF120070
PUF120080
PUF120090
PUF121100
PUF121110
PUF121120
PUF121130
PUF121140
PUF121150
PUF121160
PUF121170
PUF121180
PUF121190
PUF122000
PUF122010
PUF122020
PUF122030
PUF122040
PUF122050

```

Risø - M -

<p>Title and author(s)</p> <p>Description of the Risø puff diffusion model</p> <p>Torben Mikkelsen</p>	<p>Date October 1982</p> <p>Department or group Physics Dept.</p> <p>Group's own registration number(s)</p>
<p>43 pages + tables + illustrations</p>	
<p>Abstract</p> <p>The Risø National Laboratory, Roskilde, Denmark, atmospheric puff dispersion model is described. This three-dimensional model simulates the release of Gaussian pollutant puffs and predicts their concentration as they are diffused and advected downwind by a horizontally homogeneous, time-dependent wind. Atmospheric characteristics such as turbulence intensity, potential temperature gradient, buoyant heat flux and maximum mixing depth have been considered.</p> <p>Available on request from Risø Library, Risø National Laboratory (Risø Bibliotek), Forsøgsanlæg Risø), DK-4000 Roskilde, Denmark Telephone: (02) 37 12 12, ext. 2262. Telex: 43116</p>	<p>Copies to</p>