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Thummala, Prasanth; Huang, Lina; Zhang, Zhe; Andersen, Michael A. E.

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Analysis of Dielectric Electro Active Polymer Actuator and its High Voltage Driving Circuits

Prasanth Thummala, Lina Huang, Zhe Zhang and Michael A. E. Andersen
Technical University of Denmark, Department of Electrical Engineering, DK-2800 Kongens Lyngby, Denmark
Email: {pthu, huang, zz, ma}@elektro.dtu.dk

ABSTRACT
Actuators based on dielectric elastomers have promising applications in artificial muscles, space robotics, mechatronics, micro-air vehicles, pneumatic and electric automation technology, heating valves, loud speakers, tissue engineering, surgical tools, wind turbine flaps, toys, rotary motors, and grippers for material handling, etc. This paper focuses on the application of Dielectric Electro Active Polymer (DEAP) technology as an actuation mechanism for different applications. The DEAP material requires very high voltage (~2.5 kV DC) to fully utilize it as an actuator. In this paper the DEAP actuator is analyzed in detail and the actuator structures, for the wind turbine flap and the heating valve applications are shown. Different high voltage switch mode power supply topologies for driving the DEAP actuator are discussed. The simulation and experimental results are discussed.

Index Terms — Dielectric electro active polymer (DEAP), actuator, high voltage (HV), dc-dc converter, power electronics, heating valves, wind turbine flaps, PolyPower

1 INTRODUCTION

Smart materials which respond to external stimuli like light, temperature, pressure, pH, magnetic and electric fields by changing their shape or size have been a particular focus in the past decade [1]. The intelligent materials include, shape memory alloys, piezoelectric materials, etc. and deforming active polymers include hydro gels, dielectric elastomers, carbon-nano tubes and liquid crystalline elastomers. Electro Active Polymers (EAPs) that undergoes force and deformation when electrically stimulated were strongly focused in the last years.

An actuator is a mechanical device for moving or controlling a mechanism or a system. EAPs can be used as actuators in active structures, in particular when large deformations are required. Such EAP actuators convert electrical energy into mechanical energy and produce large strains. Several applications of dielectric elastomer actuators were discussed in [2]. From the electrical standpoint, DEAP actuators are capacitive loads. In [3] a low voltage driven DEAP actuator was developed using piezoelectric transformer. A novel activation strategy for dielectric elastomer actuators was proposed in [4]. Section 2 discusses the detailed analysis of the DEAP actuator and its electrical, mechanical, and electromechanical modeling, and the actuator structures for the heating valves and wind turbine flaps applications. We discuss the high voltage DC-DC converter topologies in Section 3, followed by the conclusion in Section 4.

2 DIELECTRIC ELASTOMERS AS ACTUATORS
Electro Active Polymers (EAPs) are categorized into two major classes: ionic and electronic. An electric field or coulomb forces drive electronic EAPs, while the actuation mechanism for ionic EAPs is through the diffusion or mobility of ions. The electronic EAPs generally require high electric fields (>100 V/µm) and the ionic EAPs require low driving voltages, nearly equal to 1-5V. Typical driving voltages for dielectric elastomer actuators lie in the range between 2 kV and 4 kV, depending on the polymer breakdown field and thickness of the polymer film. The operating principle of a dielectric elastomer actuator is shown in Figure 1. The DEAP material is a very thin (~40 µm) incompressible elastomer film with a compliant electrode layer on both sides [5]. A dielectric elastomer is basically a compliant capacitor. The electrodes are designed to be able to comply with the deformations of the elastomer. As for any capacitor, when an electric field is applied to the electrodes, positive charges appear on one electrode, and negative charges on the other. This gives rise to coulomb forces between opposite charges, generating a pressure, known as the Maxwell stress. The Maxwell stress forces the electrodes to move closer, thereby squeezing the polymer. As the polymer is thinned, it elongates in the directions perpendicular to the applied force [6]. The electrostatic pressure (or stress) \( \sigma \) generated by the actuator is

\[
\sigma = \frac{\varepsilon_r \varepsilon_0 \left( \frac{V_{DEAP}}{x} \right)^2}{Y} = \varepsilon_r \varepsilon_0 E^2
\]

where \( E \) is the imposed electrical field, \( x \) is the final thickness, \( V_{DEAP} \) is the voltage across the DEAP material, and \( \varepsilon_r \) and \( \varepsilon_0 \) are the permittivity of the free space \((8.85 \times 10^{-12} \text{ F/m})\) and the relative permittivity of the polymer, respectively. The mechanical strain \( S \) of the DE is given by

\[
S = -\varepsilon_r \varepsilon_0 \left( \frac{V_{DEAP}}{x} \right)^2 = -\frac{\varepsilon_r \varepsilon_0 \left( V_{DEAP} \left(1 + S\right) \right)^2}{Y x_0} \]

