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Measurement of the amplitude and phase transfer functions of an optical modulator using a heterodyne technique

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Introduction

External modulators such as Mach-Zehnder interferometers (MZI) and electroabsorption modulators (EAM) has proven advantageous for reduction of the pulse chirp compared to directly modulated lasers. Even pre-compensation of the pulse dispersion is possible in EAMs [1]. The chirp appearing on the transmitter pulse, being generated by a laser or an external modulator is due to the refractive index modulation following the intensity modulation. Due to temporal phase modulation induced by the change in refractive index additional frequency components are added to the pulse, generating a non-transform limited pulse. The small-signal intensity and refractive index behaviour of the modulator around an operation point can be described by the α -parameter [2], being defined as the ratio between the real and imaginary part of the susceptibility for a small externally induced perturbation. Different techniques have previously been used to measure the α -parameter in modulators [3,4].

We present a new technique that measures the full amplitude and phase transfer curves of the modulator as a function of the applied bias, from which the small signal α -parameter can be calculated. The technique measures the amplitude and phase transfer functions simultaneously and directly, compared to [3,4] where a time-consuming data analysis is necessary to calculate the α -parameter and an additional measurement is necessary to estimate the phase [4]. Additionally, the chirp profile for all operation points can be calculated.

Measurement technique and results

The amplitude and phase sensitive technique is based on a heterodyne detection scheme [5]. Figure 1 illustrates the principle, in which the component is inserted in one arm of a free space MZI. A small fraction of a 200 fs optical pulse from an optical parametric amplifier (OPA) is diffracted using an acousto-optic modulator (AOM). The diffracted pulse is coupled into and out of the EAM using high NA microscope objectives with an estimated coupling loss of 5 dB. After propagation through the EAM waveguide the pulse is superposed on the non-diffracted reference beam in a beam-splitter (BS). A time delay is included in the reference beam path to overlap the probe and reference pulses in time. A balanced detector measures the two quadratures from the interferometer. The 39 MHz frequency shifting of the probe beam due to the diffraction in the AOM and the following superposition with the reference beam give a beating signal with mode spacing of 300 kHz, equal to the repetition rate of the optical source. The current from the detector is amplified in a preamplifier before being measured with a lock-in amplifier. The reference signal for the lock-in amplifier is generated by down-mixing the 39 MHz sinusoidal electrical signal with a high harmonic in the synchronous TTL signal from the laser. An appropriate filtering of this signal ensures that the lock-in amplifier detects only the lowest harmonic. By fine-tuning the repetition rate of the system a mode beating below the 120 kHz bandwidth of the dual phase lock-in amplifier can be achieved. The signal measured by the lock-in amplifier is proportional to the probe and reference field amplitudes. The signal phase represents the optical phase delay. The probe pulse travelling through the waveguide has a pulse energy of < 500 fJ, which was measured to be in the small-signal regime of the EAM. The reference pulse has 100 pJ of energy. The noise of the system is dominated by the laser intensity noise inherent in the OPA system. A function generator is used to change the reverse bias over the EAM. The bias

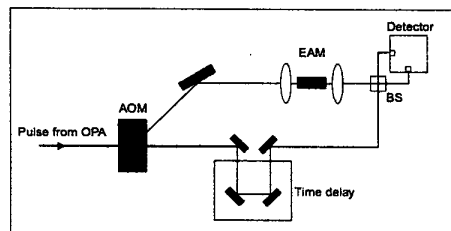


Figure 1. Schematic of the set-up.

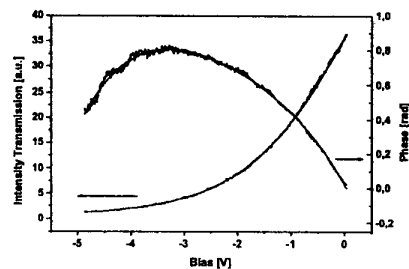


Figure 2. Intensity and phase transfer functions.