(2)
where $Y$ is the Young’s modulus and $d_o$ is the initial thickness of the material. Using the capacitive behavior of the polymer, DEAP can be used as an actuator, mecano-electrical sensor, as well as energy harvester to generate electricity. When operated as an actuator DEAP show unique properties, such as very low electrical power consumption, high specific elastic energy density, high speed of response, no noise, flexibility, high power density, large bandwidth, higher performance than competing technologies and light weight, hence it has the potential to be an effective replacement for conventional actuators.

**1.1 POLYPOWER DEAP ACTUATOR**

PolyPower™ dielectric elastomer (DE) is a silicone DE manufactured by Danfoss PolyPower A/S, Denmark. PolyPower DEAP actuator (Figure 2) is produced in thin sheets of 40 $\mu$m thickness. Table 1 shows the properties of the Danfoss PolyPower DEAP material. A DE sheet can be modeled as a strain dependent variable plate capacitor (3). For the unidirectional actuation shown in Figure 3, the capacitance of the DEAP actuator as a function of strain $S$ is

$$C = \varepsilon_o \varepsilon_r \frac{A}{x} = \varepsilon_o \varepsilon_r \frac{A (1+S)}{x_0 (1+S)} = \varepsilon_o \varepsilon_r \frac{A}{x_0 (1+S)}$$

(3)

**Table 1. Material properties of Danfoss PolyPower DEAP material**

<table>
<thead>
<tr>
<th>Property</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Film thickness</td>
<td>40 $\mu$m</td>
</tr>
<tr>
<td>Dielectric field strength</td>
<td>40 V/$\mu$m</td>
</tr>
<tr>
<td>Dielectric constant</td>
<td>3.1</td>
</tr>
</tbody>
</table>

**Figure 1.** Schematic showing the principle of operation of DEAP actuator. Right: Voltage is ON; Left: Voltage is OFF;

**Figure 2.** PolyPower DE tubular actuator

**Figure 3.** Left: A laminate of PolyPower DE material with corrugated surface and electrode, Right: Actuation direction of the DE material.

**1.2 DEAP ELECTRICAL MODELLING**

Figures 4a and 4b show the circuit representation of the electrical model for the DE system employed in this paper. In the figures, $R_S$ is the resistance of the electrodes and the wiring, $R_L$ is the resistance of the DE material, $C$ is the capacitance of the DE sheet, $L_S$ is the equivalent inductance of the electrodes and the high voltage cables, $v_i$ is the voltage of the power source, and $v_{DEAP}$ is the voltage over the DE sheet.

For the circuit shown in Figure 4a, the quasi-electrostatic pressure (1) at the surface of the DE sheet is induced by $v_{DEAP}$ which is given by

$$\frac{dv_{DEAP}(t)}{dt} + \left(\frac{R_L + R_S}{R_L R_S C}\right)v_{DEAP}(t) = \left(\frac{1}{R_S C}\right)v_i(t)$$

(4)

Similarly for the circuit shown in Figure 4b, the differential equations are given as,

$$v_{DEAP}(t) = R_S i(t) + L_S \frac{di(t)}{dt} + v_{DEAP}(t)$$

(5)

$$i = \frac{v_{DEAP}(t)}{R_i} + C \frac{dv_{DEAP}(t)}{dt}$$

(6)

Figures 5a and 5b are the block diagram representations for the electrical equivalents of the DEAP actuator.
1.3 DEAP MECHANICAL MODELLING

The choice of the material influences the stiffness of the material and the viscoelastic behavior of the DE actuators can be predicted by a Voigt–Kelvin five-parameter model (Figure 6) [7]. The strain response $S(t)$ to a step-stress input $\sigma$ of the five-parameter Voigt–Kelvin model is

$$S(t) = \sigma \left( \frac{1}{E_o} + \sum_{n=1}^{2} \frac{1}{E_n} (1 - \exp \left( - \frac{t}{\tau_n} \right)) \right)$$

where $\tau_n = \frac{\eta_n}{E_n}$ are the retardation time constants.