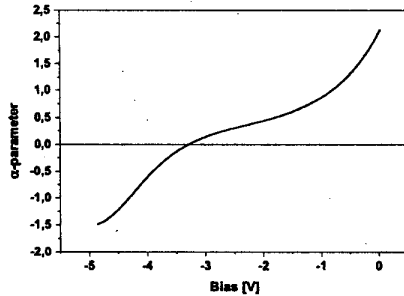


Figure 3: Calculated α -parameter from the measured data.

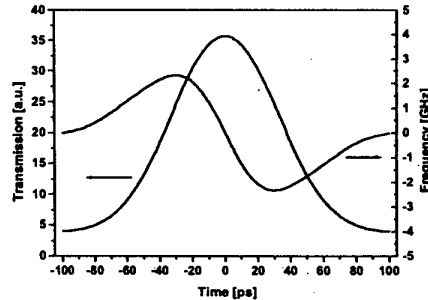


Figure 4. Calculated response of the EAM to a 5 GHz sinusoidal modulation.

is modulated using a saw-tooth shape with a 0 to -5 V swing. The modulation frequency is 55 Hz. The in-phase (X) and out-of-phase (Y) component from the lock-in amplifier is recorded on an oscilloscope, triggered by the function generator. Averaging on the oscilloscope is necessary to reduce the noise. From the X and Y components the relative amplitude transmission (T) and phase (ϕ) is calculated, $T=(X^2+Y^2)^{1/2}$ and $\phi=\text{atan}(Y/X)$, respectively.

The investigated component is a InGaAs/InGaAsP electroabsorption modulator with ten quantum wells. The device length is 200 μm . The component had an insertion loss of 12 dB at 1550 nm.

The measured intensity and phase transfer functions for the particular component investigated is shown in Figure 2, together with polynomial fits of the data. The measurement was performed with a TE polarized pulse at 1550 nm. The relative intensity transmission ($I=T^2$) shows, a reduction of the transmission as the reverse bias is applied, as expected. For a voltage sweep from 0 V to -5 V an extinction ratio of 15 dB is possible. The phase increases for increasing reverse bias until -3.3 V where it starts to decrease again. The observed maximum and change of sign of the first derivative of the phase indicates a favourable work point for low-chirp operation.

The α -parameter is calculated as

$$\alpha(V) = -\frac{2d\phi/dV}{d(\ln(I))/dV}$$

Figure 3 shows the α -parameter calculated from the polynomial fit of the measured amplitude and phase. As expected, from looking at the phase transfer function in Figure 2, the lowest α -parameter is observed at -3.3 V. Beyond this point the α -parameter is negative, and dispersion pre-compensated pulses can be generated.

To show the effect of the intensity and phase modulation at high repetition rate we calculate the response of the component to a 3 V_{pp}, 5 GHz sinusoidal modulation of the reverse bias around -1.5 V (5 GHz is chosen because it is close to the highest harmonic in a 10 Gb/s NRZ electrical pattern). The response is calculated using the fits of the measured intensity and the phase transfer curves. The extinction ratio is 9.2 dB and there is a chirp induced frequency generation of ± 2.2 GHz, corresponding to ± 0.017 nm. The pulse is negatively chirped with a blue-shifted leading edge and a red-shifted trailing edge. If instead the offset voltage is set to -3.3 V where the α -parameter is zero, a reduction of the chirp to ± 0.8 GHz is possible (not shown). The extinction ratio is in that case 9.2 dB and the insertion loss is increased with 5.5 dB.

Conclusion

We have demonstrated a new amplitude and phase sensitive technique for measuring the full amplitude and phase transfer curves of external modulators as function of applied reverse bias. The technique is faster and more direct than previous techniques. The transfer curves of an electroabsorption modulator are measured, from which a non-constant small signal α -parameter is calculated, ranging from 2.1 at 0 V to -1.5 at -5 V. An optimum point for generating transform-limited pulses is found at -3.3 V.

GiGA ApS is acknowledged for providing the components.

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