1.4 DEAP ELECTRO-MECHANICAL MODELLING

Figure 7 shows the electro-mechanical model of DEAP actuator. The input voltage $v_s$ generates a voltage across the DEAP capacitor $V_{DEAP}$ which induces an electrostatic pressure $\sigma$. The mechanical part input viz., the electrostatic pressure $\sigma$ is the input that results in a mechanical strain $S$. If the actuation strain $S$ is large, it changes the capacitance $C$, thickness $t$, and the stiffness of the material.

2.5 DIFFERENT STRUCTURES OF DEAP ACTUATORS

In this paper we focus on the application of DEAP actuator technology to two challenging applications, viz., heating valves and wind turbine flaps. The actuator structures for the two applications are discussed below.

2.5.1 WIND TURBINE FLAP APPLICATION

Implementing DEAP actuator in the wind turbine flaps will result in improved blade efficiency, reduced loads and fatigues on the blades and turbine. Figure 8 shows the typical structure of the wind turbine flap with embedded DEAP actuators.

2.5.2 HEATING VALVE APPLICATION

The current heating valve actuators in the market are thermal actuators, being noisless but consuming significant power, and electrical gear motors which are relatively energy efficient, but inherently prone to noise issues. The compact inline heating valves based on DEAP actuator will make better, cheaper and noisless valves without mechanical parts.

3 HIGH VOLTAGE POWER CONVERTERS TO DRIVE THE DEAP ACTUATOR

To drive the DEAP actuator a high voltage in the range of kilovolts is required [3, 4]. For the systematic control of the DEAP actuators that are implemented in a specific application, special high voltage power electronic (HVPE) converters with advanced control techniques are required. Simulation and experimental results for a unidirectional flyback converter are shown.

3.1 DIFFERENT TOPOLOGIES

Flyback and full bridge converters shown in Figures 10a and 10b, are some of the suitable DC-DC converter topologies for high voltage applications. However, the choice of the converter topology depends on the specific requirements of the application, which are shown in Table 2.

<table>
<thead>
<tr>
<th>Application</th>
<th>Input voltage</th>
<th>Charging Time of Actuator</th>
</tr>
</thead>
<tbody>
<tr>
<td>Wind turbine flap</td>
<td>24 V (from battery)</td>
<td>50-100 ms</td>
</tr>
<tr>
<td></td>
<td>400 V (from wind turbine)</td>
<td></td>
</tr>
<tr>
<td>Heating valve</td>
<td>3 V (from battery)</td>
<td>5-10 min</td>
</tr>
</tbody>
</table>

Table 3. Parameters of the flyback converter used in the experiment

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Values</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rated input voltage</td>
<td>24 V</td>
</tr>
<tr>
<td>Rated output voltage</td>
<td>2.5 kV</td>
</tr>
<tr>
<td>Magnetizing inductance $L_m$</td>
<td>35 µH</td>
</tr>
<tr>
<td>Flyback transformer core</td>
<td>EF20, N87</td>
</tr>
<tr>
<td>Primary turns/ Turns ratio</td>
<td>10 / 20</td>
</tr>
<tr>
<td>Leakage inductance $L_{lk}$</td>
<td>800 nH</td>
</tr>
<tr>
<td>Capacitance of DEAP actuator</td>
<td>145 nF</td>
</tr>
<tr>
<td>Primary peak current</td>
<td>5.3 A</td>
</tr>
</tbody>
</table>
In this paper we focus only on the flyback topology, for both applications. We used LT3751 capacitor charger controller to generate high voltage. However, for wind turbine flap application, if the output power requirement is too high, isolated full bridge converter is the good choice.

3.2 SIMULATION AND EXPERIMENTAL RESULTS

The simulation has been done using LTSpice software. The simulation results for a uni-directional flyback are shown below for different input voltages ($V_{in}$ = 3V, 24V and 400V).

Figures 14 and 15 are the experimental results for the uni-directional flyback converter.

4 CONCLUSION

The DEAP actuator is analyzed in detail. And the modeling of the DEAP actuator is presented. Different structures of the DEAP actuators that can be implemented in two different applications are shown. Some high voltage converter topologies for driving the capacitive loads are presented. Finally, simulation and experimental results are shown for a uni-directional flyback converter.

REFERENCES